

GIRDER 3E - SPANS 1 & 2

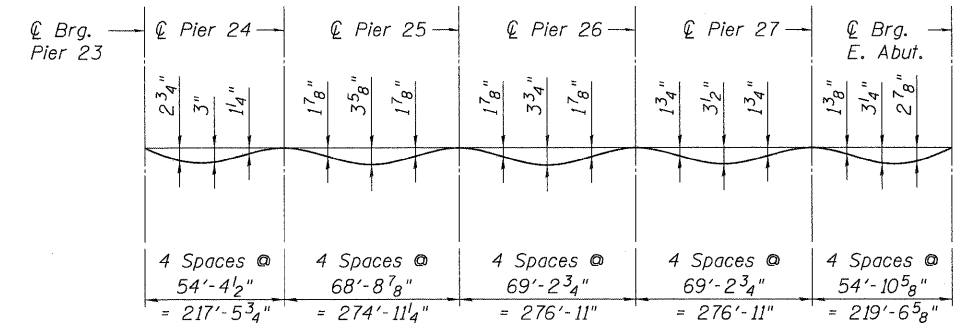
| Location  | Station   | Offset From EB I-70 P.G.L. | Theoretical Grade Elevations | Theoretical Grade Elevations Adjusted for DL Deflections |
|-----------|-----------|----------------------------|------------------------------|--|
| ☉ Brg P23 | 127+83.10 | 14.00                      | 464.94                       | 464.94   |
| AA        | 127+93.21 | 14.00                      | 464.89                       | 464.94   |
| AB        | 128+03.32 | 14.00                      | 464.84                       | 464.94   |
| AC        | 128+13.43 | 14.00                      | 464.79                       | 464.93   |
| AD        | 128+23.54 | 14.00                      | 464.74                       | 464.92   |
| AE        | 128+33.65 | 14.00                      | 464.69                       | 464.90   |
| AF        | 128+43.76 | 14.00                      | 464.64                       | 464.88   |
| AG        | 128+53.88 | 14.00                      | 464.59                       | 464.85   |
| AH        | 128+63.99 | 14.00                      | 464.54                       | 464.81   |
| AI        | 128+74.10 | 14.00                      | 464.49                       | 464.76   |
| AJ        | 128+84.21 | 14.00                      | 464.44                       | 464.70   |
| AK        | 128+94.32 | 14.00                      | 464.39                       | 464.64   |
| AL        | 129+04.43 | 14.00                      | 464.34                       | 464.57   |
| AM        | 129+14.54 | 14.00                      | 464.29                       | 464.49   |
| AN        | 129+24.66 | 14.00                      | 464.24                       | 464.41   |
| AO        | 129+34.77 | 14.00                      | 464.19                       | 464.33   |
| AP        | 129+44.88 | 14.00                      | 464.14                       | 464.25   |
| AQ        | 129+54.99 | 14.00                      | 464.08                       | 464.17   |
| AR        | 129+65.10 | 14.00                      | 464.03                       | 464.09   |
| AS        | 129+75.21 | 14.00                      | 463.98                       | 464.02   |
| AT        | 129+85.32 | 14.00                      | 463.93                       | 463.95   |
| AU        | 129+95.43 | 14.00                      | 463.88                       | 463.89   |
| ☉ Pier 24 | 130+03.00 | 14.00                      | 463.84                       | 463.84   |
| AV        | 130+13.11 | 14.00                      | 463.79                       | 463.81   |
| AW        | 130+23.22 | 14.00                      | 463.74                       | 463.77   |
| AX        | 130+33.33 | 14.00                      | 463.69                       | 463.73   |
| AY        | 130+43.45 | 14.00                      | 463.64                       | 463.71   |
| AZ        | 130+53.56 | 14.00                      | 463.59                       | 463.69   |
| BA        | 130+63.67 | 14.00                      | 463.54                       | 463.67   |
| BB        | 130+73.78 | 14.00                      | 463.49                       | 463.65   |
| BC        | 130+83.89 | 14.00                      | 463.44                       | 463.63   |
| BD        | 130+94.00 | 14.00                      | 463.39                       | 463.61   |
| BE        | 131+04.11 | 14.00                      | 463.34                       | 463.59   |
| BF        | 131+14.22 | 14.00                      | 463.29                       | 463.56   |
| BG        | 131+24.34 | 14.00                      | 463.24                       | 463.52   |
| BH        | 131+34.45 | 14.00                      | 463.19                       | 463.48   |
| BI        | 131+44.56 | 14.00                      | 463.14                       | 463.43   |
| BJ        | 131+54.67 | 14.00                      | 463.09                       | 463.37   |
| BK        | 131+64.78 | 14.00                      | 463.04                       | 463.31   |
| BL        | 131+74.89 | 14.00                      | 462.98                       | 463.24   |
| BM        | 131+85.00 | 14.00                      | 462.93                       | 463.16   |
| BN        | 131+95.12 | 14.00                      | 462.88                       | 463.09   |
| BO        | 132+05.23 | 14.00                      | 462.83                       | 463.00   |
| BP        | 132+15.34 | 14.00                      | 462.77                       | 462.91   |
| BQ        | 132+25.45 | 14.00                      | 462.71                       | 462.82   |
| BR        | 132+35.56 | 14.00                      | 462.64                       | 462.72   |
| BS        | 132+45.67 | 14.00                      | 462.57                       | 462.62   |
| BT        | 132+55.78 | 14.00                      | 462.49                       | 462.51   |
| BU        | 132+65.89 | 14.00                      | 462.40                       | 462.42   |
| BV        |           |                            |                              |  |

