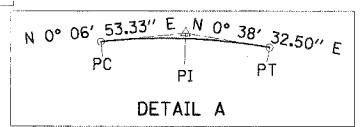
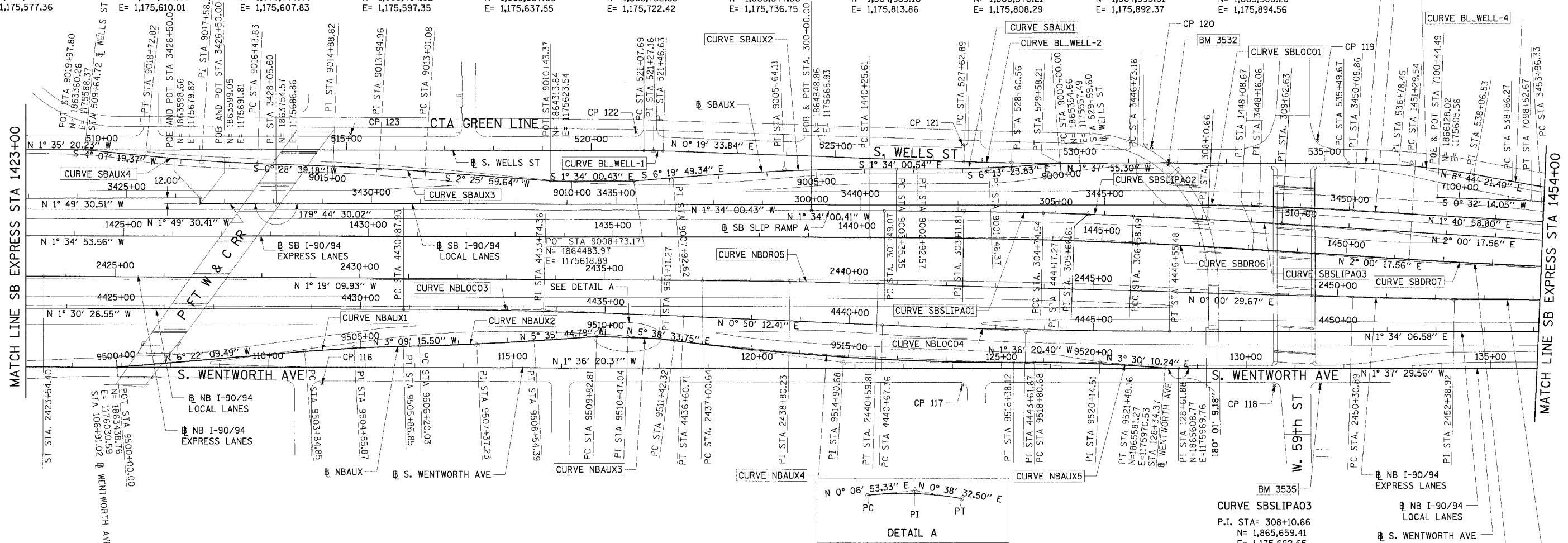


F.A.I. RTE.	SECTION	COUNTY	TOTAL SHEETS	SHEET NO.
90/94		COOK	556	34
STA.	TO STA.			
FED. ROAD DIST. NO. 1	ILLINOIS	FED. AID PROJECT		
* (1B1B, ETC. 2324.6-1P)R-8			62300	

