



## GEOTECHNICAL DESIGN MEMORANDUM

**To:** Mr. Kurt Naus, P.E., S.E.

**From:** Suhaib Ibrahim  
Min Zhang, Ph.D., P.E.

**Date:** February 24, 2022

**Subject:** **IDOT PTB 189/011 IL 59 Northbound over I-55**  
**Geotechnical Recommendations**  
**Box Culvert Extensions at Seil Road West of IL 59 and IL 59 South of Seil Road**

This design memorandum presents geotechnical recommendations for the proposed design and extension of two existing box culvert structures at the Illinois Route 59 (SN: 099-0351) and Seil Road (SN: 099-0022) in Will County, Illinois. As part of the Phase II design, GSG completed a geotechnical investigation at the proposed culvert locations. The purpose of the investigation was to verify the results of the Phase I exploration completed by Himalayan Consultants (Himalayan) in 2018, and to provide supplemental design recommendations for the proposed improvements as necessary.

### 1. Introduction

As part of the Phase I design, Himalayan provided a structural geotechnical report for the proposed design and extension of two existing box culverts based on the preliminary plan and profiles and cross section, provided by IDOT in October 2018. Four (4) borings were completed to depths of 10.0 to 15.0 feet, at the proposed work locations. Geotechnical evaluation and recommendations were provided for the proposed extensions. The Phase 1 design report provided by Himalayan Consultants is included as **Attachment E**.

Based on the cross sections provided by Benesch for the proposed improvements in November 2020 (**Attachment A**) and the plan view of the culverts (**Attachment B**), the project includes extending two existing culverts at Seil Road and IL 59 in Will County, IL. The proposed geometry information is summarized in **Tables 1 and 2** for Phase I and II investigations, respectively.

**Table 1 Summary of Culvert information During Phase I investigation**

Structure	Inlet Elevation (feet)	Outlet Elevation (feet)	Upstream Extension (feet)	Downstream Extension (feet)
IL 59 Culvert	587.5	586.43	28.0	170.0
Seil Road Culvert	586.0	585.8	20.0	30.0

**Table 2 Summary of Culvert information During Phase II investigation**

Structure	Inlet Elevation (feet)	Outlet Elevation (feet)	Upstream Extension (feet)	Downstream Extension (feet)
IL 59 Culvert	587.2	586.9	24.5	160.0
Seil Road Culvert	585.7	585.5	14.0	44.0

## 2. Field Exploration Summary

GSG completed one soil boring (GCB-01) to a depth of 40.0 feet for the proposed improvements during Phase II field exploration. GSG also completed three subgrade borings (SGB-110, SGB-116, and SGB-117), one retaining wall boring (RWB-13), and one overhead sign boring (OHS-10) in the vicinity of the two culverts. A boring location plan, including the Phase 1 borings completed by Himalayan (CB-01 through CB-04), is provided in **Attachment B**. Copies of the boring logs are provided in **Attachment C**.

The surface elevation for boring GCB-01 (drilled by GSG) is 609.6 feet and was blind drilled to elevation 589.6 feet, approximately where CB-01 through CB-04 were drilled. Silty clay fill was encountered between elevations 589.6 and 581.0 feet, followed by very stiff to hard silty clay to elevation 549.6 feet, with unconfined compressive strength ranging between 2.9 and 4.6 tsf. Medium dense silty loam was encountered between elevations 549.6 and 548.0 feet, with SPT blow count (N) values of 23 blows per foot. The SGB borings encountered silty clay fill within the full boring depths. The general soil condition observed during the Phase II investigation was consistent with borings completed by Himalayan Consultants during the Phase I investigation, with the exception of the saturated sand layer encountered in CB-04 between elevations 586.5 to 584.0 feet.

Groundwater was not encountered during drilling at boring GCB-01. Based on the color change from brown and gray to gray, it is anticipated that the long-term groundwater level could be at an approximate elevation 579 feet, which is deeper than the ground water level provided by Himalayan.



### 3. Foundation Analysis and Recommendations

The following recommendations for the Culvert and Wingwalls are provided in the SGR by Himalayan dated 12/26/2018:

- For both culverts, the foundation soil at the invert elevation was estimated to have a factored bearing resistance of 6000 psf for strength limit state and a bearing resistance of 3700 psf for service limit state. The differential settlement along the culvert extensions is estimated to be 0.5 inch or less under this design bearing resistance.
- For the anticipated concrete wingwalls at both culverts, a factored bearing resistance of 7000 psf for strength limit state and a bearing resistance of 4000 psf for service limit state can be used to design the footing for the T type of wingwall bearing on very stiff to hard silty clay. The differential settlement along the wall is estimated to be 0.5 inch or less under this design bearing resistance.
- For yielding wingwalls, the following lateral earth pressure parameters were recommended assuming free drain of granular backfill was used. A geometric drain and free drain granular backfill should be placed behind the wall.

Backfill/Load on top of Wingwalls	Horizontal Backfill	1V:2.5H Backfill	Adjacent to the height of barrel
Equivalent fluid pressure (psf/ft)	40	50	60

- High moisture and low strength soil encountered at the invert elevation or the bottom of the wingwall should be removed and replaced with granular backfill.

GSG concurs with the foundation analysis and recommendations regarding bearing resistance, culvert type, and wingwall recommendations as summarized above.

### 4. Excavation Recommendations

It is anticipated that the roadway embankment will be open cut in order to construct the culvert extensions. All excavations that extend more than 4 feet should be sloped or braced to prevent excavation instability. The excavation sloping and bracing should be designed in accordance with the Occupational Safety and Health Administration (OSHA) 29 CFR, Part 1926, regulations and requirements.

The top elevation of the embankment above the IL 59 Culvert is at approximately 609 feet and the bottom of the culvert at 587.0 feet. The total excavation depth will be approximately 22 feet. For Seil Road Culvert, the top of the embankment above the culvert is at approximately



606 feet, and the bottom of the culvert at 585.5 feet. The total excavation depth will be approximately 20.5 feet. Slope stability analysis for the excavations was performed using software SLIDE 2018. SLIDE 2018 is a comprehensive slope stability analysis software used to evaluate the proposed slopes for the project based on the limit equilibrium method. A circular failure analysis was evaluated for both a short term (undrained) and long term (drained) using the simplified Bishop analyses methods.

**Table 3 – Slope Stability Analyses Results**

Analysis Exhibit	Soil Profile Location	Proposed Excavation Slope	Analysis Type	Factor of Safety	Minimum Required Factor of Safety
Exhibit 1a	IL 59 Culvert SGB-116, SGB-110, OHS-10	1.75H:1V	Circular – Short Term	5.2	1.7
Exhibit 1b			Circular – Long Term	1.8	1.7
Exhibit 1c	Seil Rd Culvert SGB-117, RWB-13	1.75H:1V	Circular – Short Term	4.7	1.7
Exhibit 1d			Circular – Long Term	1.8	1.7

Based on the analyses performed, a maximum slope of 1.75H:1V should be maintained to satisfy the minimum factor of safety of 1.7. Copies of the analysis exhibits are included in the Slope Stability Analyses Exhibits (**Attachment D**).

Should you have any questions or require additional information, please call us at 630-994-2600.

Sincerely,



Suhaib Ibrahim  
Project Engineer



Min Zhang, Ph.D., P.E.  
Project Engineer

Attachment A: IL 59 and Seil Road Culvert Cross Sections

Attachment B: Soil Boring Location Plan

Attachment C: Soil Boring Logs

Attachment D: Slope Stability Analyses Exhibits

Attachment E: I-55 at IL 59\_Culvert SGR by Himalayan Consultants



## **Attachment A**

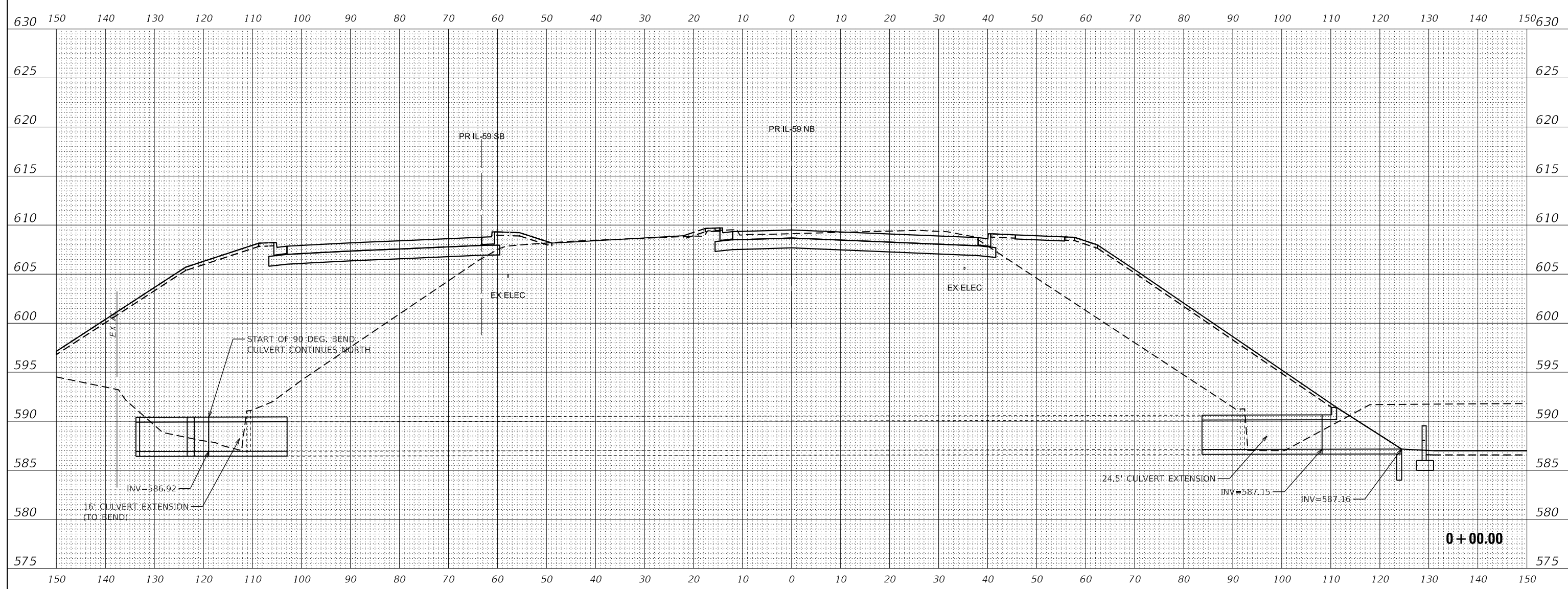
### **IL 59 and Seil Road Culvert Cross Sections**

FINAL SURVEY	SURVEYED	DATE
NOTE BOOK	PLOTTED	BY
NO.	TEMPLATE	
	AREAS CHECKED	

ORIGINAL SURVEY	SURVEYED	DATE
NOTE BOOK	PLOTTED	BY
NO.	TEMPLATE	
	AREAS CHECKED	

MODEL: SMODELNAMEN  
FILE NAME: SFILEL

NOTE: CULVERT IS ALIGNED AT A 94.05 DEG. SKEW TO PROPOSED IL 59 NB ALIGNMENT



USER NAME = \$USERS	DESIGNED -	REVISED -
PLOT SCALE = \$SCALES	DRAWN -	REVISED -
PLOT DATE = \$DATES	CHECKED -	REVISED -
	DATE -	REVISED -

**STATE OF ILLINOIS  
DEPARTMENT OF TRANSPORTATION**

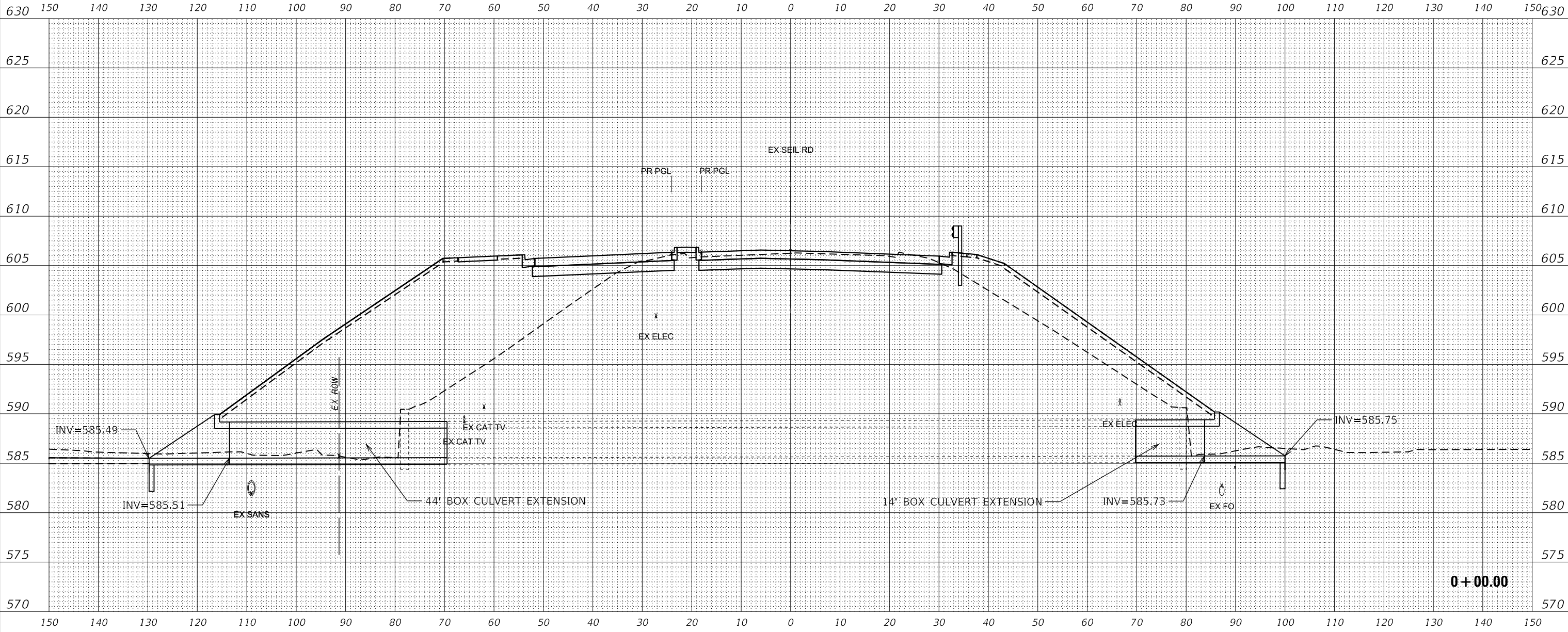
SCALE: SHEET OF SHEETS STA. 0+00.00 TO STA. 0+00.00

F.A. RTE.	SECTION	COUNTY	TOTAL SHEETS	SHEET NO.
CONTRACT NO.				
ILLINOIS FED. AID PROJECT				

DATE	
BY	
SURVEYED	
PLOTTED	
TEMPLATE	
NOTE BOOK	
AREAS CHECKED	
NO.	

