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**STRUCTURE GEOTECHNICAL REPORT  
CIRCLE INTERCHANGE RECONSTRUCTION  
RETAINING WALL 20 (PROPOSED SN 016-1811)  
F.A.I ROUTE 90/94/290  
IDOT D-91-227-13/ PTB 163-001  
COOK COUNTY, ILLINOIS**

**For  
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<b>11. Abstract</b>		
<p>A 414.7-foot long, 13.6 feet maximum retained height new Mechanically Stabilized Earth (MSE) retaining walls will be constructed along the back-to-back and extended sections to retain the proposed Ramp EN Bridge east approach as well as the NB CD Road back slope. The proposed back-to-back fill MSE wall wraps around the proposed east abutment of EN Ramp Bridge.</p> <p>Beneath the pavement or topsoil, the subsurface soils consists of up to 3 to 13 feet of fill materials, up to 5 feet medium stiff to very stiff clay crust, up to 43 feet of very soft to medium stiff silty clay, 25 feet of very stiff to hard clay loam, and 40 feet of hard silty clay loam or dense to very dense silt to silty loam and sand extending to the boring termination depths or weathered bedrock. Sound bedrock was encountered at an elevation of about 490 feet. Groundwater was encountered within the fill layers at elevations of 580 to 589 feet. Groundwater is also present within the granular layers just above the top of bedrock.</p> <p>For the back-to-back portion of MSE wall between Stations 1610+98.10 and 1611+59.91, the proposed MSE wall is feasible with the use of Class III LCCF fill material. The wall will have a maximum factored bearing resistance of 2,200 psf using a geotechnical resistance factor of 0.65. The maximum long-term consolidation settlement of foundation soils will be less than 1-inch.</p> <p>For the extended portion of South MSE wall, to minimize the excavation behind the wall between Stations 1611+59.91 and 1613+88.64, we recommend using Class III LCCF with 0.7 H reinforcement width. It should be noted that the normal weight portion of the overall embankment behind the wall system be laid back so it does not exert any earth pressure on the LCCF backfill that is to be placed behind the LCCF MSE Mass. It is understood that an MSE wall was used in this portion because of the presence of a main drain under it at an elevation of about 560 feet.</p>		
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**STRUCTURE GEOTECHNICAL REPORT  
CIRCLE INTERCHANGE RECONSTRUCTION  
RETAINING WALL 20 (PROPOSED SN 016-1811)  
F.A.I. ROUTE 94 (I-290 WB TO I-90/94 SB)  
IDOT D-91-227-13/PTB 163-001  
COOK COUNTY, ILLINOIS  
FOR  
AECOM**

## **1.0 INTRODUCTION**

This report presents the results of Wang Engineering, Inc. (Wang) subsurface investigation, laboratory testing, geotechnical engineering evaluations and recommendations for a new retaining wall, designated as SN 016-1811 (Retaining Wall 20) proposed along the east approach of Ramp EN Bridge (SN 016-1712) in connection with the Circle Interchange Reconstruction project in the City of Chicago, Cook County, Illinois. A *Site Location Map* is presented as Exhibit 1.

The purpose of our investigation was to characterize the site soil and groundwater conditions, perform geotechnical engineering analyses, and provide recommendations for the design and construction of the new wall structure.

### **1.1 Project Description**

The Circle Interchange is over 50 years old and has significant congestion and safety problems. The project is aiming to improve safety and mobility as well as upgrade the mainline and interchange facilities. The project will also improve other modes of transportation such as transit, pedestrians and bicyclists within the same corridor.

The Circle Interchange Reconstruction project is along Interstate 90/94 (I-90/94) from south of Roosevelt Road to north of Lake Street, along Interstate 290 (I-290) from Loomis Street to the Circle Interchange; and along Congress Parkway from the Circle Interchange to Canal Street/Old Post Office. The routes typically have three lanes of traffic in each direction with mostly one lane ramp at interchanges. Locally, the north leg is known as the Kennedy Expressway, the south leg as the Dan Ryan Expressway and the west leg as the Eisenhower Expressway. Within the project area, there are

several cross street bridges over I-90/94 and I-290 considered for reconstruction. Along I-90/94, from south to north, the cross street overpasses include Taylor Street, Van Buren Street, Jackson Boulevard, and Adams Street. Along I-290, from west to east, the cross street overpasses include Morgan Street, Peoria Street, and Halsted Street.

The proposed improvements include additional through lanes in each direction on I-90/94. The horizontal alignment and vertical profiles throughout the interchange will be improved. A new two-lane flyover, Ramp NW (Flyover) will be constructed for I-90/94 northbound to I-290 westbound traffic. Cross street bridges, Morgan Street, Harrison Street, Halsted Street, Peoria Street, Taylor Street, Adams Street, Jackson Boulevard, and Van Buren Street will be reconstructed. Various existing ramps will be reconstructed and up to fifty new retaining walls will be constructed.