<b>CURVE SBAUX1</b> P.I. STA= 9001+46.37 N= 1,865,209.16 E= 1,175,573.36 Δ= 4° 39' 23" D= 1° 35' 30" R= 3600.00' T= 146.37' L= 292.57' E= 2.97' θ= N/A T.R.= N/A S.E. RUN= N/A P.C. STA= 9000+00.00 N= 1,865,354.66 E= 1,175,557.49 P.T. STA= 9002+92.57 N= 1,865,062.84 E= 1,175,577.36	<b>CURVE SBAUX2</b> P.I. STA= 9005+64.11 N= 1,864,791.41 E= 1,175,584.78 Δ= 4° 45' 49" D= 1° 02' 30" R= 5500.00' T= 228.77' L= 457.27' E= 4.76' θ= N/A T.R.= N/A S.E. RUN= N/A P.C. STA= 9003+35.35 N= 1,865,020.09 E= 1,175,578.53 P.T. STA= 9007+92.62 N= 1,864,564.03 E= 1,175,607.83	<b>CURVE SBAUX3</b> P.I. STA= 9013+94.96 N= 1,863,962.56 E= 1,175,608.62 Δ= 1° 57' 20" D= 1° 02' 30" R= 5500.00' T= 93.88' L= 187.72' E= 0.80' θ= N/A T.R.= N/A S.E. RUN= N/A P.C. STA= 9013+01.08 N= 1,864,056.35 E= 1,175,612.60 P.T. STA= 9014+88.82 N= 1,863,868.69 E= 1,175,607.83	<b>CURVE SBAUX4</b> P.I. STA= 9017+58.36 N= 1,863,599.16 E= 1,175,605.59 Δ= 3° 38' 40" D= 1° 35' 30" R= 3600.00' T= 114.53' L= 228.99' E= 0.80' θ= N/A T.R.= N/A S.E. RUN= N/A P.C. STA= 9016+43.83 N= 1,863,713.69 E= 1,175,606.54 P.T. STA= 9018+72.82 N= 1,863,484.92 E= 1,175,597.35	<b>CURVE SBLOCO1</b> P.I. STA= 3448+16.06 N= 1,865,764.28 E= 1,175,631.89 Δ= 3° 14' 59" D= 0° 50' 33" R= 6800.00' T= 192.90' L= 385.69' E= 1.82' θ= 2.5% T.R.= 41' (41') S.E. RUN= 103' (103') P.C. STA= 3446+23.16 N= 1,865,571.45 E= 1,175,637.16 P.T. STA= 3450+08.86 N= 1,865,957.09 E= 1,175,637.55	<b>CURVE SBDRO6</b> P.I. STA= 1444+17.27 N= 1,865,361.46 E= 1,175,708.72 Δ= 3° 35' 11" D= 0° 27' 29" R= 12510.00' T= 391.66' L= 783.06' E= 2.74' θ= NC T.R.= N/A S.E. RUN= N/A P.C. STA= 1440+25.61 N= 1,864,969.95 E= 1,175,719.53 P.T. STA= 1448+08.67 N= 1,865,752.88 E= 1,175,722.42	<b>CURVE SBDRO7</b> P.I. STA= 1455+16.63 N= 1,866,460.40 E= 1,175,747.19 Δ= 3° 33' 01" D= 0° 27' 31" R= 12490.00' T= 387.09' L= 773.94' E= 6.00' θ= NC T.R.= N/A S.E. RUN= N/A P.C. STA= 1451+29.54 N= 1,866,073.55 E= 1,175,733.65 P.T. STA= 1459+03.48 N= 1,866,847.36 E= 1,175,736.75	<b>CURVE NBDRO5</b> P.I. STA= 2438+80.23 N= 1,864,809.56 E= 1,175,813.83 Δ= 1° 19' 40" D= 0° 22' 11" R= 15500.00' T= 179.59' L= 359.17' E= 1.44' θ= NC T.R.= N/A S.E. RUN= N/A P.C. STA= 2437+00.64 N= 1,864,630.02 E= 1,175,817.97 P.T. STA= 2440+59.81 N= 1,864,989.16 E= 1,175,813.86	<b>CURVE NBDRO6</b> P.I. STA= 2452+38.92 N= 1,866,168.26 E= 1,175,814.03 Δ= 1° 35' 21" D= 0° 22' 55" R= 15000.00' T= 208.03' L= 416.02' E= 1.04' θ= NC T.R.= N/A S.E. RUN= N/A P.C. STA= 2450+30.89 N= 1,865,960.24 E= 1,175,814.00 P.T. STA= 2454+46.92 N= 1,866,376.21 E= 1,175,808.29	<b>CURVE NBLOCO3</b> P.I. STA= 4433+74.36 N= 1,864,307.20 E= 1,175,888.18 Δ= 2° 20' 39" D= 0° 24' 33" R= 14000.00' T= 572.79' L= 1044.00' E= 1.44' θ= NC T.R.= N/A S.E. RUN= N/A P.C. STA= 4430+87.93 N= 1,864,020.87 E= 1,175,895.72 P.T. STA= 4436+60.71 N= 1,864,593.61 E= 1,175,892.37	<b>CURVE NBLOCO4</b> P.I. STA= 4443+61.67 N= 1,865,294.49 E= 1,175,902.60 Δ= 2° 24' 19" D= 0° 24' 33" R= 14000.00' T= 293.90' L= 587.72' E= 3.08' θ= NC T.R.= N/A S.E. RUN= N/A P.C. STA= 4440+67.76 N= 1,865,000.61 E= 1,175,898.31 P.T. STA= 4446+55.48 N= 1,865,588.28 E= 1,175,894.56