DATE	
BY	
SURVEYED	
PLOTTED	
TEMPLATE	
NOTE BOOK	
AREAS CHECKED	
NO.	

NOTE: CULVERT IS ALIGNED AT A 94.03 DEG. SKEW TO EXISTING SEIL ROAD ALIGNMENT



MODEL: SMODELMMMS  
FILE NAME: SP1ELS

USER NAME = \$USERS	DESIGNED - _____	REVISED - _____
	DRAWN - _____	REVISED - _____
PLOT SCALE = \$SCALE\$	CHECKED - _____	REVISED - _____
PLOT DATE = \$DATE\$	DATE - _____	REVISED - _____

**STATE OF ILLINOIS  
DEPARTMENT OF TRANSPORTATION**

SCALE: _____	SHEET _____ OF _____ SHEETS	STA. 0+00.00 TO STA. 0+00.00.
--------------	-----------------------------	-------------------------------

F.A. RTE.	SECTION	COUNTY	TOTAL SHEETS	SHEET NO.
CONTRACT NO. _____				
ILLINOIS FED. AID PROJECT				

**Attachment B**  
**Soil Boring Location Plan**





**Attachment C**  
**Soil Boring Logs**



# SOIL BORING LOG

ROUTE I-55 and IL 59 DESCRIPTION Culvert LOGGED BY MH

SECTION 2018-075-R LOCATION West of IL-59 SB

COUNTY WILL DRILLING METHOD HSA HAMMER TYPE AUTO

STRUCT. NO.	Station	DEPTH	BLOW	UCS	MOIST	Surface Water Elev.	Stream Bed Elev.	Groundwater Elev.:	First Encounter	Upon Completion	After	Hrs.	DEPTH	BLOW	UCS	MOIST
		(ft)	(/6")	(tsf)	(%)	ft	ft		ft	ft	ft		(ft)	(/6")	(tsf)	(%)
Culvert Boring						N/A	N/A		None	N/A	N/A					
GCB-01	7002+3.6			Qu												
	28.00ft RT															
	609.62	ft														
Blind drill to 20 feet						Brown, Gray, and Black, Moist FILL: SILTY CLAY, trace sand and gravel										
														6		
														4		NR
														5		
														2		
														5	4.8	16
		-5												6	B	
														6		
														9	5.8	15
														10	B	
														5		
						580.62								7	4.6	22
		-10												13	B	
														4		
														6	2.9	17
														9	B	
														9		
														10	3.5	18
		-15												11	P	
														9		
														11		13
														12		
														9		
														11		13
														12		
														9		
														11		13
														12		
		589.62												9		
		-20												11		13
														12		
														9		
														11		13
														12		
														9		
														11		13
														12		
														9		
														11		13
														12		
														9		
														11		13
														12		
														9		
														11		13
														12		
														9		
														11		13
														12		
														9		
														11		13
														12		
														9		
														11		13
														12		
														9		
														11		13
														12		
														9		
														11		13
														12		
														9		
														11		13
														12		
														9		
														11		13
														12		
														9		
														11		13
														12		
														9		
														11		13
														12		
														9		
														11		13
														12		
														9		
														11		13
														12		
														9		
														11		13
														12		
														9		
														11		13
														12		
														9		
														11		13
														12		
														9		
														11		13
														12		
														9		
														11		13
														12		
														9		
														11		13
														12		
														9		
														11		13
														12		
														9		
														11		13
														12		
														9		
														11		13
														12		
														9		
														11		13
														12		
														9		
														11		13
														12		
														9		
														11		13
														12		
														9		
														11		13



# SOIL BORING LOG

ROUTE I-55 and IL 59 DESCRIPTION Culvert LOGGED BY MH

SECTION 2018-075-R LOCATION West of IL-59 SB

COUNTY WILL DRILLING METHOD HSA HAMMER TYPE AUTO

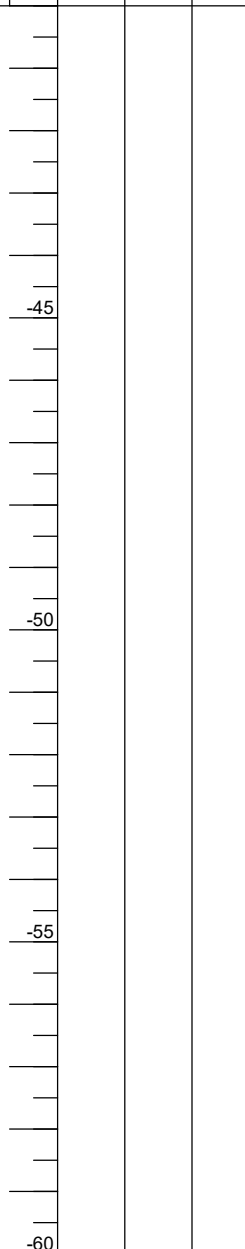
STRUCT. NO. Culvert Boring  
Station \_\_\_\_\_

BORING NO. GCB-01  
Station 7002+3.6  
Offset 28.00ft RT  
Ground Surface Elev. 609.62 ft

D E P T H  (ft)	B L O W S  (/6")	U C S  (tsf)	M O I S T  (%)
-----------------------------------	------------------------------------	--------------------------	----------------------------------

Surface Water Elev. N/A ft  
Stream Bed Elev. N/A ft  
  
Groundwater Elev.:  
First Encounter None ft  
Upon Completion N/A ft  
After N/A Hrs. N/A ft

limestone fragments (ML)  
End of Boring



The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)  
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)



# SOIL BORING LOG

ROUTE I-55 and IL 59 DESCRIPTION Roadway Boring LOGGED BY MH

SECTION 2018-075-R LOCATION Ramp D

COUNTY WILL DRILLING METHOD HSA HAMMER TYPE AUTO

STRUCT. NO. Station	DEPTH (ft)	BLOW COUNT (/6")	UCS Qu (tsf)	MOIST CONTENT (%)	Surface Water Elev. <u>N/A</u> ft Stream Bed Elev. <u>N/A</u> ft
BORING NO. <u>SGB-110</u> Station <u>400+53.7904</u> Offset <u>18.06ft LT</u> Ground Surface Elev. <u>603.23</u> ft					Groundwater Elev.: First Encounter <u>None</u> ft Upon Completion <u>N/A</u> ft After <u>N/A</u> Hrs. <u>N/A</u> ft
10 inches of Asphalt 5 inches of Aggregate Base Course <u>601.98</u>		5			
Brown, Black, and Gray, Moist FILL: SILTY CLAY, with sand and gravel		4	4.8	22	
		8	B		
	4				
	5	4.6	13		
	-5	9	B		
Cobbles at 6-7.5 feet	9				
	11	4.5	16		
	12	P			
Cobbles at 8.5-10 feet	12				
	8	5.4	12		
	-10	14	B		
	32				
	15		10		
	7				
	4				
	8	5.0	20		
	-15	8	P		
<u>587.23</u>					
Brown, Black, and Gray, Moist FILL: SILTY CLAY, trace gravel	5				
	5	2.5	25		
	7	B			
	4				
	5	5.0	22		
<u>583.23</u> -20	10	P			

End of Boring

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)

The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)







# SOIL BORING LOG

ROUTE I-55 and IL 59 DESCRIPTION Ramp D from IL-59 SB to SW Frontage Rd LOGGED BY AB

SECTION 2018-075-R LOCATION West of IL 59

COUNTY WILL DRILLING METHOD HSA HAMMER TYPE AUTO

STRUCT. NO. Station	DEPTH H	BLOW S	UCS Qu	MOIST T	Surface Water Elev. Stream Bed Elev.	DEPTH H	BLOW S	UCS Qu	MOIST T
	(ft)	(/6")	(tsf)	(%)	N/A ft N/A ft	(ft)	(/6")	(tsf)	(%)
BORING NO. <u>OHS-10</u> Station <u>402+36.60</u> Offset <u>17.21ft LT</u> Ground Surface Elev. <u>592.15</u> ft					Groundwater Elev.: First Encounter <u>573.7</u> ft ▼ Upon Completion <u>N/A</u> ft After <u>N/A</u> Hrs. <u>N/A</u> ft				
6 inches of Topsoil Brown, Black and Gray, Moist FILL: SILTY CLAY, trace gravel and organics	591.65	2 3 4	1.5 B	20	20.0 feet End of Boring				
		4							
		7 9	6.0 B	19					
	-5					-25			
	586.15								
Gray and Brown, Moist FILL: SILTY CLAY, trace gravel		5 6 8	4.0 B	20					
		3 4 6	3.1 B	22					
	-10					-30			
	581.15								
Very Stiff Gray, Moist SILTY CLAY (CL/ML)		5 8 10	3.5 P	19					
		4 6 8	3.0 P	19					
	-15					-35			
	576.15								
LIMESTONE, highly weathered		8 13 13		7					
		32							
		50/2"		6					
Auger and split spoon refusal at	572.15	-20				-40			

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)  
 The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)





# SOIL BORING LOG

ROUTE I-55 and IL 59 DESCRIPTION Retaining Wall 1 LOGGED BY AB

SECTION 2018-075-R LOCATION Seil Rd WB off road

COUNTY WILL DRILLING METHOD HSA HAMMER TYPE AUTO

STRUCT. NO. W099-1001  
 Station \_\_\_\_\_

BORING NO. RWB-13  
 Station 4015+79.5151  
 Offset 17.86ft LT  
 Ground Surface Elev. 602.30 ft

DEPTH H S	UCS Qu	MOIST T	Surface Water Elev. _____ N/A ft	DEPTH H S	UCS Qu	MOIST T
(ft)	(tsf)	(%)	Stream Bed Elev. _____ N/A ft	(ft)	(tsf)	(%)
6 inches of Topsoil Brown, Gray, and Black, Moist FILL: SILTY CLAY, with gravel						
5				5		
6	0.6	22		8	4.2	23
6	B			10	B	
			578.80			
3				4		
7	2.3	16		7	4.2	20
-5	B			-25	B	
4				10		
7	4.4	14		14	NR	19
16	B			13		
7				3		
6	2.5	17		4	1.7	32
-10	B			5	B	
			572.30	-30		
6						
7	4.2	16				
10	B					
2						
5	2.9	21				
-15	B			-35		
10						
10	NR	22				
10						
5						
9	6.9	21				
-20	B			-40		

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)  
 The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)