## **1.2 Proposed Structure**

Retaining wall 20 (SN 016-1811) is proposed to support the east approach of the EN Ramp Bridge. Based on the Type, Size, and Location (TSL) plan dated September 22, 2017 provided by HBM Engineering Group, LLC. (HBM), the wall is proposed to be a Mechanically Stabilized Earth (MSE) wall. The north MSE wall begins at Station 1611+59.91 on north side of EN Ramp, wraps the proposed EN Bridge east abutment, and ends at Station 1610+98.10 on south side of EN Ramp. The south wall begins at this point and ends at Station 1613+88.64. The north MSE wall will have a maximum retained of 13.6 feet. The TSL plan is included in the *Appendix D*.

## **1.3 Existing Structure**

There is no existing retaining wall structure due to a new alignment of EN Ramp Bridge.

## **2.0 SITE CONDITIONS AND GEOLOGICAL SETTING**

The site is located within the City of Chicago at the I-90/94 and I-290 Circle Interchange. On the USGS *Chicago Loop 7.5 Minute Series* map, the wall is located in the NW<sup>1</sup>/<sub>4</sub> of Section 16, Tier 39 N, Range 14 E of the Third Principal Meridian.

The following review of published geologic data, with emphasis on factors that might influence the design and construction of the proposed engineering works, is meant to place the project area within a geological framework and confirm the dependability and consistency of the present subsurface investigation results. For the study of the regional geologic framework, Wang considered

northeastern Illinois in general and Cook County in particular. Exhibit 2 illustrates the *Site and Regional Geology*.

## **2.1 Physiography**

The wall is situated within the Chicago Lake Plain Physiographic Subsection. The area is characterized by a flat surface that slopes gently toward the lake, largely made of groundmoraine till covered by thin and discontinuous lacustrine silt and clay. The ground elevation along the wall ranges from 583 feet at the west end to 591 feet at the east end.

## **2.2 Surficial Cover**

The project area was shaped during the Wisconsin-age glaciation, and more than 75-foot thick drift covers the bedrock (Leetaru et al. 2004). The glacial cover is made up of clay and silt of the Equality Formation of the Mason Group and diamictons of the Wadsworth and Lemont Formations of the Wedron Group (Hansel and Johnson 1996). The Equality Formation is made up of bedded silt and clay, locally laminated, with lenses and/or thin beds of sand and gravel. The Wadsworth Formation consists of relatively homogenous, massive, gray till with clay to silty clay matrix, with dolostone and shale clasts and occasional lenses of sorted and stratified silt. The Wadsworth Formation is underlain by the pebbly silty clay loam to silty loam diamicton of the Yorkville Member of the Lemont Formation, known informally as the Chicago “hardpan.”

From a geotechnical viewpoint, the Equality Formation is characterized by low strength, medium to high plasticity, and medium to high moisture content, whereas the Wadsworth Formation is characterized by low plasticity, medium to low moisture content, medium to very stiff consistency, poor permeability, and low compressibility. The Yorkville Member (hardpan) is characterized by low plasticity, high blow counts, and low moisture content (Bauer et al. 1991; Peck and Reed 1954).

## **2.3 Bedrock**

In the project area, the glacial deposits unconformably rest over approximately 350-foot thick Silurian-age dolostone (Leetaru et al 2004). The top of bedrock may be encountered at 475 to 500 feet elevation or 75 to 100 feet below ground surface (bgs) or more. The Silurian dolostone dips gently eastward at a pace of 15 feet per mile. Only inactive faults are known in the area, and the seismic risk is minimal (Leetaru et al. 2004; Willman 1971). There are no records of mining activity in the area, but deep tunnel excavations are known to exist.

Our subsurface investigation results fit into the local geologic context. The borings drilled in the project area revealed the native sediments consist of clay to silty clay diamicton of the Wadsworth Formation resting on top of more competent silty clay loam diamicton (hardpan) of the Lemont Formation, which in turn is underlain by bedrock. Sound dolostone bedrock was sampled at a depth of 102 feet bgs, corresponding to 490 feet elevation, within the range predicted based on published geological data.

### **3.0 METHODS OF INVESTIGATION**

The following sections outline the subsurface and laboratory investigations. All elevations in this report are based on NAVD 1988.

#### **3.1 Subsurface Investigation**

Wang drilled six structure borings, designated as 20-RWB-01 and 21-RWB-01 through 21-RWB-05 drilled in September to November, 2013. Wang has also referenced two nearby structure borings, designated as 1710-B-01 and 1705-B-06A drilled from July to September, 2013. Wang also performed Boring VST-06 to obtain in-situ vane shear strength of soft clay. The as-drilled boring locations were surveyed by Dynasty Group, Inc. and station and offset information for each boring were provided by AECOM. Boring location data are presented in the *Boring Logs* (Appendix A). The as-drilled boring locations are shown in the *Boring Location Plan* (Exhibit 3).

ATV- and truck-mounted drilling rigs equipped with hollow stem augers, were used to advance and maintain an open borehole to 10 feet depth after that mud rotary was used to the boring termination depth. Soil sampling was performed according to AASHTO T 206, "*Penetration Test and Split Barrel Sampling of Soils.*" The soil was sampled at 2.5-foot intervals to 30 feet bgs and at 5-foot intervals to boring termination depths. Soil samples collected from each sampling interval were placed in sealed jars and transported to Wang Geotechnical Laboratory in Lombard, Illinois for further examination and laboratory testing.