GIRDER 3E - SPANS 3 & 4

| Location  | Station   | Offset From EB I-70 P.G.L. | Theoretical Grade Elevations | Theoretical Grade Elevations Adjusted for DL Deflections |
|-----------|-----------|----------------------------|------------------------------|--|
| ☉ Pier 25 | 132+81.00 | 14.00                      | 462.27                       | 462.27   |
| BW        | 132+91.11 | 14.00                      | 462.17                       | 462.18   |
| BX        | 133+01.22 | 14.00                      | 462.07                       | 462.09   |
| BY        | 133+11.33 | 14.00                      | 461.96                       | 462.00   |
| BZ        | 133+21.45 | 14.00                      | 461.85                       | 461.92   |
| CA        | 133+31.56 | 14.00                      | 461.74                       | 461.83   |
| CB        | 133+41.67 | 14.00                      | 461.61                       | 461.74   |
| CC        | 133+51.78 | 14.00                      | 461.49                       | 461.65   |
| CD        | 133+61.89 | 14.00                      | 461.35                       | 461.55   |
| CE        | 133+72.00 | 14.00                      | 461.22                       | 461.44   |
| CF        | 133+82.11 | 14.00                      | 461.07                       | 461.33   |
| CG        | 133+92.22 | 14.00                      | 460.93                       | 461.21   |
| CH        | 134+02.34 | 14.00                      | 460.77                       | 461.06   |
| CI        | 134+12.45 | 14.00                      | 460.61                       | 460.92   |
| CJ        | 134+22.56 | 14.00                      | 460.45                       | 460.76   |
| CK        | 134+32.67 | 14.00                      | 460.28                       | 460.58   |
| CL        | 134+42.78 | 14.00                      | 460.11                       | 460.40   |
| CM        | 134+52.89 | 14.00                      | 459.93                       | 460.20   |
| CN        | 134+63.00 | 14.00                      | 459.75                       | 459.99   |
| CO        | 134+73.12 | 14.00                      | 459.56                       | 459.78   |
| CP        | 134+83.23 | 14.00                      | 459.37                       | 459.55   |
| CQ        | 134+93.34 | 14.00                      | 459.17                       | 459.32   |
| CR        | 135+03.45 | 14.00                      | 458.96                       | 459.08   |
| CS        | 135+13.56 | 14.00                      | 458.75                       | 458.84   |
| CT        | 135+23.67 | 14.00                      | 458.54                       | 458.60   |
| CU        | 135+33.78 | 14.00                      | 458.32                       | 458.35   |
| CV        | 135+43.89 | 14.00                      | 458.10                       | 458.12   |
| CW        | 135+54.01 | 14.00                      | 457.87                       | 457.88   |
| CX        |           |                            |                              |  |
| ☉ Pier 26 | 135+61.00 | 14.00                      | 457.71                       | 457.71   |
| CY        | 135+71.11 | 14.00                      | 457.47                       | 457.48   |
| CZ        | 135+81.22 | 14.00                      | 457.22                       | 457.24   |
| DA        | 135+91.33 | 14.00                      | 456.98                       | 457.01   |
| DB        | 136+01.45 | 14.00                      | 456.72                       | 456.78   |
| DC        | 136+11.56 | 14.00                      | 456.46                       | 456.55   |
| DD        | 136+21.67 | 14.00                      | 456.20                       | 456.32   |
| DE        | 136+31.78 | 14.00                      | 455.93                       | 456.08   |
| DF        | 136+41.89 | 14.00                      | 455.66                       | 455.84   |
| DG        | 136+52.00 | 14.00                      | 455.38                       | 455.59   |
| DH        | 136+62.11 | 14.00                      | 455.09                       | 455.33   |
| DI        | 136+72.22 | 14.00                      | 454.80                       | 455.07   |
| DJ        | 136+82.34 | 14.00                      | 454.51                       | 454.78   |
| DK        | 136+92.45 | 14.00                      | 454.21                       | 454.49   |
| DL        | 137+02.56 | 14.00                      | 453.91                       | 454.20   |
| DM        | 137+12.67 | 14.00                      | 453.60                       | 453.88   |
| DN        | 137+22.78 | 14.00                      | 453.30                       | 453.57   |
| DO        | 137+32.89 | 14.00                      | 453.00                       | 453.25   |
| DP        | 137+43.00 | 14.00                      | 452.69                       | 452.92   |
| DQ        | 137+53.12 | 14.00                      | 452.39                       | 452.59   |
| DR        | 137+63.23 | 14.00                      | 452.09                       | 452.26   |
| DS        | 137+73.34 | 14.00                      | 451.78                       | 451.92   |
| DT        | 137+83.45 | 14.00                      | 451.48                       | 451.58   |
| DU        | 137+93.56 | 14.00                      | 451.18                       | 451.25   |
| DV        | 138+03.67 | 14.00                      | 450.87                       | 450.92   |
| DW        | 138+13.78 | 14.00                      | 450.57                       | 450.59   |
| DX        | 138+23.89 | 14.00                      | 450.27                       | 450.28   |
| DY        | 138+34.01 | 14.00                      | 449.96                       | 449.97   |
| DZ        |           |                            |                              |  |