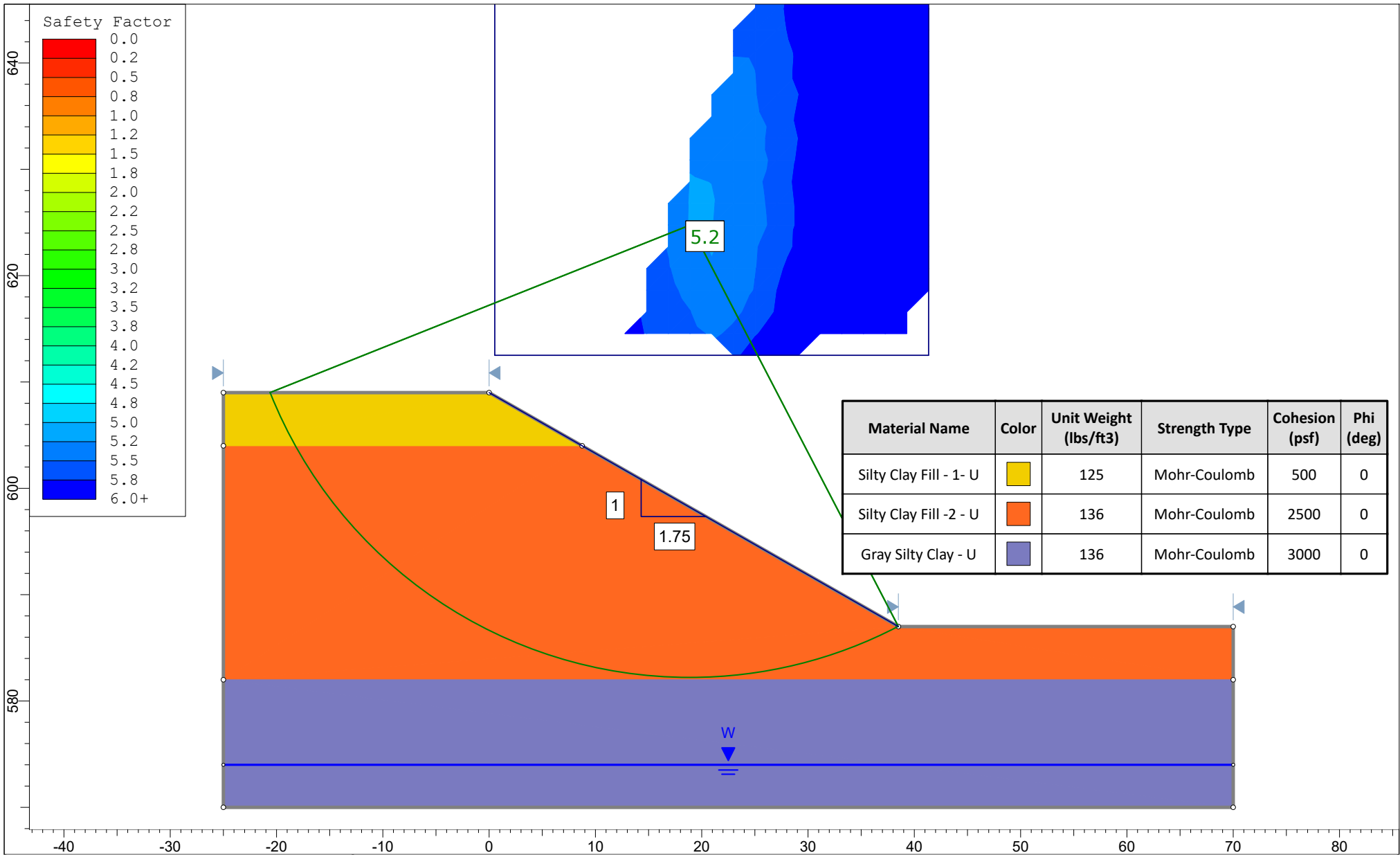






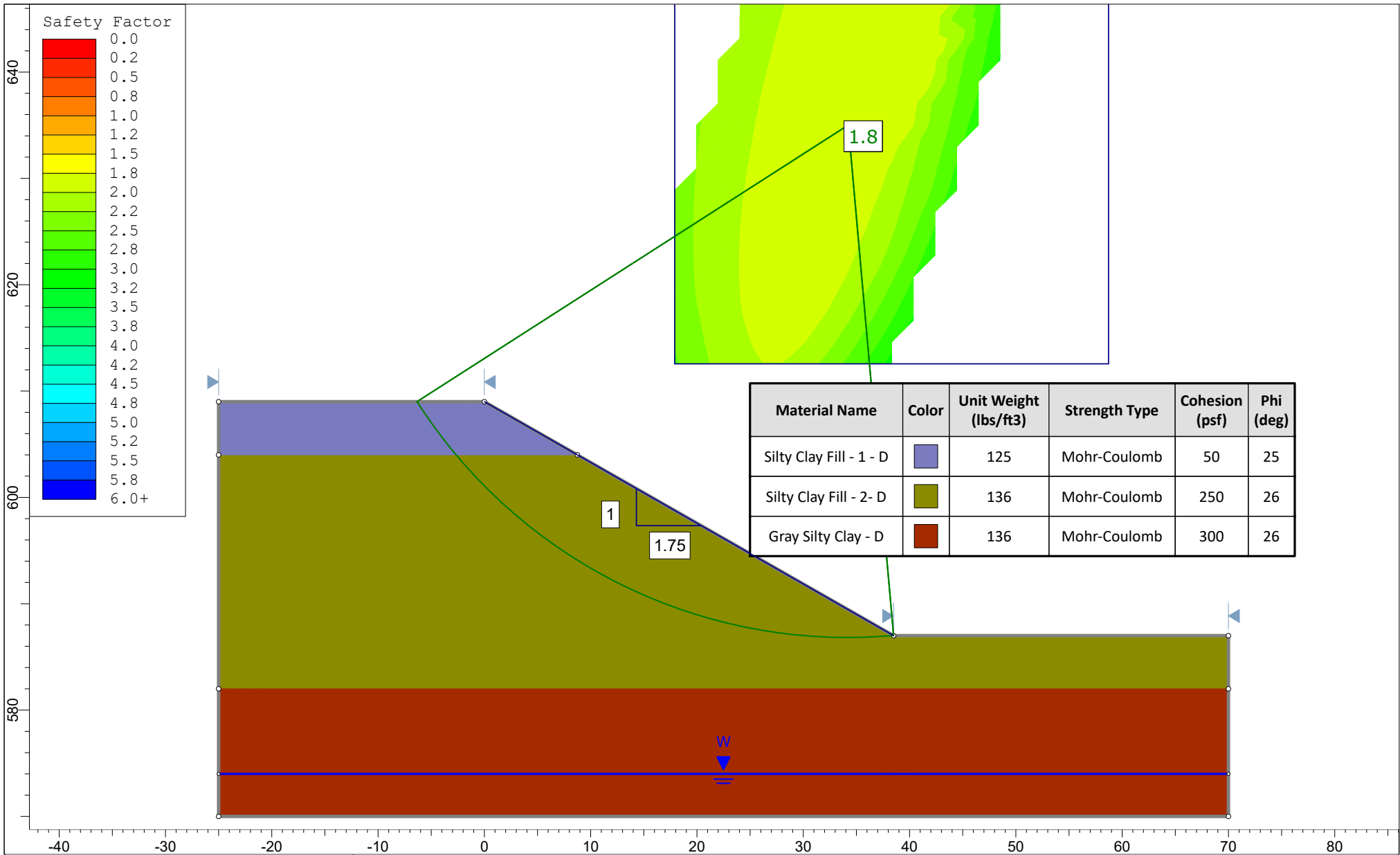


**Attachment D**  
**Slope Stability Analyses Exhibits**



**GSG CONSULTANTS, INC.**  
 623 Cooper Court • Schaumburg, IL 60173  
 Tel: 630.994.2600 • Fax: 312.733.5612  
[www.gsg-consultants.com](http://www.gsg-consultants.com)

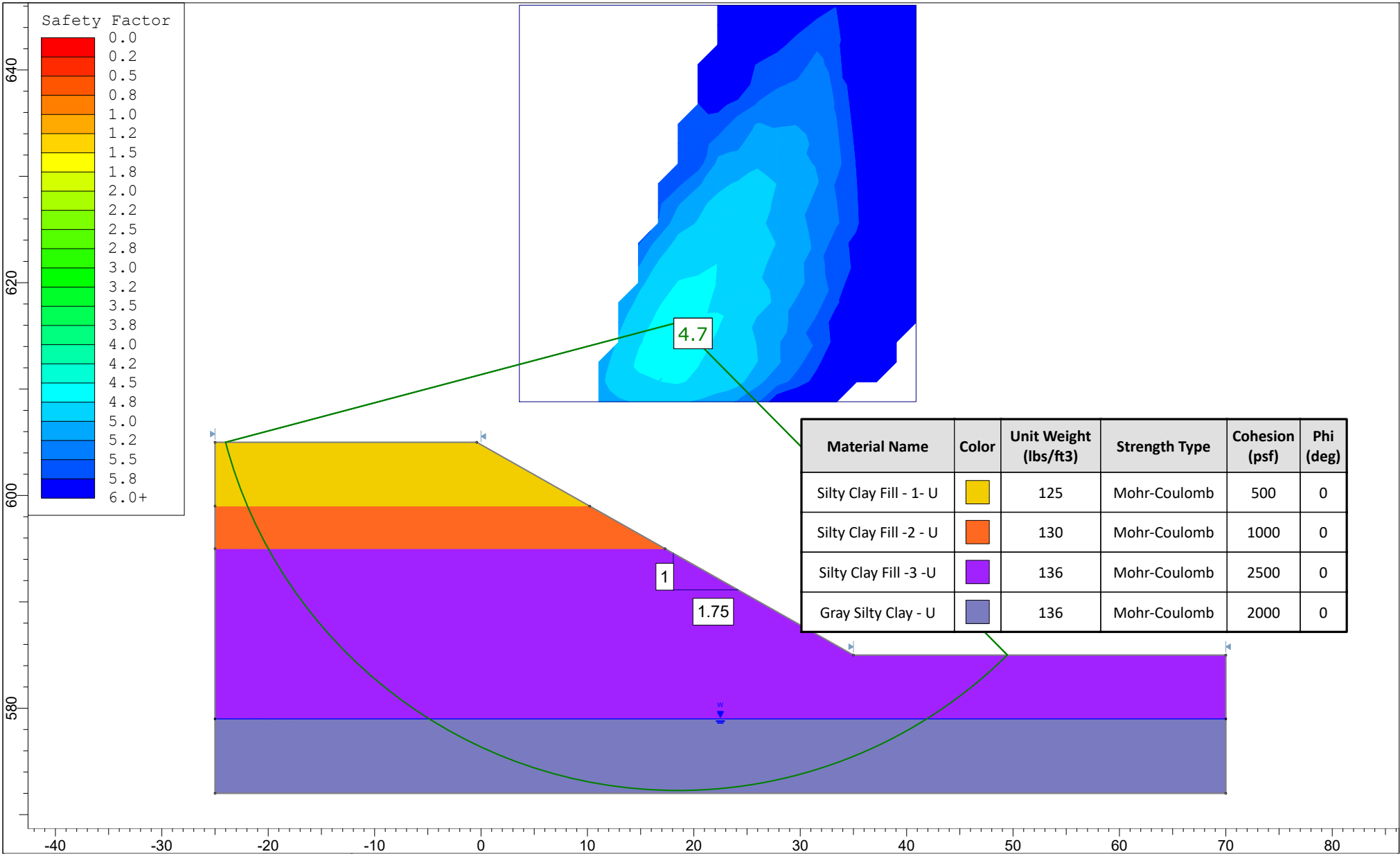
<i>Project</i>		IL 59 Culvert Excavation	
<i>Analysis Description</i>		Exhibit 1a - Circular Failure Short Term - Undrained	
<i>Drawn By</i>	MZ	<i>Scale</i>	1:150
<i>Date</i>	11/24/2020	<i>Company</i>	GSG Consultants, Inc.
		<i>File Name</i>	IL59 Culvert.slmd



**GSG CONSULTANTS, INC.**  
 623 Cooper Court • Schaumburg, IL 60173  
 Tel: 630.994.2600 • Fax: 312.733.5612  
[www.gsg-consultants.com](http://www.gsg-consultants.com)

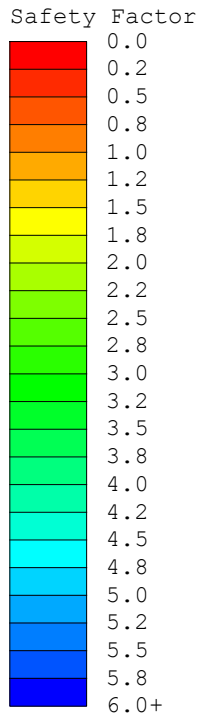
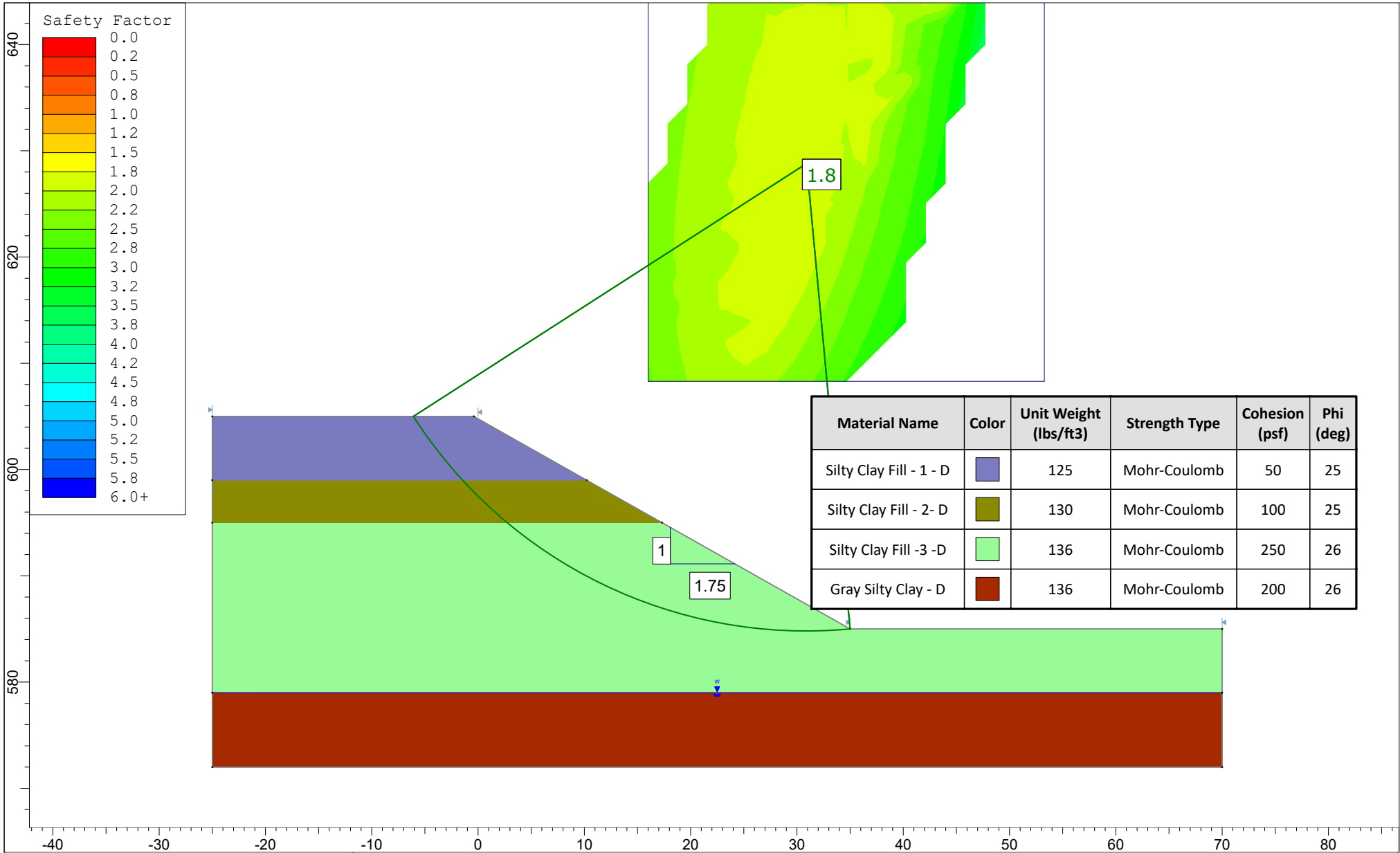
<i>Project</i>		IL 59 Culvert Excavation	
<i>Analysis Description</i>		Exhibit 1b - Circular Failure Long Term - Drained	
<i>Drawn By</i>	MZ	<i>Scale</i>	1:150
<i>Date</i>	11/24/2020	<i>Company</i>	GSG Consultants, Inc.
		<i>File Name</i>	IL59 Culvert.slmd