Field boring logs, prepared and maintained by a Wang engineer or geologist, include lithological descriptions, visual-manual soil/rock classifications, results of Rimac and pocket penetrometer unconfined compressive strength tests, results of Standard Penetration Tests (SPT) recorded as blows per 6 inches of penetration. The SPT N value, shown on the soil profile, is the sum of the second and third blows per 6 inches. The soils were described and classified according to Illinois Division of

Highways (IDH) Textural Classification system. The field logs were finalized by an experienced engineering geologist after verifying the field visual classifications and laboratory test results.

Groundwater observations were made during drilling to a depth of 10 feet before using rotary wash method. Due to safety considerations, boreholes were backfilled with grout immediately upon completion.

### **3.2 Vane Shear Tests**

Wang performed vane shear tests in Boring VST-06. Vane shear test was performed using calibrated RocTest vane shear equipment. Tests were performed in undisturbed and remolded conditions. The sensitivity shown on the boring logs is the ratio of shear strength in undisturbed and remolded conditions. In general, the vane shear values for soft clays were significantly higher than the corresponding values from unconfined compressive strength tests using the RIMAC apparatus. Vane shear test results were used for analyses.

### **3.3 Laboratory Testing**

The soil samples were tested in the laboratory for moisture content (AASHTO T265), Atterberg limits (AASHTO T 89/T 90) and particle size analyses (AASHTO T 88) tests were performed on selected soil samples representing the main soil layers encountered during the investigation. Field visual descriptions of the soil samples were verified in the laboratory. Laboratory test results are shown in the *Boring Logs* (Appendix A), in the *Soil Profile* (Exhibit 4), and in the *Laboratory Test Results* (Appendix B).

## **4.0 RESULTS OF FIELD AND LABORATORY INVESTIGATIONS**

Detailed descriptions of the soil conditions encountered during our subsurface investigation are presented in the attached *Boring Logs* (Appendix A) and in the *Soil Profile* (Exhibit 4). Please note that strata contact lines represent approximate boundaries between soil types. The actual transition between soil types in the field may be gradual in horizontal and vertical directions.

### **4.1 Soil Conditions**

Borings drilled on the roadway encountered 13 to 14 inches of concrete overlying 3 to 5 inches of asphalt followed by crushed stone base course. Borings drilled on the grassy area encountered 5 to 12 inches of silty loam topsoil. In descending order, the general lithologic succession encountered

beneath the pavement structure or topsoil includes: 1) man-made ground (fill); 2) medium stiff to very stiff silty clay to silty clay loam; 3) very soft to medium stiff clay to silty clay; 4) stiff to hard clay to silty clay loam; 5) hard silty clay loam and dense to very dense silt to silty loam and gravelly sand; and 6) strong dolostone.

*1) Man-made ground (fill)*

Underneath the topsoil, pavement structure, or at the surface, the borings encountered 3 to 13 feet of fill materials. Granular fill consists of medium dense to dense, gray crushed stone to brown sandy gravel and sandy loam. Cohesive fill includes very stiff to hard, brown to gray silty clay to silty clay loam and clay loam. The granular fill layer has N-values of 15 to over 50 blows per foot and moisture content values of 6 to 17%. The cohesive fill layer has unconfined compressive strength ( $Q_u$ ) values of 1.0 to 7.8 tsf and moisture content values of 13 to 19%.

*2) Medium stiff to very stiff silty clay to silty clay loam*

Beneath the fill, at elevations of 580 to 587 feet, the borings encountered 3 to 5-foot thick of medium stiff to very stiff, brown to gray silty clay to silty clay loam. This layer has  $Q_u$  values ranging from 0.8 to 3.0 tsf and moisture content values of 17 to 25%. This layer is commonly known as the “crust.”

*3) Very soft to medium stiff clay to silty clay*

At elevations of 574 to 582 feet (3 to 16 feet bgs), the borings revealed up to 43 feet of very soft to medium stiff, gray clay to silty clay with Rimac  $Q_u$  values of 0.08 to 0.82 tsf and moisture content values of 18 to 29%. Laboratory index testing on samples from this layer showed liquid limit ( $L_L$ ) values of 31 to 34% and plastic limit ( $P_L$ ) values of 16 to 17%. This layer is commonly known as the “Chicago Blue Clay.”

As discussed in Section 3.2, undrained shear strength values from vane shear tests are generally higher than Rimac tests. In-situ undisturbed vane shear strengths obtained in Boring VST-06 between elevations 577 and 542 feet varied from 580 to 980 psf.

*4) Stiff to hard clay to silty clay loam*

At elevations of 536 to 542 feet (42 to 52 feet bgs), the borings encountered up to 25 feet of stiff to hard clay to silty clay loam. The clay to silty clay has  $Q_u$  values of 1.2 to 8.5 tsf and moisture content values of 11 to 27%. Laboratory index testing on samples from this layer showed  $L_L$  values of 25 to 41% and  $P_L$  values of 15 to 18%.