GIRDER 3E - SPAN 5

| Location   | Station   | Offset From EB I-70 P.G.L. | Theoretical Grade Elevations | Theoretical Grade Elevations Adjusted for DL Deflections |
|------------|-----------|----------------------------|------------------------------|--|
| ☉ Pier 27  | 138+41.00 | 14.00                      | 449.75                       | 449.75   |
| EA         | 138+51.11 | 14.00                      | 449.45                       | 449.46   |
| EB         | 138+61.22 | 14.00                      | 449.15                       | 449.17   |
| EC         | 138+71.33 | 14.00                      | 448.84                       | 448.89   |
| ED         | 138+81.45 | 14.00                      | 448.54                       | 448.61   |
| EE         | 138+91.56 | 14.00                      | 448.24                       | 448.34   |
| EF         | 139+01.67 | 14.00                      | 447.93                       | 448.07   |
| EG         | 139+11.78 | 14.00                      | 447.63                       | 447.80   |
| EH         | 139+21.89 | 14.00                      | 447.33                       | 447.53   |
| EI         | 139+32.00 | 14.00                      | 447.02                       | 447.25   |
| EJ         | 139+42.11 | 14.00                      | 446.72                       | 446.97   |
| EK         | 139+52.22 | 14.00                      | 446.42                       | 446.69   |
| EL         | 139+62.34 | 14.00                      | 446.11                       | 446.40   |
| EM         | 139+72.45 | 14.00                      | 445.81                       | 446.10   |
| EN         | 139+82.56 | 14.00                      | 445.51                       | 445.79   |
| EO         | 139+92.67 | 14.00                      | 445.20                       | 445.48   |
| EP         | 140+02.78 | 14.00                      | 444.90                       | 445.15   |
| EQ         | 140+12.89 | 14.00                      | 444.60                       | 444.82   |
| ER         | 140+23.00 | 14.00                      | 444.29                       | 444.48   |
| ES         | 140+33.12 | 14.00                      | 443.99                       | 444.14   |
| ET         | 140+43.23 | 14.00                      | 443.69                       | 443.79   |
| EU         | 140+53.34 | 14.00                      | 443.38                       | 443.43   |
| EV         |           |                            |                              |  |
| ☉ Brg Abut | 140+63.00 | 14.00                      | 443.09                       | 443.09   |



DEAD LOAD DEFLECTION DIAGRAM - GIRDER 3E

(Includes weight of concrete only.)

NOTES:

1. Work this sheet with Sheets S-6 through S-21.
2. The above deflections are not to be used in the field if the engineer is working from the grade elevations adjusted for dead load deflections as shown on this sheet.

FILE NAME = \S:\2202-20866-001\STRUCT\CD\01 DESIGN\08202018\SHEET\08202018-CONN-05-007-SHT-SP.DGN  
 BONDHUJOD \S:\2202-20866-001\STRUCT\CD\01 DESIGN\08202018\SHEET\08202018-CONN-05-007-SHT-SP.DGN  
 TENG & ASSOCIATES, INC.  
 ENGINEERS/ARCHITECTS/PLANNERS  
 CHICAGO, ILLINOIS