**GSG CONSULTANTS, INC.**  
 623 Cooper Court • Schaumburg, IL 60173  
 Tel: 630.994.2600 • Fax: 312.733.5612  
[www.gsg-consultants.com](http://www.gsg-consultants.com)

<i>Project</i>			Seil Road Culvert Excavation		
<i>Analysis Description</i>			Exhibit 1c - Circular Failure Short Term - Undrained		
<i>Drawn By</i>	MZ	<i>Scale</i>	1:150	<i>Company</i>	GSG Consultants, Inc.
<i>Date</i>	11/24/2020	<i>File Name</i>	Seil Rd Culvert.slmd		



Material Name	Color	Unit Weight (lbs/ft3)	Strength Type	Cohesion (psf)	Phi (deg)
Silty Clay Fill - 1 - D		125	Mohr-Coulomb	50	25
Silty Clay Fill - 2 - D		130	Mohr-Coulomb	100	25
Silty Clay Fill - 3 - D		136	Mohr-Coulomb	250	26
Gray Silty Clay - D		136	Mohr-Coulomb	200	26

**GSG CONSULTANTS, INC.**  
 623 Cooper Court • Schaumburg, IL 60173  
 Tel: 630.994.2600 • Fax: 312.733.5612  
[www.gsg-consultants.com](http://www.gsg-consultants.com)

<i>Project</i>			
Soil Road Culvert Excavation			
<i>Analysis Description</i>			
Exhibit 1d - Circular Failure Long Term - Drained			
<i>Drawn By</i>	MZ	<i>Scale</i>	1:150
<i>Date</i>	11/24/2020	<i>Company</i>	GSG Consultants, Inc.
		<i>File Name</i>	Seil Rd Culvert.slmd

## **Attachment E**

**I-55 at IL 59\_Culvert SGR by Himalayan Consultants**

# STRUCTURE GEOTECHNICAL REPORT

Box Culvert Extensions  
at  
Seil Road-West of IL 59  
and  
IL 59-South of Seil Road  
I-55 and IL 59 Interchange Improvements  
Will County, Illinois

*Prepared For:*

Illinois Department of Transportation District One  
201 West Center Court  
Schaumburg, IL 60196

*Prepared By:*



Himalayan Consultants, LLC  
8770 W. Bryn Mawr Ave, Suite 1300  
Chicago, IL 60631  
Phone: 773-867-2956

Original Date: 11/28/2018

Revised Date: 12/26/2018

# TABLE OF CONTENTS

<b>1.0</b>	<b>EXECUTIVE SUMMARY .....</b>	<b>1</b>
<b>2.0</b>	<b>INTRODUCTION .....</b>	<b>2</b>
<b>3.0</b>	<b>PROJECT DESCRIPTION.....</b>	<b>2</b>
3.1	Culvert Extension at Seil Road.....	2
3.2	Culvert Extension at IL 59 .....	2
<b>4.0</b>	<b>SUBSURFACE INVESTIGATION AND TESTING .....</b>	<b>3</b>
4.1	Field Investigation .....	3
4.2	Laboratory Testing .....	4
<b>5.0</b>	<b>INVESTIGATION RESULTS .....</b>	<b>4</b>
5.1	Soil Conditions .....	4
5.1.1	Culvert Extension at Seil Road.....	4
5.1.2	Culvert Extension at IL 59 .....	5
5.2	Groundwater Conditions .....	5
<b>6.0</b>	<b>FOUNDATION ANALYSIS AND RECOMMENDATIONS.....</b>	<b>6</b>
6.1	Erosion Considerations.....	6
6.2	Bearing Resistance .....	6
6.2.1	Culvert Extension at Seil Road.....	6
6.2.2	Culvert Extension at IL 59 .....	6
6.3	Settlement .....	7
6.4	Downstream Retaining Wall .....	7
6.5	Wingwalls.....	7
6.5.1	Bearing Resistance .....	8
6.5.2	Settlement.....	8
6.5.3	Lateral Earth Pressure.....	8
6.5.4	Cast-In-Place or Precast Considerations .....	8
<b>7.0</b>	<b>CONSTRUCTION CONSIDERATIONS.....</b>	<b>9</b>

7.1	Site Preparation .....	9
7.2	Excavation, Dewatering, and Utilities.....	9
7.3	Filling and Backfilling.....	9
7.4	Earthwork Operations.....	9
<b>8.0</b>	<b>LIMITATIONS.....</b>	<b>10</b>
<b>9.0</b>	<b>REFERENCES.....</b>	<b>11</b>

**APPENDICES**

**Appendix A Exhibits**

- Exhibit 1: Site Location Map
- Exhibit 2: Site and Regional Geological Map
- Exhibit 3: Boring Location Plan

**Appendix B Boring Logs and Soil Profile**

- Exhibit 4: Soil Profile

**Appendix C Laboratory Test Results**

**Appendix D Preliminary Design Drawings**

## ACRONYMS, ABBREVIATIONS, AND SYMBOLS

AASHTO	American Association of State Highway Transportation Officials
ASTM	American Society of Testing Materials
bgs	Below ground surface
bpf	Blows per foot
$c_u$	Undrained Cohesion
IDOT	Illinois Department of Transportation
IDH	Illinois Division of Highways
ksi	Kips per square inch
$N_{60}$	Blow counts corrected for hammer efficiency
$N_{160}$	Blow counts corrected for hammer efficiency and overburden effects
NCDC	National Climatic Data Center
PVC	Polyvinyl Chloride
psi	Pounds per square inch
pci	Pounds per cubic inch
psf	Pounds per square foot
tsf	Tons per square foot
$Q_u$	Unconfined compressive strength
RCBC	Reinforced Concrete Box Culvert
RCP	Reinforced Concrete Pipe
SPT	Standard Penetration Test
$\phi$	Angle of internal friction
$\gamma$	Moist soil unit weight
$\mu$	Coefficient of friction
$\epsilon_{50}$	Strain at one half the maximum principal stress difference
$k_s$	Soil modulus of elastic loading
$k_c$	Soil modulus of cyclic loading
$K_a$	Active earth pressure coefficient
$K_p$	Passive earth pressure coefficient
$K_o$	At-rest earth pressure coefficient
LRFD	Load and Resistance Factor design

## 1.0 EXECUTIVE SUMMARY

This report presents the findings and recommendations of a geotechnical investigation conducted in connection with the design and extension of two existing box culvert structures proposed at the existing Illinois Route 59 and Seil Road, in Will County, Illinois.

The existing culvert at Seil Road (Culvert SN 099-0022) is a 5 feet x 3 feet double barrel reinforced concrete box culvert (RCBC) structure which will be extended by approximately 20 and 30 feet in the upstream and downstream sections, respectively. The existing culvert at IL 59 (Culvert SN 099-0351) consists of a 5 feet x 3 feet double barrel RCBC which will be extended by approximately 28 and 170 feet in the upstream and downstream sections, respectively.

The soils encountered in borings CB-01 and CB-02 advanced for the proposed box culvert extension at Seil Road are fill materials consisting of very stiff to hard, brown and gray silty clay with trace gravel ( $Q_u = 2.1$  to  $6.2$  tsf) and are underlain by hard silty clay ( $Q_u = 4.9$  to  $8.0$  tsf.) to the boring completion depths (approximate elevations 583 to 581 feet). The soils encountered in borings CB-03 and CB-04 advanced for the box culvert extension at IL 59 Road are fill materials consisting of very stiff to hard, brown and gray silty clay with trace gravel ( $Q_u = 2.5$  to  $> 4.5$  tsf). The fill materials are underlain by very stiff to hard silty clay ( $Q_u = 2.1$  to  $5.7$  tsf.) to the boring completion depths (approximate elevations 581 to 577 feet). In CB-04 a saturated layer of loose, brown and gray sand ( $N$  value = 9) was encountered at 5.5 to 8 feet below existing grades between elevations 586.5 to 584 feet.

For culvert extension at IL 59, the contractor should expect up to 2.5 feet thick layer of saturated loose sand at approximately 1 foot below the inlet invert elevation. The loose sand should be removed and replaced with coarse aggregates as indicated in Section 6.2 of this report. After removal and replacement of unsuitable soils encountered in culvert extension at IL 59, the foundation soils at or near invert elevations for both culvert extensions are estimated to have a factored bearing resistance of 6,000 psf for strength limit state (value based on a geotechnical resistance factor of 0.45 per AASHTO LRFD Table 10.5.5.2.2-1) and a bearing resistance of 3,700 psf for service limit state (value based on 1-inch settlement). The actual extent of removal should be verified during construction.

Groundwater seepage should be anticipated during construction. In view of the foundation soils that generally consist of very stiff to hard silty clay along the major part of the culvert extension and the anticipated removal/replacement of unsuitable soils, the differential settlement of the foundation soils along the proposed culvert alignment is estimated to be 0.5 inches or less.

A factored bearing resistance of 7,000 psf for strength limit state (value based on a geotechnical resistance factor of 0.55 per AASHTO LRFD Table 11.5.7.1)) and a bearing resistance of 4,000 psf for service limit state (value based on 1-inch settlement) can be used for design of spread footings for T-type wingwalls bearing on very stiff to hard clays located approximately 4 feet below the proposed culvert invert elevations.



## **2.0 INTRODUCTION**

This report provides the results of a subsurface investigation, field and laboratory testing, geotechnical analyses and recommendations conducted in connection with the design and extension of two box culvert structures proposed at the existing Illinois Route 59 and Seil Road, in Will County, Illinois (hereafter referred to as Project Site). The Project Site is located in the Village of Shorewood, northwestern portion of Will County. See Exhibit 1 in Appendix A for general location of the Project Site.

The purpose of this investigation was to characterize the site soil and groundwater conditions, perform geotechnical analyses, and provide recommendations for the design and extension of the proposed culvert structures. It is understood that the project is currently still in Phase I and the proposed structure information is preliminary. The TSL plans will be prepared as part of the Phase II design.

## **3.0 PROJECT DESCRIPTION**

### **3.1 Culvert Extension at Seil Road**

Based on the preliminary design drawings provided by IDOT dated November 10 2018, the existing structure (Culvert SN 099-0022) consists of a 5 feet x 3 feet double barrel RCBC. The existing RCBC will be extended by approximately 20 feet and 30 feet in the upstream and downstream sections, respectively. The culvert will also have concrete wingwalls that are anticipated to sit at a 45-degree angle (Wingwall Length: To be determined).

The inlet and outlet invert elevations of the proposed RCBC extension are approximately 586.0 feet and 585.8 feet, respectively.

### **3.2 Culvert Extension at IL 59**

The existing culvert (Culvert SN 099-0351) consists of a 5 feet x 3 feet double barrel RCBC. The existing RCBC will be extended by approximately 28 feet in the upstream section and by approximately 170 feet in the downstream section. The extended portion will connect to the existing culvert at an 90 degree angle. The culvert will also have concrete wingwalls that are anticipated to sit at a 45-degree angle (Wingwall Length: To be determined).

The inlet and outlet invert elevations of the proposed RCBC extension are approximately 587.5 feet and 586.43, respectively. The invert elevation at the intermediate location just past the IL 59 SB ramp is 587.50 feet.

## 4.0 SUBSURFACE INVESTIGATION AND TESTING

### 4.1 Field Investigation

From September 25 to 28, 2018, Wang Engineering, Inc. (Wang), advanced 4 borings designated as CB-01 to CB-04 at the Project Site. The borings were drilled by Wang at the location provided by IDOT and the Phase I designer.

Borings CB-01 and CB-02 were located near the downstream and upstream locations of the proposed culvert extension at Seil Road west of IL 59, respectively. Similarly, borings CB-03 and CB-04 were located near the downstream and upstream locations of the proposed culvert structure at IL 59 South of Seil Road, respectively. The borings were advanced from existing ground to boring termination depths which ranged from about 10 to 15 feet below existing grades (approximate elevations 583 to 577 feet). The borings were advanced from elevations of approximately 593 feet to 591 feet.

Borings CB-01, CB-02 and CB-04 were advanced with a rotary drilling rig in accordance with the specifications for the Standard Penetration Test (SPT) AASHTO T206. Soil sampling was performed at 2.5-foot interval from ground surface to the termination depths of the borings. Blow counts were recorded at 6-inch intervals and are shown on the boring logs. The number of blows required to advance the sampler the last 12 inches is termed the Standard Penetration Resistance (N). The N value is an indication of the consistency and relative density of soils.

Boring CB-03 was advanced using hand auger. The soil was continuously sampled with an LB-sized Geoprobe in 2-foot intervals. Soil samples collected from each sampling interval were placed in sealed jars and transported to the Wang laboratory for further examination and laboratory testing.

Himalayan supervised the drilling and sampling activities, conducted field-testing of soil samples and prepared field logs describing the soils. The split-spoon samples obtained from the drilling operation were visually classified in the field. Cohesive samples were tested for unconfined compressive strength ( $Q_u$ ) using an IDOT modified RIMAC test device and/or calibrated hand penetrometer in the field.

Wang provided the as-drilled northing and easting coordinates and boring elevations including the stationing and offsets for borings. The as-drilled boring locations are shown in the Boring Location Plan (Exhibit 3, Appendix A) and boring location data are presented in the Boring Logs (Appendix B).