*(5) Hard silty clay loam and very dense silt to silty loam and gravelly sand*

At elevations of 515 to 531 feet (57 to 82 feet bgs) the borings encountered up to 40 feet of hard silty clay loam to silty loam, dense to very dense silt to silty loam and very dense gravelly sand. This layer has  $Q_u$  values of greater than 4.5 tsf, moisture content values of 10 to 17%, and N values of 38 to over 50 blows per foot. Numerous sampler refusal and hard drilling conditions were recorded within this layer.

*(6) Strong dolostone*

The nearby structure boring, 1705-B-06A encountered strong bedrock at elevation of 490 feet or 102 feet bgs. Based on the 10-foot rock core obtained from the borings, the measured RQD value is 62% corresponding fair rock quality. *Bedrock core photograph is shown in Appendix A.*

## **4.2 Groundwater Conditions**

The groundwater was not observed during drilling or after drilling in borings due to the mud rotary drilling from 10 feet bgs. A Piezometer 1703-PZ-01 was installed for the nearby structure about 400 feet north of the proposed retaining wall 20 on November 12, 2014 and monitored until July 2017. The screen was placed with the top and bottom elevations at 507.2 and 487.2 feet (75 to 95 feet bgs), respectively within granular layers above bedrock. A summary of the monitoring data between November 2014 and March 2017 is shown in Figure 1.

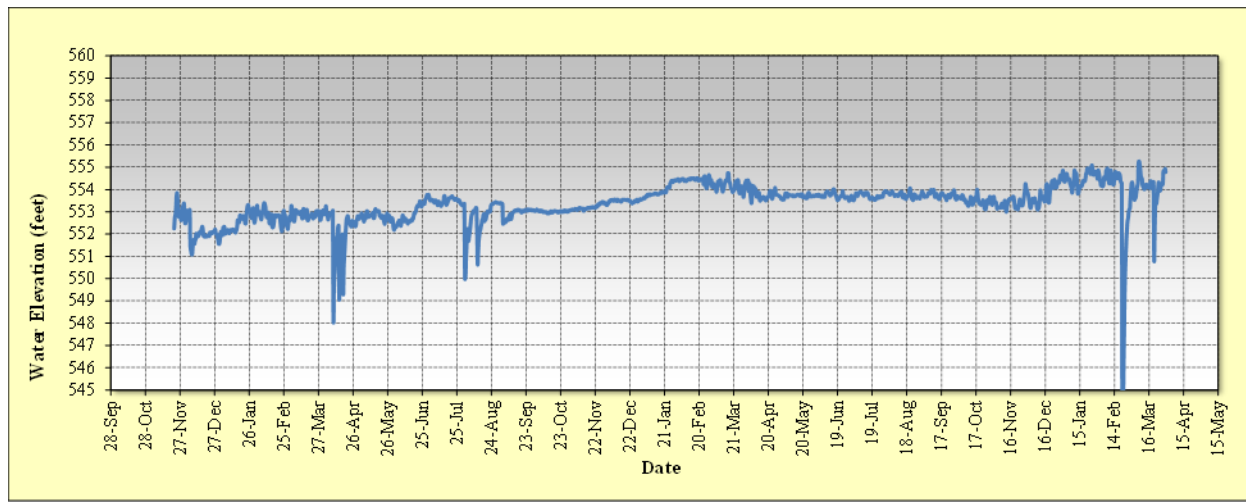


Figure 1: Summary of Groundwater Monitoring Data

The data shows groundwater that is under hydrostatic pressure head. The average hydrostatic elevation within the aquifer is about 553 feet. However, the hydrostatic pressure will not impact the proposed Wall 20 construction since the MSE wall is proposed at much higher elevations.

Although groundwater was not observed within upper fill layers, we anticipate perched water may be encountered during times of heavy precipitation. Therefore, the design and construction of the wall should consider the perched water between 589 and 580 feet elevations within the fill layers with permanent groundwater elevation for 553 feet.

### 4.3 Seismic Design Considerations

The retaining wall is located in Seismic Performance Zone (SPZ) 1 and is not required to be designed for seismic forces as per 2012 IDOT *Bridge Manual* (IDOT 2012).

## 5.0 ANALYSIS AND RECOMMENDATIONS

### 5.1 Retaining Wall Type Evaluation

Based on the TSL plan, the proposed Retaining Wall 20 is mostly fill wall between Station 1610+99.10 and Station 1611+59.91 retaining the east approach of the Ramp EN Bridge then it becomes a primarily cut wall between Station 1611+59.91 and Station 1613+88.64 to retain EN Ramp embankment and northbound CD Road backslope. The back-to-back portion of the MSE wall is fill wall and will have a maximum retained height of approximately 13.5 feet and a maximum wall



height measured from the top of levelling pad to the top of Coping/Finished Grade at B.F. of wall will be 17.0 feet. The extended portion of MSE wall is a cut wall and will have a maximum total height of 14.2 feet and a maximum retained height of 10.7 feet.

Consideration was given in using standard cast-in-place concrete cantilever (T-type) with spread footings; however, it was ruled out due to low bearing resistance and excessive settlements of foundation soils. They would need to be supported on driven piles or drilled shafts. Driven piles are not considered suitable due to noise and vibration concerns but drilled shafts placed on hardpan could be used. The proposed MSE wall is a feasible option but will require preloading or ground improvement with lightweight fill to satisfy the maximum 1-inch settlement criterion for the roadway for back-to-back portion of the wall.