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<b>CURVE NBAUX1</b> P.I. STA= 9504+85.87 N= 1,863,921.64 E= 1,175,976.69 Δ= 3° 12' 54" D= 1° 35' 30" R= 3600.00' T= 101.03' L= 202.00' E= 1.42' θ= N/A T.R.= N/A S.E. RUN= N/A P.C. STA= 9503+84.85 N= 1,863,821.23 E= 1,175,987.89 P.T. STA= 9505+86.85 N= 1,864,022.51 E= 1,175,971.13	<b>CURVE NBAUX2</b> P.I. STA= 9507+37.23 N= 1,864,172.66 E= 1,175,962.85 Δ= 2° 26' 29" D= 1° 02' 30" R= 5500.00' T= 117.20' L= 234.36' E= 1.25' θ= N/A T.R.= N/A S.E. RUN= N/A P.C. STA= 9506+20.03 N= 1,864,055.64 E= 1,175,969.30 P.T. STA= 9508+54.39 N= 1,864,289.30 E= 1,175,951.42	<b>CURVE NBAUX3</b> P.I. STA= 9510+47.04 N= 1,864,481.34 E= 1,175,939.03 Δ= 0° 31' 39" D= 0° 24' 38" R= 13952.00' T= 64.23' L= 128.46' E= 0.15' θ= N/A T.R.= N/A S.E. RUN= N/A P.C. STA= 9509+82.81 N= 1,864,417.11 E= 1,175,938.90 P.T. STA= 9511+11.27 N= 1,864,545.57 E= 1,175,939.75	<b>CURVE NBAUX4</b> P.I. STA= 9514+90.68 N= 1,864,923.14 E= 1,175,977.06 Δ= 7° 14' 54" D= 1° 02' 30" R= 5500.00' T= 348.36' L= 695.79' E= 11.02' θ= N/A T.R.= N/A S.E. RUN= N/A P.C. STA= 9511+42.32 N= 1,864,576.47 E= 1,175,942.80 P.T. STA= 9518+38.12 N= 1,865,271.36 E= 1,175,967.30	<b>CURVE NBAUX5</b> P.I. STA= 9520+14.51 N= 1,865,447.69 E= 1,175,962.35 Δ= 5° 06' 31" D= 1° 54' 35" R= 3000.00' T= 133.83' L= 267.48' E= 0.16' θ= 2.4 T.R.= 11' (0') S.E. RUN= 66' (0') P.C. STA= 9518+80.68 N= 1,865,313.91 E= 1,175,966.10 P.T. STA= 9521+48.16 N= 1,865,581.27 E= 1,175,970.53	<b>CURVE BL_WELL-1</b> P.I. STA= 521+27.16 N= 1,864,522.25 E= 1,175,556.14 Δ= 1° 54' 54" D= 4° 55' 05" R= 1165.00' T= 19.47' L= 38.94' E= 0.16' θ= N/A T.R.= N/A S.E. RUN= N/A P.C. STA= 521+07.69 N= 1,864,502.79 E= 1,175,556.68 P.T. STA= 521+46.63 N= 1,864,541.72 E= 1,175,556.25	<b>CURVE BL_WELL-2</b> P.I. STA= 528+60.56 N= 1,865,255.64 E= 1,175,560.31 Δ= 1° 57' 29" D= 1° 00' 09" R= 5715.00' T= 97.67' L= 195.31' E= 0.83' θ= N/A T.R.= N/A S.E. RUN= N/A P.C. STA= 527+62.89 N= 1,865,157.98 E= 1,175,559.75 P.T. STA= 529+58.21 N= 1,865,353.27 E= 1,175,557.53	<b>CURVE BL_WELL-3</b> P.I. STA= 536+78.45 N= 1,866,073.22 E= 1,175,537.02 Δ= 10° 22' 17" D= 4° 02' 16" R= 1419.00' T= 128.78' L= 256.86' E= 5.83' θ= N/A T.R.= N/A S.E. RUN= N/A P.C. STA= 535+49.67 N= 1,864,994.49 E= 1,175,540.68 P.T. STA= 538+06.53 N= 1,866,200.51 E= 1,175,556.58	<b>CURVE SBSLIPA01</b> P.I. STA= 303+11.81 N= 1,865,160.56 E= 1,175,660.40 Δ= 1° 25' 14" D= 0° 26' 11" R= 13128.07' T= 127.96' L= 325.47' E= 1.01' θ= N/A T.R.= N/A S.E. RUN= N/A P.C. STA= 301+49.07 N= 1,864,997.88 E= 1,175,664.85 P.C.C. STA= 304+74.54 N= 1,865,323.30 E= 1,175,659.99	<b>CURVE SBSLIPA02</b> P.I. STA= 305+66.61 N= 1,865,415.38 E= 1,175,659.75 Δ= 0° 49' 32" D= 0° 26' 54" R= 12779.64' T= 92.08' L= 184.15' E= 0.33' θ= N/A T.R.= N/A S.E. RUN= N/A P.C.C. STA= 304+74.54 N= 1,865,323.30 E= 1,175,659.99	<b>CURVE SBLOCO3</b> P.I. STA= 308+10.66 N= 1,865,659.41 E= 1,175,662.65 Δ= 1° 19' 32" D= 0° 26' 10" R= 13137.24' T= 151.98' L= 303.94' E= 0.88' θ= N/A T.R.= N/A S.E. RUN= N/A P.C.C. STA= 306+58.69 N= 1,865,507.45 E= 1,175,660.85 P.T. STA= 309+62.63 N= 1,865,811.30 E= 1,175,667.96
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CTE | AECOM

- NOTES:**
- AVERAGE GRID TO GROUND CONVERSION FACTOR = 1.000010988654360
  - FOR BENCH MARK INFORMATION, SEE SHEET 1 OF ALIGNMENT PLAN SHEETS.

REVISIONS	
NAME	DATE

ILLINOIS DEPARTMENT OF TRANSPORTATION  
F.A.I. 90/94 (DAN RYAN EXPRESSWAY)  
71ST STREET TO 31ST STREET (NB EXPRESS LANES)

ALIGNMENT PLAN

SCALE: 1"=100'  
DATE: 7/7/05

DRAWN BY: NJH/AMM  
CHECKED BY: JAL/MS

06/24/2005 10:46:47 AM