Groundwater levels were measured while drilling and at completion of each boring. Upon completion of sampling and water level observations, all boreholes were properly backfilled with soil cuttings

and/or bentonite chips for safety considerations. The ground surface was restored to its original condition.

## **4.2 Laboratory Testing**

Soil samples were tested in accordance with IDOT procedures outlined in the IDOT Geotechnical Manual [Ref. 1]. The split-spoon samples obtained from the drilling operation were visually classified in the field. The acquired soil samples were then tested in the Wang laboratory for determination of natural water content (AASHTO T265). The Atterberg Limits (AASHTO T89 and T90) and Particle Size Analyses (AASHTO T88) were performed on selected samples.

Each sample was examined and classified by Himalayan in accordance with the Illinois Division of Highways (IDH) Textural Classification System. See Appendices B and C for laboratory test results.

## **5.0 INVESTIGATION RESULTS**

A more detailed description of soil and groundwater conditions encountered at each boring location is included within the Boring Logs (Appendix B). See Exhibit 4 (Appendix B) for soil profile. It should be noted that the soil stratification lines shown in the boring logs represent approximate boundaries between soil types. The actual transition between soil types in the field may be gradual in horizontal and vertical directions.

### **5.1 Soil Conditions**

#### **5.1.1 Culvert Extension at Seil Road**

The borings CB-01 and CB-02 drilled west of IL 59 near the downstream and upstream of proposed culvert extension encountered grass, bushes and weeds at the surface. Topsoil (5-8 inches) was encountered in borings. The general soils encountered beneath the topsoil include 1) Fill Materials (Man-made ground) and 2) Native Materials consisting of silty clay

#### Fill Materials

Beneath the ground, fill materials were present to depths ranging from 5.5 to 7.5 feet. Fill soils generally consisted of very stiff to hard, brown and gray silty clay with trace gravel. The unconfined compressive strength ( $Q_u$ ) for the soil samples ranged from 2.1 to 6.2 tsf and the natural water contents of these soils ranged from 15 to 22 %. Laboratory testing on samples from this layer shows liquid limit (LL) ranging from 39 to 40% and plastic limit (PL) of 20% for both samples, with Plasticity Index (PI) values ranging from 19 to 20%. The IDH Classification for these soils is Silty Clay.

### Silty Clay

Beneath the fill, the soils transition to native materials and consist of hard silty clay to the boring completion depths (approximate elevations 583 to 581 feet). The  $Q_u$  values for soil samples ranged between 4.9 to 8.0 tsf. The natural water contents for the samples ranged from 18 to 20%.

#### **5.1.2 Culvert Extension at IL 59**

The borings CB-03 and CB-04 drilled south of Seil Road near the downstream and upstream of proposed culvert encountered grass, bushes and weeds at the surface. Topsoil (8 inches) was encountered in borings. The general soils encountered beneath the topsoil include 1) Fill Materials (Man-made ground) and Native Materials consisting of 1) Silty clay and 2) Sand.

### Fill Materials

Beneath the ground, fill materials were encountered to depths ranging from 2 to 3 feet. Fill soils generally consisted of very stiff to hard, brown and gray silty clay with trace gravel. The  $Q_u$  values for the soils ranged from 2.5 to >4.5 tsf. The natural water contents of these soils ranged from 16 to 19%. Laboratory testing on samples from this layer shows a LL value of 39% and PL value of 21% (PI = 18%). The IDH Classification for these soils is Silty Clay.

### Silty Clay

Beneath the fill, the soils transition to native materials and consist of hard silty clay to the boring completion depths (approximate elevations 577 to 581 feet). The  $Q_u$  values for soil samples ranged between 2.1 to 5.7 tsf. The natural water contents for the samples ranged from 15 to 22%. Laboratory testing on samples from this layer shows a LL value of 40% and PL value of 20% (PI = 20%). The IDH Classification for these soils is Silty Clay.

### Sand

An exception was found in boring CB-04 where a saturated layer of loose, brown and gray sand (N value = 9) was encountered at 5.5 to 8 feet below existing grades between elevations of approximately 586.5 to 584 feet. The natural water content for the sample was 22%.

## **5.2 Groundwater Conditions**

Groundwater was encountered in boring CB-04 at an elevation of approximately 586 feet. at the time of this investigation. Based on change in soil coloration from brown to gray, we estimate the design high water elevation to be at an approximate elevation of 587 feet.

Note that fluctuation in the groundwater levels should be anticipated due to the seasonal variation in precipitation, surface runoff and water levels in the drainage ditch.

## **6.0 FOUNDATION ANALYSIS AND RECOMMENDATIONS**

Himalayan has performed bearing resistance, settlement, and global stability analysis for the new culvert extensions. The results of our geotechnical analysis and recommendations are provided in the following sections:

### **6.1 Erosion Considerations**

Based on the boring logs, the soils encountered at streambed elevation (approximately 587 feet), consist of very stiff to hard silty clays. Although these soils are relatively resistant to erosion, we recommend placing stone riprap or a concrete apron at the ends of the culvert to prevent local erosion on a long term basis, This will also prevent sediments from entering and accumulating in the culvert, minimize long term maintenance, and provide protection to the stream bed at the interface.

### **6.2 Bearing Resistance**

#### **6.2.1 Culvert Extension at Seil Road**

The subsurface investigation indicates the subsurface soils at and within 3 to 5 feet of the inlet and outlet invert elevations (586.05 and 585.82 feet) are primarily very stiff to hard silty clays. Based on these soil conditions, the foundation soils at invert elevations are estimated to have a factored bearing resistance of 6,000 psf for strength limit state (value based on a geotechnical resistance factor of 0.45 per AASHTO LRFD Table 10.5.5.2.2-1) and a bearing resistance of 3,700 psf for service limit state (value based on 1-inch settlement).

The foundation soils are anticipated to provide a stable working platform for the placement of the culvert extensions.

#### **6.2.2 Culvert Extension at IL 59**

Based on the investigation results, the subsurface soils at and within 4 feet of the new culvert invert elevations (586.43 to 587.5 feet) are primarily very stiff to hard silty clays. However, it should be noted that a saturated layer of loose sand, approximately 2.5 feet thick was encountered at about 1 foot below the inlet invert elevation in boring CB-04. If these soils are encountered during construction, they should be undercut/removed to reach suitable bearing soils below (very stiff silty clays) and replaced with coarse aggregates meeting the gradation requirements of CA-1, CA-7, CA-11 as defined in Section 1004 of IDOT Standard Specifications for Road and Bridge Construction (Standard

Specifications) [Ref. 5]. Replacement material should extend a minimum of 2.0 feet beyond each side of the box. The actual extent of removal and replacement should be verified during construction.

After the recommended removal and replacement, the foundation soils will provide a stable working platform and sufficient bearing resistance for the placement of the culvert extension.

### **6.3 Settlement**

Considering the foundation soils that consist of very stiff to hard silty clays and the anticipated removal/replacement of unsuitable soils as described in Section 6.2.2, the differential settlement of the foundation soils along the new culvert extensions is anticipated to be 0.5 inches or less. We estimate the settlement is suitable for the construction of the proposed culvert structure.

We estimate 1 to 2 feet of new fill on top of the culvert extensions and 4 to 5 feet of new fill around the culvert extensions.

### **6.4 Downstream Retaining Wall**

A retaining wall is proposed near the downstream end of the box culvert extension at Seil Road to retain a portion of the south side of the roadway embankment. The global stability analysis of the retaining wall should be performed as part of the retaining wall design analysis.

### **6.5 Wingwalls**

Horizontal cantilever wingwalls should be used if the wingwalls are less than or equal to 16 feet in length and the wingwall locations can be adequately dewatered [Ref. 3]. Horizontal cantilever wingwalls should be designed based on the structural guideline provided in Section 4.2 of the IDOT Culvert Manual [Ref. 3].

The L-type cantilever wingwalls may be used for longer wall lengths ranging 14 to 30 feet. The wingwalls for these walls should be founded at a minimum depth of 3.0 feet below the culvert invert elevations.

It is anticipated that T-type cantilever concrete retaining walls may be considered for the proposed culvert extensions. These walls will be bearing on soils. The bottom of the footing for these walls is set below the frost penetration depth, which is generally 4 feet below the top of finished grade. The following sections provide recommendation for design of these wingwalls:

### **6.5.1 Bearing Resistance**

A factored bearing resistance of 7,000 psf for strength limit state (value based on a geotechnical resistance factor of 0.55 per AASHTO LRFD Table 11.5.7.1)) and a bearing resistance of 4,000 psf for service limit state (value based on 1-inch settlement) can be used for design of spread footings for T-type wingwalls bearing on very stiff to hard clays.

### **6.5.2 Settlement**

Considering the very stiff to hard clays present below the anticipated footing bases for the wingwalls, the total post-construction settlement and total differential settlement are not expected to exceed 1 inch and 0.5 inch, respectively. We estimate the settlement is suitable for construction of the anticipated T-type wingwalls.

### **6.5.3 Lateral Earth Pressure**

For yielding wingwalls with horizontal backfill, it is recommended that a lateral active earth pressure of 40 psf per foot of depth (equivalent fluid pressure) be used (assuming a free-draining granular backfill is utilized). For yielding walls with a sloping surface (1V:2.5H) and free-draining granular backfill, an equivalent fluid pressure 50 psf per foot of depth may be used. An equivalent fluid pressure of 60 psf per foot should be used for soils located adjacent to the height of barrel.

In order to prevent/alleviate the buildup of potential excessive hydrostatic pressures and frost pressures, drainage behind the wall should consist of a geocomposite wall drain and porous granular backfill, consistent with Section 3.11.2.3 of the IDOT Bridge Manual. The geocomposite wall drain on the back face should be continuous [Ref. 2].

A value of 0.40 may be used for the coefficient of friction ( $\mu$ ) between the concrete base and drained cohesive soils (assuming a concrete base on the very stiff to hard cohesive soils) per NAVFAC Design Manual 7.2 [Ref. 6]. A value of 0.53 may be used for the coefficient of friction between the concrete base and granular materials CA-1, CA-7, CA-11 indicated in Section 6.2.

The final site grades should be sloped to permanently direct any collected rain water, or surface run off away from the front and back of the wall.

### **6.5.4 Cast-In-Place or Precast Considerations**

After removal and replacement of unsuitable soils encountered in culvert extension at IL 59, the differential settlements are anticipated to be about 0.5 inches for the proposed culvert extensions which should not cause excessive separation of the precast sections. Therefore, both the cast-in-place and precast culvert extension options are feasible.

## **7.0 CONSTRUCTION CONSIDERATIONS**

### **7.1 Site Preparation**

Vegetation, surface topsoil, existing pavement and debris should be cleared and stripped where the new culvert barrels and wingwalls will be constructed. The site should be prepared in accordance with the requirements of the IDOT Standard Specifications. Any unstable or unsuitable materials should be removed and replaced with compacted fill as described in Section 7.3.

### **7.2 Excavation, Dewatering, and Utilities**

The foundation excavations should be performed in accordance with local, state and federal regulations. If excavations are  $\geq 4$  feet, the slopes should be graded, benched and shielded in accordance with the latest Occupational Safety and Health Administration (OSHA) safety standards and requirements for temporary side slopes. Allowances should be made for any surcharge loads adjacent to the excavation areas. Movement of adjacent soils near the edge of and into excavation areas should be prevented and the potential effects of ground movements upon nearby utilities should be considered during construction.

Based on the upstream boring CB-04 advanced as part of culvert extension at IL 59 South of Seil Road, the contractor should expect a 2.5 feet thick saturated layer of loose sand sandwiched between very stiff and hard silty clays (approximate elevations 586.5 to 584 feet). Groundwater seepage should be anticipated during construction.

In general, we expect that groundwater seepage into the excavations within mostly cohesive soils could be controlled with sump pump and pit procedures. However, where excavations penetrate to water bearing granular soils and adjacent to lower lying wetland areas more extensive dewatering should be anticipated.

### **7.3 Filling and Backfilling**

The fill material should be free of organic matter and debris and should be compacted in accordance with the requirements of Section 205 of the IDOT Standard Specifications. The structural fill utilized to attain the final design elevations should satisfy the requirements of the IDOT Standard Specifications. The backfill materials must be as per the IDOT Standard Specifications.

### **7.4 Earthwork Operations**

The required earthwork can be accomplished with conventional equipment. Moisture and traffic will cause deterioration of exposed subgrade soils. The construction contractor should take measures to



prevent erosion of the exposed subgrade due to water or surface runoff. A compacted subgrade will minimize water runoff erosion.

Earth moving operations should be scheduled to not coincide with excessive cold or wet weather (early spring, late fall or winter). Any soil allowed to freeze or soften due to standing water should be removed. Wet weather can cause problems with subgrade compaction. It is recommended that an experienced geotechnical engineer or representative be retained to inspect the exposed subgrade, verify soils in the field, monitor earthwork operations, and provide material inspection services during construction phase of the project.

## 8.0 LIMITATIONS

Our analysis and recommendations are based upon the data obtained from the borings drilled at locations shown on the boring logs and boring location plan included in this report. Because the evaluation is based upon subsurface physical data obtained from soil borings only at specific locations and time and only to the depths sampled, the report does not reflect potential variations in the subsurface conditions that may occur between the borings or elsewhere on the site, variations whose nature and extent may not become evident until the course of construction.

The conclusions or recommendations contained represent our professional opinions. No warranty or guarantee is expressed or implied. If variations are encountered and/or the project scope is altered, we should be timely informed so that our recommendations can be adjusted accordingly.


It has been a pleasure to assist Illinois Department of Transportation on this project. Please contact us if there are any questions, or if we can be of further service.