The following sections present the results of our geotechnical engineering analyses and recommendations for the MSE wall design and construction.

## **5.2 Back-to-Back MSE Wall Section**

This section covers our evaluations and recommendation for the back-to-back MSE wall section. The MSE retaining wall base should be established a minimum of 3.5 feet below the finished grade at the front face of the wall for frost protection. The proposed MSE walls on the north and south sides are back-to-back wall sections and are retaining new fill. We note that there is an existing main drain alignment enters the wall area at an approximate Station 1610+70 on the south side, primarily follows the right edge right side wall on the south side and exits at an approximate Station 1612+30 on the south side. Based on the cross sections, the existing main is a 4.5-foot wide and 4.0-foot high with an invert elevation of 556.85 feet.

### *5.2.1 Bearing Resistance and External Stability Analyses*

Based on our boring data, the foundation soils at the MSE wall base elevations includes about 3.5 feet of granular fill overlying up to 35 feet of soft to medium stiff clay to silty clay. We estimate, without treatment, the foundation soils will have a nominal bearing resistance of 3,400 psf and a factored bearing resistance of 2,200 psf based on a geotechnical resistance factor of 0.65 (AASHTO 2014).

We analyzed the following options to satisfy the factored bearing resistance available, external stability, and settlement. A reinforcement length equal to 70 percent of the total wall height or a minimum of 8 feet was used.

1. Using regular fill material (unit weight of 125 pcf) for the MSE wall zone and fill area; and
2. Using IDOT District One Class III Lightweight Cellular Concrete Fill (LCCF) for the MSE reinforcement zone between the back-to-back walls.

For the Option 1, at the highest portion of the wall near Station 1611+04.56, the wall will apply a maximum factored equivalent bearing pressure of 4,750 psf with a regular MSE wall fill material (unit weight is 125 pcf) which exceeds the factored bearing resistance available, thus Option 1 is not feasible.

In Option 2, to reduce the applied wall pressure, we have considered IDOT District One Class III LCCF with unit weight of 42 pcf for the MSE wall zone, and fill area in the back-to-back wall. There are no lateral forces pushing the wall; therefore, eccentricity is not a concern. We estimate the wall will apply a maximum equivalent factored bearing pressure of 1,700 psf; thus, the foundation soils will have sufficient bearing resistance to support the wall. This option is recommended.

The estimated friction angle between an MSE wall base and underlying cohesive soil is 30°, and the corresponding friction coefficient is 0.58. MSE retaining walls are designed based on a geotechnical sliding resistance factor of 1.0 for soil-on-soil contact (AASHTO 2014).

### 5.2.2 Settlement Analyses

We performed settlement analyses using data from Borings 20-RWB-01 and 21-RWB-01 since it is more conservative and closest to maximum height of the wall. We calculated the corresponding long-term settlement of cohesive foundation soils using IDOT *Spreadsheet for Cohesive Soils* dated December 9, 2014.

We noted that in calculating the net service pressure for settlement evaluations, the effect of excavation required to the MSE wall base was taken into consideration. The estimated long-term settlement at the maximum height was less than 1 inch, which is governed by the roadway.

### 5.2.3 Global Stability Analyses

With Class III LCCF being used as a fill material in reinforced zone and in between the walls and the whole mass will act as rigid body with significant reduction of the driving forces, we do not see global instability concerns for the proposed back-to-back MSE retaining wall section.

## 5.3 Extended South MSE Wall Section

The extended MSE Wall section between Station 1611+59.91 and 1613+88.64 is a primarily cut wall to retain the proposed Ramp EN embankment and the proposed Northbound CD Road backslope. The MSE retaining wall base should be established a minimum of 3.5 feet below the finished grade at the front face of the wall for frost protection. For open cut excavations needed for the MSE Wall, the excavation backslope shall be 1:1.5 (V:H) and be backfilled with LCCF in order to reduce lateral pressure exerted by regular backfill on the LCCF fill. It is understood that an MSE wall was used in this portion because of the presence of a main drain under it at an elevation of about 560 feet.

### 5.3.1 Bearing Resistance and External Stability Analyses

Based on our boring data, the foundation soils at the MSE wall base elevations includes about 3 feet of stiff to very stiff silty clay overlying up to 40 feet of soft to medium stiff clay to silty clay. We estimate the foundation soils will have a nominal bearing resistance of 3,100 psf and a factored bearing resistance of 2,000 psf based on a geotechnical resistance factor of 0.65 (AASHTO 2014).

We have considered reinforcement lengths equal to 70 percent of the total wall height or a minimum of 8 feet. We have analyzed several alternatives for the fill material to be used in the reinforcement zone and fill area on top of 1:1.5 (V:H) excavation back-slope, as follows:

1. Using regular fill material (unit weight of 125 pcf) for the MSE wall zone fill area;
2. Using IDOT District One Class III LCCF for the MSE reinforcement zone and on top of laid back excavation back-slope.; and
3. Using IDOT District One Class III LCCF (unit weight of 42 pcf) for the bottom MSE wall zone and regular fill (unit weight of 125 pcf) for the top 3 feet of MSE wall zone fill area, and on top of laid back excavation back-slope.

For the Option 1, at the highest portion of the wall near Station 1611+59.91, the wall will apply a maximum factored equivalent bearing pressure of 4,150 psf for 0.7 H reinforcement length with

regular MSE wall fill material (unit weight is 125 pcf) which exceeds the factored bearing resistance available.

For the Option 2, we have considered Class III LCCF for the MSE wall reinforcement zone and on top of laid back excavation back-slope, thus no lateral push was considered. We estimate the wall will apply a maximum factored equivalent bearing pressure of 1,250 psf, thus the foundation soils will have sufficient bearing resistance to support the wall.

For the Option 3, we have considered Class III LCCF for bottom of the MSE wall and regular fill for the top 3 feet of the MSE wall and on top of laid back excavation back-slope. We estimate the wall backfilled with Class III LCCF will apply a maximum equivalent factored bearing pressure of 1,900 psf, thus the foundation soils will have sufficient bearing resistance to support the wall. The wall will have an adequate resistance against sliding.

The estimated friction angle between an MSE wall base and underlying cohesive soil is 30°, and the corresponding friction coefficient is 0.58. MSE retaining walls are designed based on a geotechnical sliding resistance factor of 1.0 for soil-on-soil contact (AASHTO 2014).

To minimize the excavation behind the wall, we recommend Options 2 or Option 3 with 0.7 H reinforcement width for the extended wall section. It should be noted that the normal weight portion of the overall embankment behind the wall system be laid back so it does not exert any earth pressure on the LCCF backfill that is to be placed behind the LCCF MSE Mass.

### *5.3.2 Settlement Analyses*

For the Options 2 and 3, considering the unloading and reloading effect and the placement of LCCF in at least the half of MSE Wall zone area, the estimated long-term settlement will be 1 inch or less.

### *5.3.3 Global Stability Analyses*

Global stability analysis was performed for the MSE wall maximum section with total height of 14.2 feet for both short-term (undrained) and long-term (drained). The computer program, SLIDE Version 6.0, was used to calculate the factor of safety (FOS). We estimate the maximum wall section has a short-term factor of safety (FOS) of 2.4 and a long-term FOS of 2.3 (Appendices C-1 and C-2), therefore satisfying the minimum IDOT FOS requirements (IDOT, 2015). The undrained analysis for

temporarily excavated ground sloped at 1:1.5 (V:H) before construction of MSE wall showed FOS of 2.6 (Appendix C-3).

## **6.0 CONSTRUCTION CONSIDERATIONS**

### **6.1 Excavation**

Any required excavations should be performed in accordance with local, state, and federal regulations including current OSHA regulations. The potential effect of ground movements upon nearby structures and utilities should be considered during construction. The extended portion of south wall will require temporary open cut excavations that could have maximum back-slope of 1:1.5 (V:H), depending on actual ground conditions encountered during construction.

### **6.2 Dewatering**

Based on the results of our investigation and proposed excavation for the wall, perched water is likely to be encountered during construction during times of heavy precipitation which should be removed through conventional sump and pump methods.

### **6.3 Filling and Backfilling**

All fill and backfill materials will be as per IDOT *Standard Specification for Road and Bridge Construction* (IDOT 2016).

### **6.4 Wall Construction**

The wall should be constructed as per IDOT *Standard Specification for Road and Bridge Construction* (IDOT 2016). Class III LCCF should be as per IDOT District One special provision.

### **6.5 Construction Monitoring**

There is no need for special construction monitoring for the retaining wall except normally required by the IDOT *Standard Specification for Road and Bridge Construction* (IDOT 2016).

## 7.0 QUALIFICATIONS

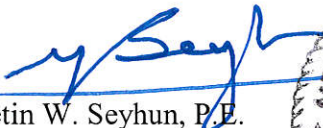
The analysis and recommendations submitted in this report are based upon the data obtained from the borings drilled at the locations shown on the boring logs and in Exhibit 3. This report does not reflect any variations that may occur between the borings or elsewhere on the site, variations whose nature and extent may not become evident until the course of construction. In the event that any changes in the design and/or location of Retaining Wall 20 (SN016-1811) are planned, we should be timely informed so that our recommendations can be adjusted accordingly.

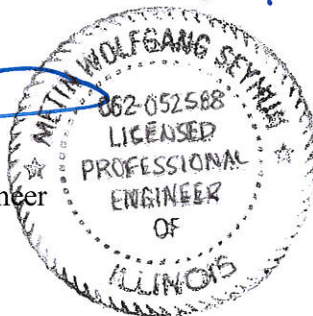
It has been a pleasure to assist AECOM and the Illinois Department of Transportation on this project. Please call if there are any questions, or if we can be of further service.


Respectfully Submitted,

WANG ENGINEERING, INC.