Respectfully Submitted,


**Himalayan Consultants, LLC**



Shardul Sharma  
Geotechnical Engineer



Gopal K. Adhikary  
Senior Geotechnical Engineer



Mark A. Babich, P.E.  
QA/QC Reviewer

## **9.0 REFERENCES**

1. Illinois Department of Transportation (2015). Geotechnical Manual.
2. Illinois Department of Transportation (2012). Bridge Manual.
3. Illinois Department of Transportation (2017). Culvert Manual.
4. AASHTO LRFD Bridge Design Specifications (2016). Section 11-Walls, Abutments and Piers.
5. Illinois Department of Transportation (2016). Standard Specifications for Road and Bridge Construction.
6. United States Navy Naval Facilities Engineering Command (1986). Foundations and Structures.

## **APPENDICES**

### **Appendix A Exhibits**

- Exhibit 1: Site Location Map
- Exhibit 2: Boring Location Plan

### **Appendix B Boring Logs and Soil Profile**

- Exhibit 4: Soil Profile

### **Appendix C Laboratory Test Results**

### **Appendix D Preliminary Design Drawings**

# **APPENDIX A**

## **EXHIBITS**

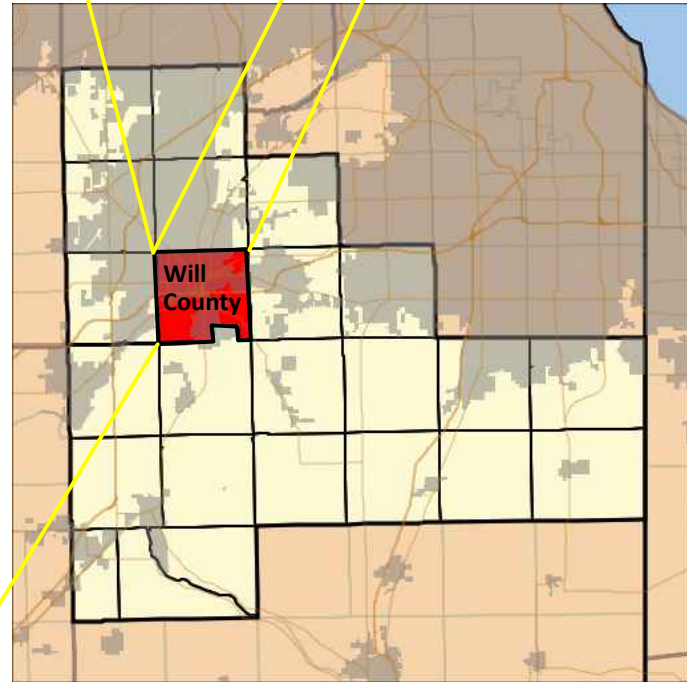
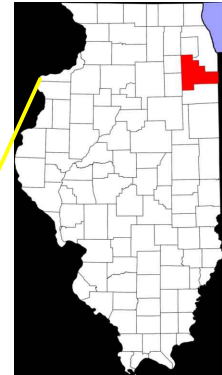
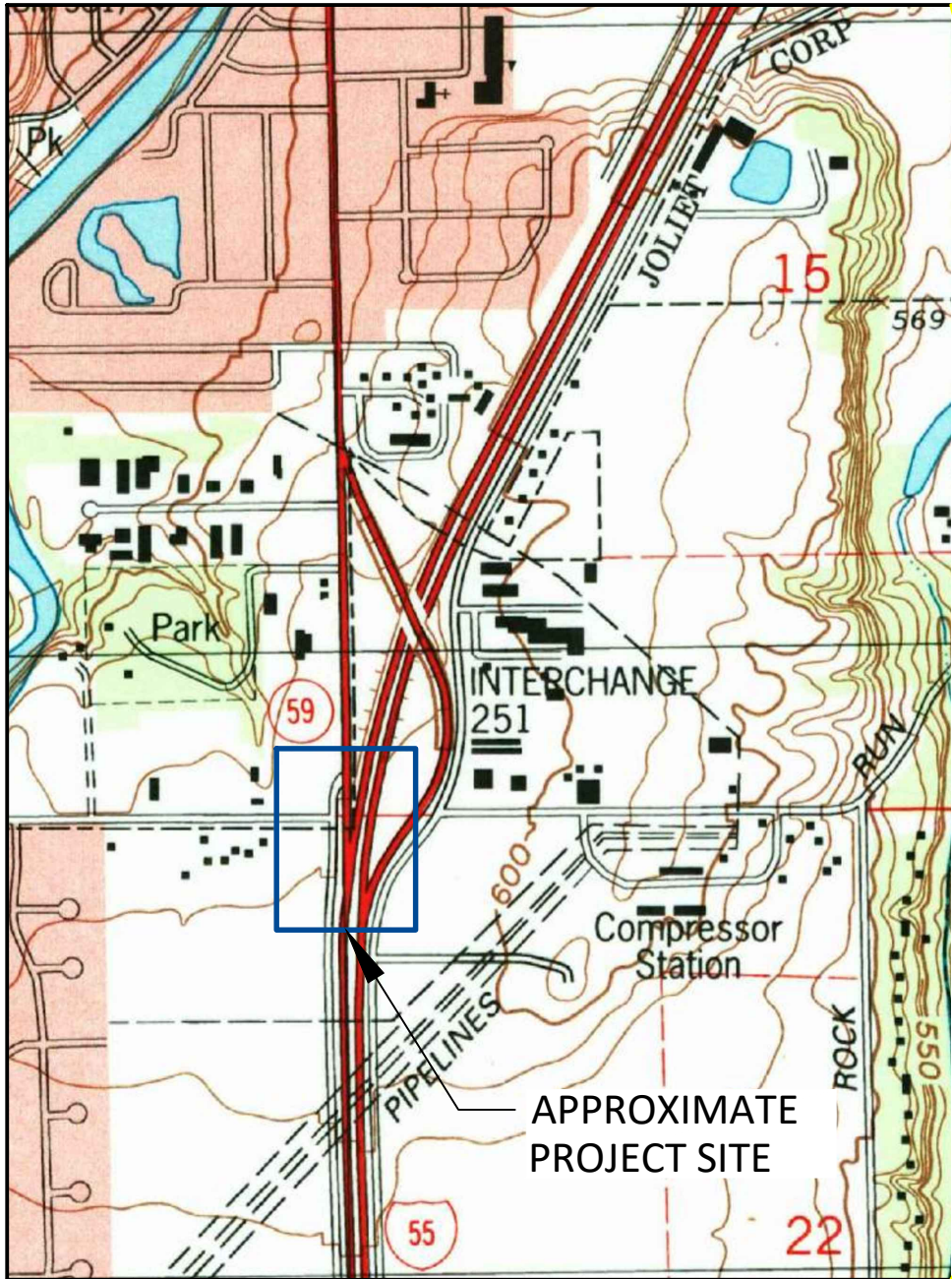



Exhibit  
**1**

**Project Location Map**  
 Box Culvert at Seil Road West of IL 59 and IL 59 South of Seil Road  
 I-55 at IL 59 Access Project  
 Will County, Illinois

Graphic Scale  
  
 1 inch = 1000 feet  
 Topographic Map Retrieved from USGS




**Himalayan Consultants, LLC**  
 Engineers and Hydrogeologists  
 8770 W. Bryn Mawr Avenue, Suite 1300  
 Chicago, Illinois 60631  
 Phone: (773) 867-2956






Exhibit  
**2**

**Boring Location Map**  
Box Culvert at Seil Road West of IL 59 and IL 59 South of Seil Road  
I-55 at IL 59 Access Project  
Will County, Illinois

**LEGEND**  
 Boring (B-X)  
*Map Retrieved from Will County GIS*

Graphic Scale  
  
 1 inch = 100 feet


**Himalayan Consultants, LLC**  
 Engineers and Hydrogeologists  
 8770 W. Bryn Mawr Avenue, Suite 1300  
 Chicago, Illinois 60631  
 Phone: (773) 867-2956

## **APPENDIX B**

### **BORING LOGS AND SOIL PROFILE**













**LEGEND FOR BORING LOG**

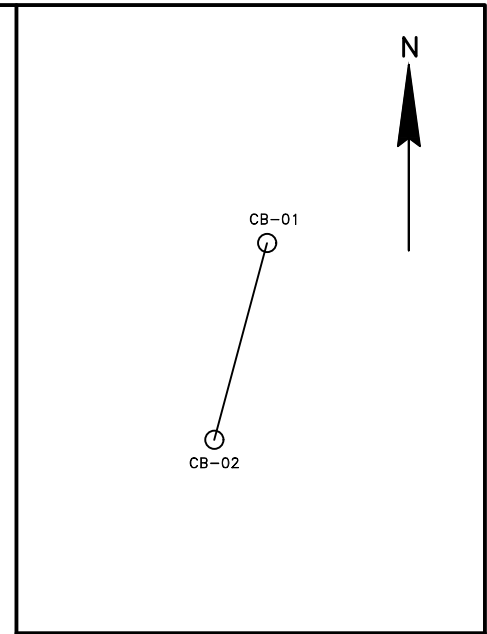
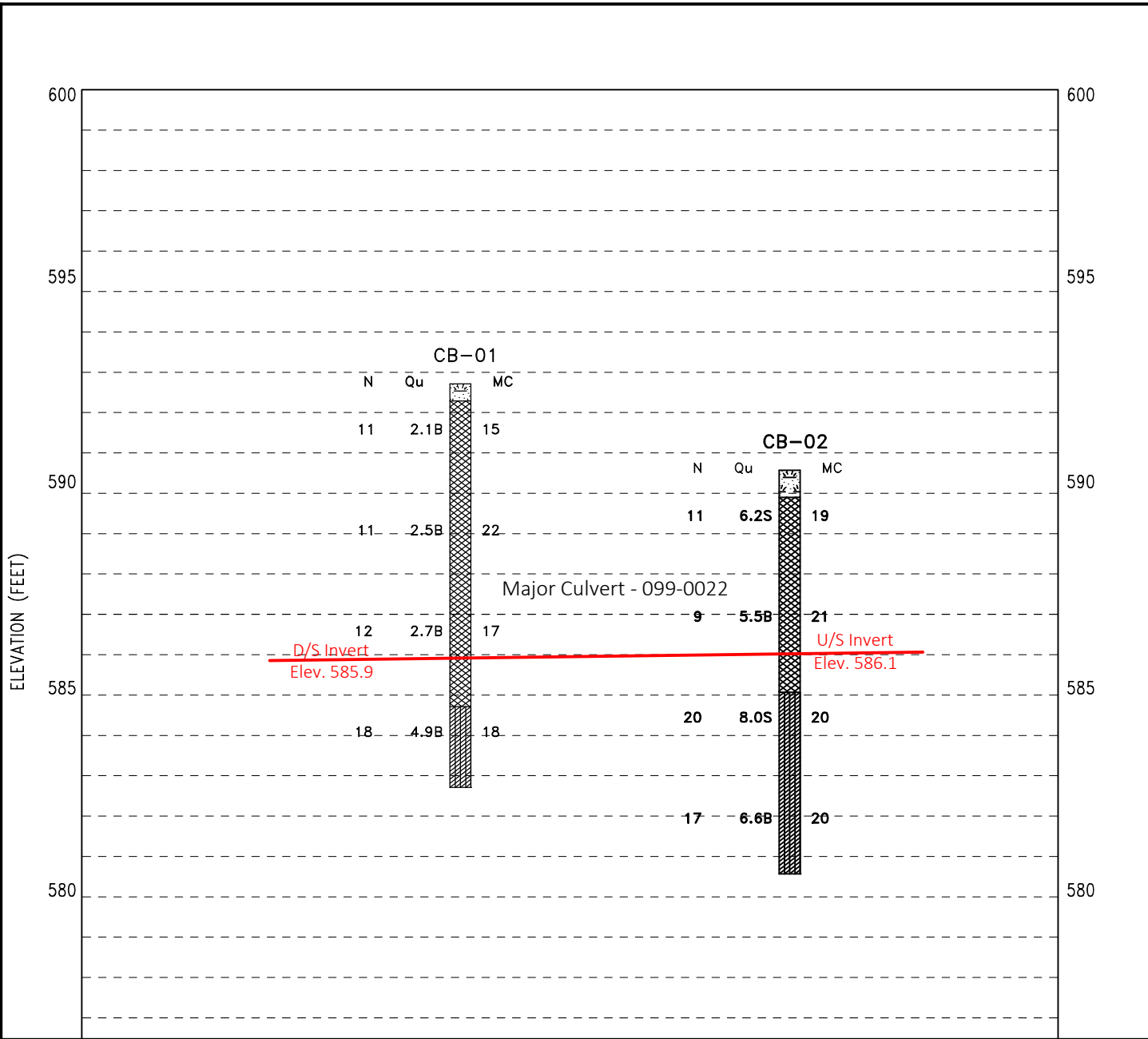
Relative Density of Non - Cohesive Soils	
N-Blows/ 12 inches	Relative Density Term
0-3	Very Loose
4-9	Loose
10-29	Medium Dense
30-49	Dense
50-80+	Very Dense

Consistency of Cohesive Soils	
Unconfined Compressive Strength Qu, tsf	Consistency Term
<0.25	Very Soft
0.25-0.49	Soft
0.50-0.99	Medium Stiff
1.00-1.99	Stiff
2.00-3.99	Very Stiff
>4.00	Hard

Relative Drilling Resistace	
RDR	Drilling Resistance Term
1	Very Easy
2	Easy
3	Moderate
4	Hard
5	Very Hard

Proportional Terms		
		Percent of Dry Weight
Trace	1-9	
Little	10-19	
Some	20-34	
And	35-50	
Gradation Terminology		
Boulders	>200mm	
Cobbles	200mm to 75mm	
Gravel	75mm to 2mm	
Sand	2-0mm to	
	0.074mm	
Silt	0.074mm to	
	0.002mm	
Clay	<0.002mm	