Exp. 11/30/2019

  
Metin W. Seyhun, P.E.  
Senior Geotechnical Engineer



  
Corina T. Farez, P.E., P.G.  
Vice President

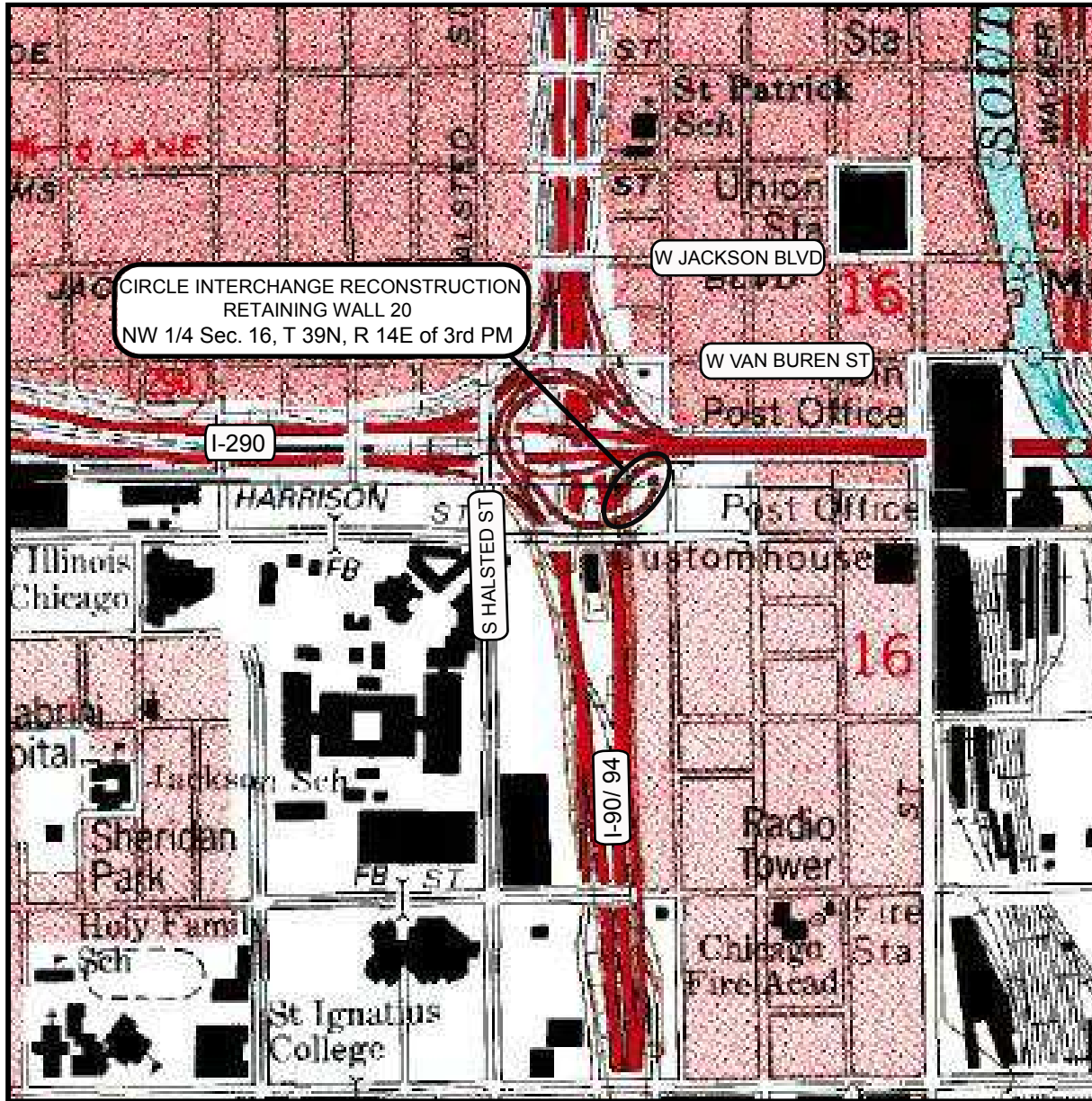
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## ***REFERENCES***

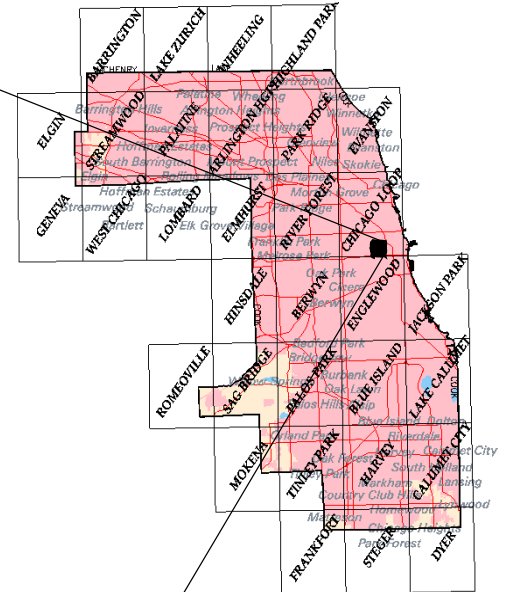
- AMERICAN ASSOCIATION OF STATE HIGHWAY TRANSPORTATION OFFICIALS (2014) *LRFD Bridge Design Specifications*. United States Department of Transportation, Washington, D.C.
- BAUER, R.A., CURRY, B.B., GRAESE, A.M., VAIDEN, R.C., SU, W.J., and HASEK, M.J., 1991, *Geotechnical Properties of Selected Pleistocene, Silurian, and Ordovician Deposits of Northeastern Illinois*: Environmental Geology 139, Illinois State Geological Survey, 69 p.
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- PECK, R.B., and REED, W.C., 1954, *Engineering Properties of Chicago Subsoils*: University of Illinois Engineering Experiment Station Bulletin No. 423: Urbana, University of Illinois, 62 p.
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## **EXHIBITS**