Drilling and Sampling Terms	
SS=	Split Spoon
ST=	Shelby Tube
SPT*=	Standard Penetration Test (N-Value)
Q <sub>u</sub> =	Unconfined Compressive Strength
P=	Pocket Penetrometer
S=	Shear failur of sample, Rimac test
B=	Bulge Failure of sample, Rimac Test
TMR =	Truck Mounted Rig
ATV =	All Terrain Vehicle Rig
[-%]	SPT Hammer Efficiency
*SPT N-Value is the sum of the second and third numbers	




### Explanation:

- CB-04 1061+64.81 — Borehole Number Station
  - Borehole Lithology
  - N—N-value, (blow/12in)
  - Qu—UC Strength, (tsf)
  - MC—Moisture Content (%)
- Lithology Graphics**
- Topsoil
  - IDH Sand, Sandy Loam
  - Fill
  - IDH Silty Clay, Silty Clay Loam

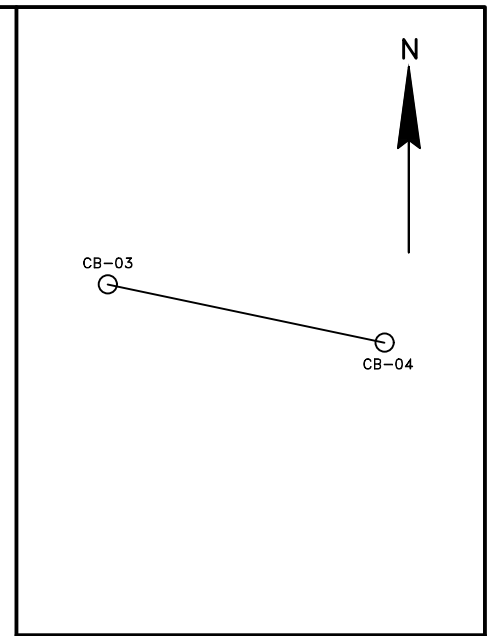
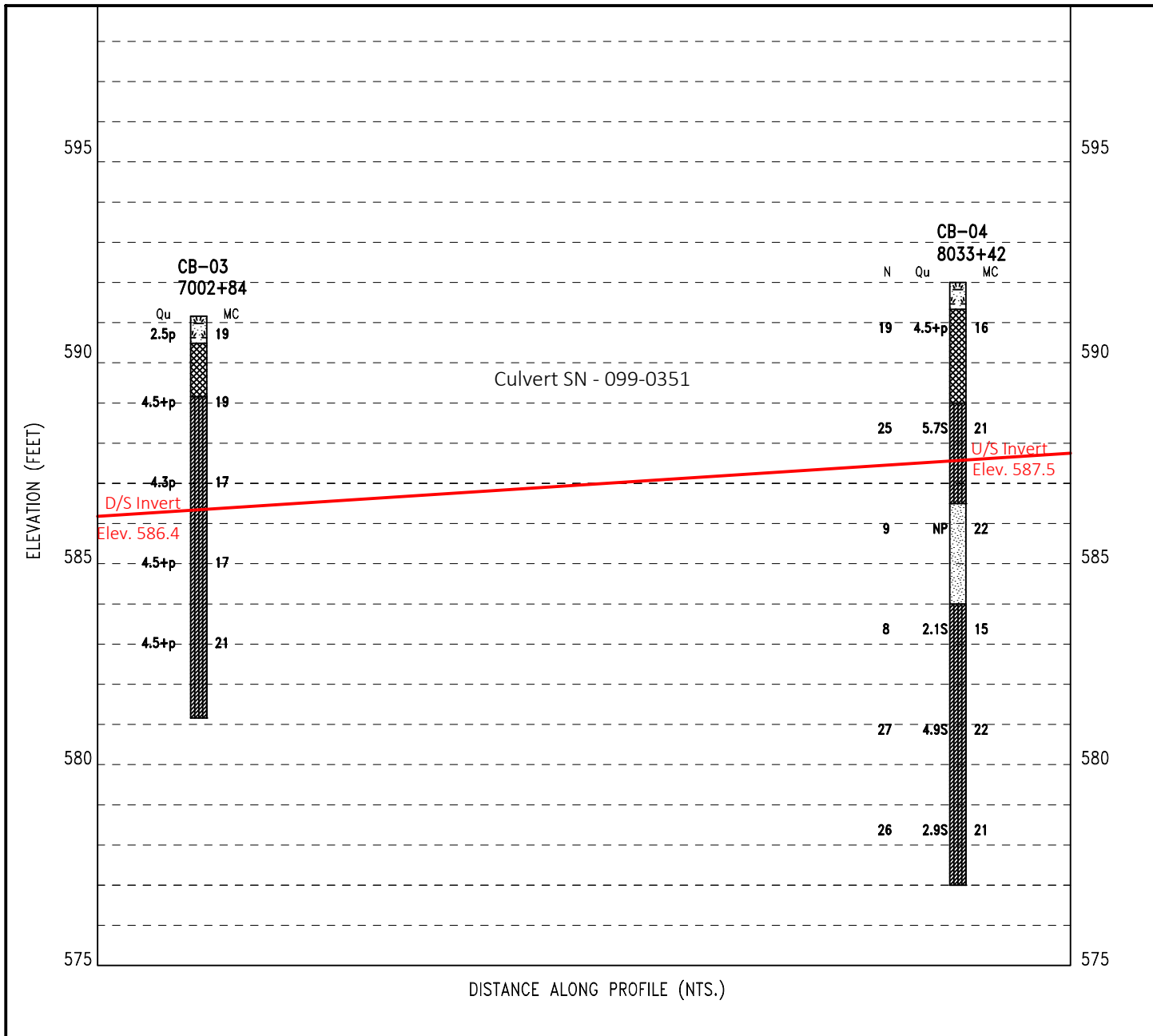
Vertical Scale  
1 in = 4 ft

Exhibit  
**3-1**

**Soil Profile**  
Box Culvert at Seil Road West of IL 59 and IL 59 South of Seil Road  
I-55 at IL 59 Access Project  
Will County, Illinois



**Himalayan Consultants, LLC**  
Engineers and Hydrogeologists  
8770 W. Bryn Mawr Avenue, Suite 1300  
Chicago, Illinois 60631  
Phone: (773) 867-2956  
Fax: (773) 867-2910



**Explanation:**

CB-04  
1061+64.81

— Borehole Number Station

— Borehole Lithology

N--N-value, (blow/12in)  
Qu--UC Strength, (tsf)  
MC--Moisture Content (%)

**Lithology Graphics**

Topsoil      IDH Sand, Sandy Loam

Fill            IDH Silty Clay, Silty Clay Loam

**Vertical Scale**  
1 in = 4 ft

Exhibit  
**3-2**

**Soil Profile**  
 Box Culvert at Seil Road West of IL 59 and IL 59 South of Seil Road  
 I-55 at IL 59 Access Project  
 Will County, Illinois



**Himalayan Consultants, LLC**  
 Engineers and Hydrogeologists  
 8770 W. Bryn Mawr Avenue, Suite 1300  
 Chicago, Illinois 60631  
 Phone: (773) 867-2956  
 Fax: (773) 867-2910

## **APPENDIX C**

### **LABORATORY TEST RESULTS**

**LIQUID LIMIT, PLASTIC LIMIT, and PLASTICITY INDEX of SOILS**  
AASHTO T 89, T 90 / ASTM D 4318

Client: IDOT  
Project: I-55 at IL-59  
WEI Job No: 555-16-04  
Prep Method: air dried

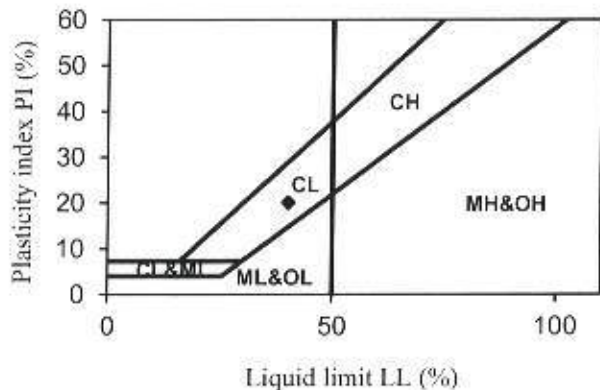
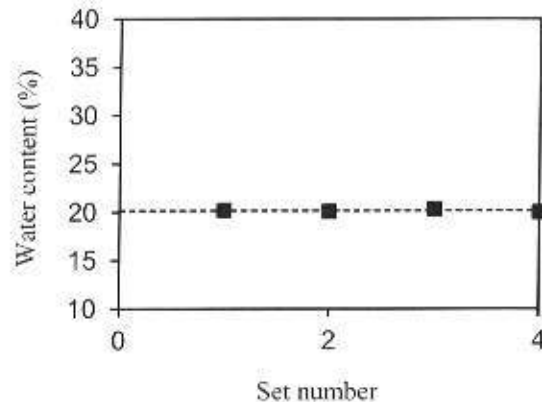
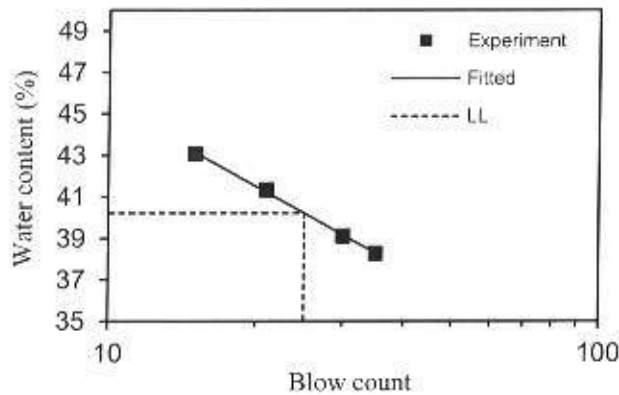
Analyst name: M. Ciapas  
Test date: October 10, 2018  
Soil Sample ID: CB-01, No. 2 (3.5-5.0 ft.)  
Sample description: Brown Silty Clay  
% retained on #40 sieve: 5%

Set #	Tare mass (g) Wc	Tare with wet soil (g) Ww	Tare with dry soil (g) Wd	Blow count N	Water content (%) w	Water content fitted (%)
1	11.31	24.64	20.95	35	38.28	38.28
2	11.23	24.00	20.41	30	39.11	39.16
3	11.32	25.27	21.19	21	41.34	41.21
4	11.11	25.36	21.07	15	43.07	43.14

Liquid limit (%) = 40.21  
Slope of flow line = 0.141

Set #	Tare mass (g) Mc	Tare with wet soil (g) Mw	Tare with dry soil (g) Md	Water content (%) w
1	11.20	23.76	21.65	20.19
2	11.70	23.48	21.51	20.08
3	11.37	23.09	21.11	20.33
4	11.09	23.21	21.19	20.00

Plastic limit (%) = 20.15



Liquid limit (%) = 40  
Plastic limit (%) = 20  
Plasticity index (%) = 20

Prepared by: Jay Date: 10.12.18  
Checked by: At Date: 10/19/18

**LIQUID LIMIT, PLASTIC LIMIT, and PLASTICITY INDEX of SOILS**  
AASHTO T 89, T 90 / ASTM D 4318

Client: IDOT  
Project: I-55 at IL-59  
WEI Job No: 555-16-04  
Prep Method: air dried

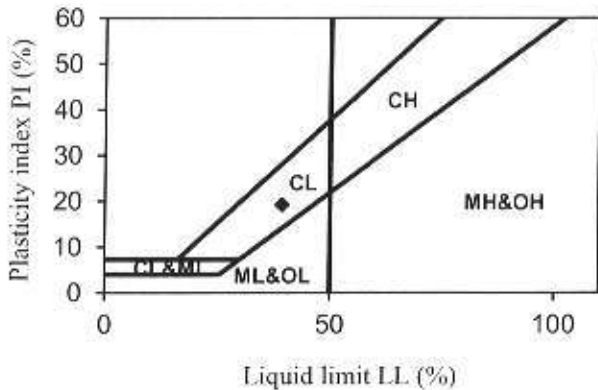
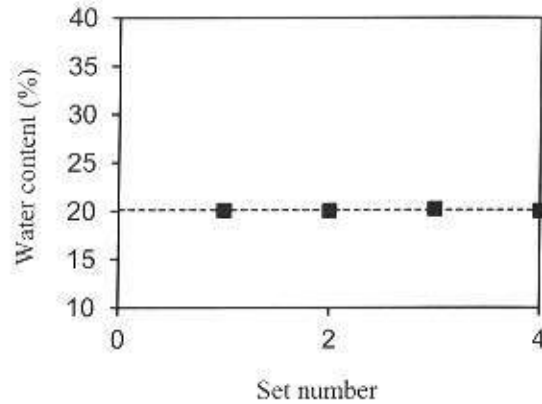
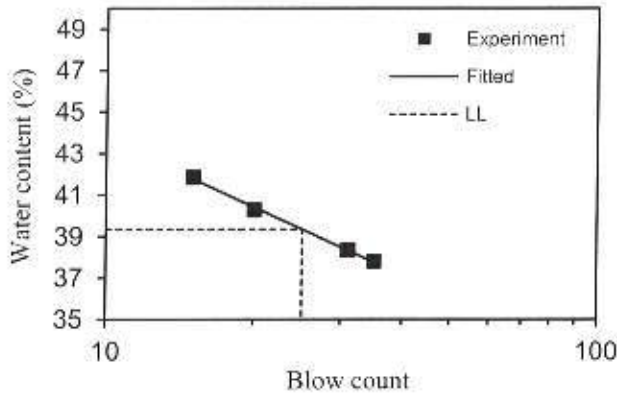
Analyst name: M. Ciapas  
Test date: October 10, 2018  
Soil Sample ID: CB-02, No. 2 (3.5-5.0 ft.)  
Sample description: Brown Silty Clay  
% retained on #40 sieve: 3%

Set #	Tare mass (g) We	Tare with wet soil (g) Ww	Tare with dry soil (g) Wd	Blow count N	Water content (%) w	Water content fitted (%)
1	11.40	26.71	22.31	35	37.80	37.76
2	11.74	24.91	21.26	31	38.34	38.34
3	11.28	25.35	21.31	20	40.28	40.41
4	11.02	25.22	21.03	15	41.86	41.77

Liquid limit (%) = 39.35  
Slope of flow line = 0.119

Set #	Tare mass (g) Me	Tare with wet soil (g) Mw	Tare with dry soil (g) Md	Water content (%) w
1	11.15	23.35	21.31	20.08
2	11.17	22.84	20.89	20.06
3	11.20	23.38	21.33	20.24
4	11.21	22.65	20.74	20.04

Plastic limit (%) = 20.10



Liquid limit (%) = 39  
Plastic limit (%) = 20  
Plasticity index (%) = 19

Prepared by: [Signature] Date: 10-12-18  
Checked by: [Signature] Date: 10/19/18







1145 North Main Street  
Lombard, Illinois 60148  
Phone (630) 953-9928  
www.wangeng.com

**LIQUID LIMIT, PLASTIC LIMIT, and PLASTICITY INDEX of SOILS**  
AASHTO T 89, T 90 / ASTM D 4318

Client: IDOT  
Project: I-55 at IL-59  
WEI Job No: 555-16-04  
Prep Method: air dried

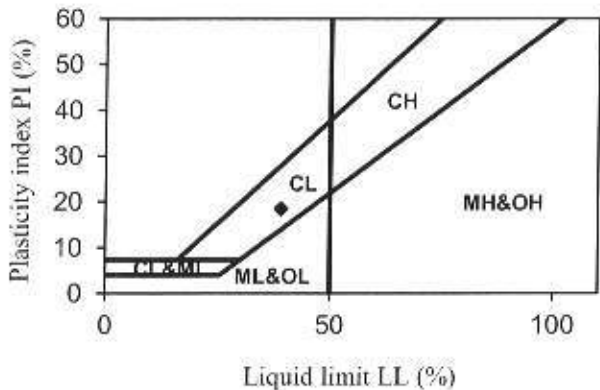
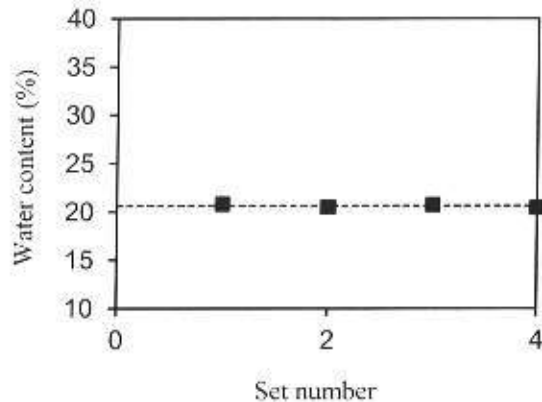
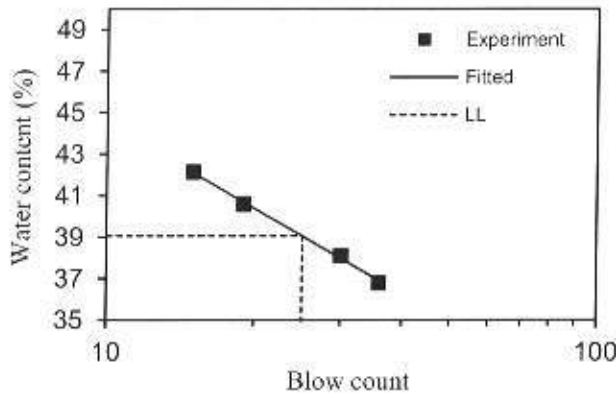
Analyst name: M. Ciapas  
Test date: October 10, 2018  
Soil Sample ID: CB-03, No. 2 (2.0-4.0 ft.)  
Sample description: Brown Silty Clay  
% retained on #40 sieve: 4%

Set #	Tare mass (g) We	Tare with wet soil (g) Ww	Tare with dry soil (g) Wd	Blow count N	Water content (%) w	Water content fitted (%)
1	11.18	24.08	20.61	36	36.80	36.89
2	11.15	24.34	20.70	30	38.12	37.97
3	11.09	25.57	21.39	19	40.58	40.68
4	11.16	24.89	20.82	15	42.13	42.09

Liquid limit (%) = 39.05  
Slope of flow line = 0.151

Set #	Tare mass (g) Mc	Tare with wet soil (g) Mw	Tare with dry soil (g) Md	Water content (%) w
1	11.17	22.85	20.84	20.79
2	11.16	22.45	20.53	20.49
3	11.33	22.63	20.69	20.73
4	11.32	23.64	21.55	20.43

Plastic limit (%) = 20.61



Liquid limit (%) = 39  
Plastic limit (%) = 21  
Plasticity index (%) = 18

Prepared by: Jay Date: 10.12.18  
Checked by: AT Date: 10/19/18



## LIQUID LIMIT, PLASTIC LIMIT, and PLASTICITY INDEX of SOILS

AASHTO T 89, T 90 / ASTM D 4318

Client: IDOT

Analyst name: M. Ciapas

Project: 1-55 at IL-59

Test date: October 10, 2018

WEI Job No: 555-16-04

Soil Sample ID: CB-04, No. 2 (3.5-5.0 ft.)

Prep Method: air dried

Sample description: Brown Silty Clay

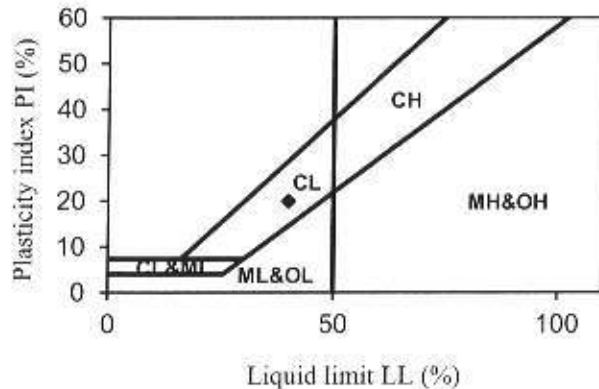
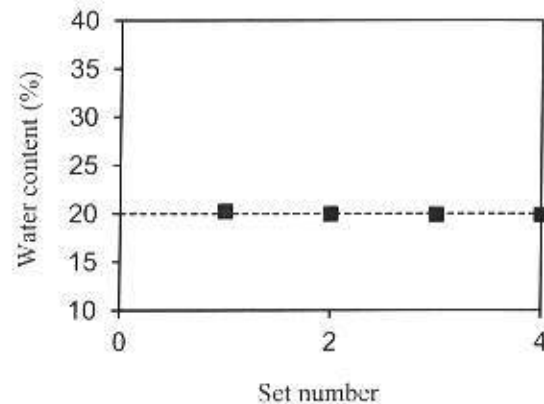
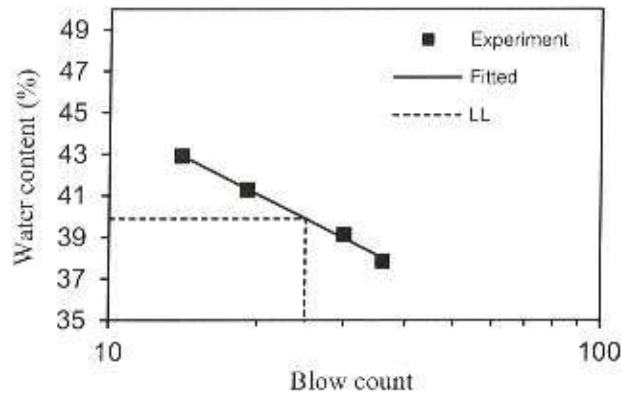
% retained on #40 sieve: 2%

Set #	Tare mass (g) We	Tare with wet soil (g) Ww	Tare with dry soil (g) Wd	Blow count N	Water content (%) w	Water content fitted (%)
1	11.17	23.99	20.47	36	37.85	37.99
2	10.97	23.06	19.66	30	39.13	38.94
3	11.23	24.30	20.48	19	41.30	41.33
4	11.15	24.77	20.68	14	42.92	42.93

Liquid limit (%) = 39.90  
Slope of flow line = 0.130

Set #	Tare mass (g) Mc	Tare with wet soil (g) Mw	Tare with dry soil (g) Md	Water content (%) w
1	11.15	22.50	20.59	20.23
2	11.18	22.65	20.74	19.98
3	11.20	24.03	21.90	19.91
4	11.19	23.14	21.16	19.86

Plastic limit (%) = 19.99



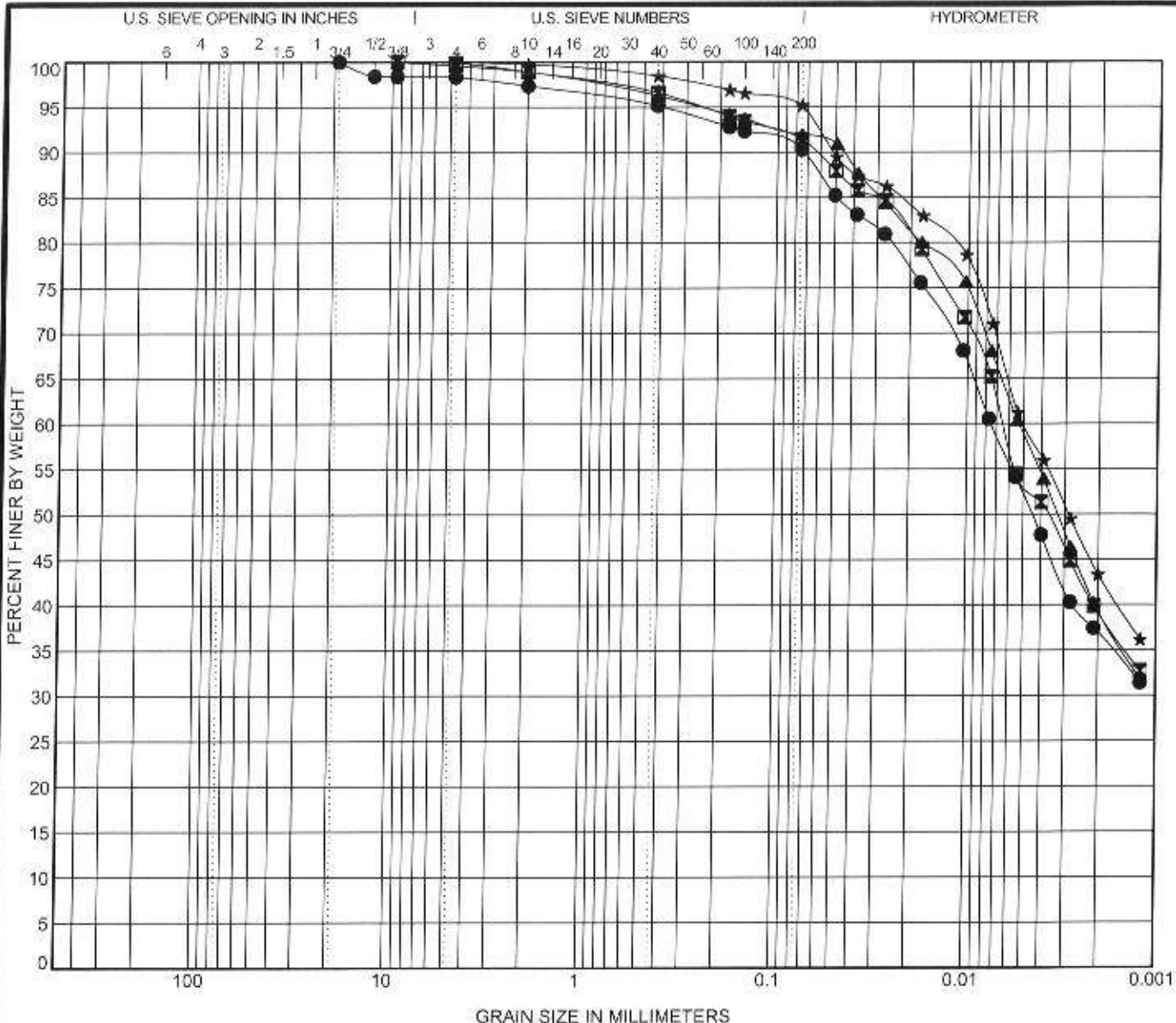
Liquid limit (%) = 40  
Plastic limit (%) = 20  
Plasticity index (%) = 20

Prepared by: Jay

Date: 10.12.18

Checked by: AF

Date: 10/19/18



COBBLES	GRAVEL	SAND		SILT AND CLAY
		coarse	fine	

Specimen Identification	IDH Classification	LL	PL	PI	Cc	Cu
● CB-01#2 3.5 ft	<b>Silty Clay</b>	40	20	20		
⊠ CB-02#2 3.5 ft	<b>Silty Clay</b>	39	20	19		
▲ CB-03#2 2.0 ft	<b>Silty Clay</b>	39	21	18		
★ CB-04#2 3.5 ft	<b>Silty Clay</b>	40	20	20		

Specimen Identification	D100	D60	D30	D10	%Gravel	%Sand	%Silt	%Clay
● CB-01#2 3.5 ft	19	0.007			2.6	7.2	53.2	36.9
⊠ CB-02#2 3.5 ft	9.5	0.006			1.1	7.6	52.1	39.2
▲ CB-03#2 2.0 ft	9.5	0.005			1.1	7.0	52.5	39.5
★ CB-04#2 3.5 ft	4.75	0.005			0.3	4.7	51.7	43.3

WEI GRAIN SIZE IDH 5051604.GPJ US LAB.GDT 10/12/18



Wang Engineering, Inc.  
 1145 North Main Street  
 Lombard, Illinois 60148  
 Telephone: 630-953-9928  
 Fax:

**GRAIN SIZE DISTRIBUTION**

Project: I-55 at IL 59  
 Location: Will County, IL  
 Number: 555-16-04

## **APPENDIX D**

### **Preliminary Design Drawings**