Cook County

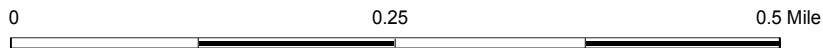


SITE LOCATION MAP: CIRCLE INTERCHANGE RECONSTRUCTION, RETAINING WALL 20, SN 016-1811, CHICAGO, IL

SCALE: GRAPHICAL

EXHIBIT 1

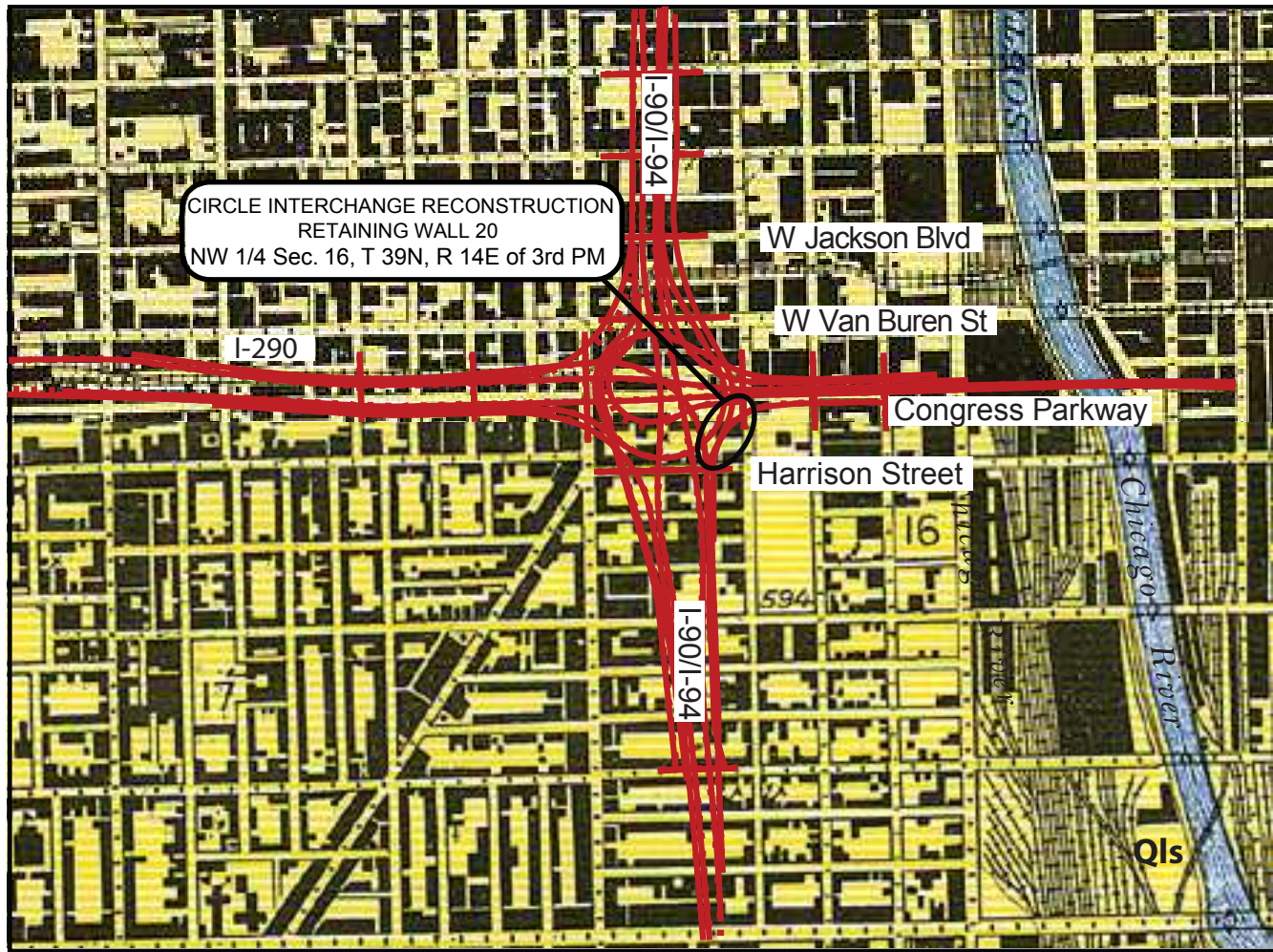
DRAWN BY: RKC  
CHECKED BY: NSB



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FOR AECOM

1100-04-01



### REGIONAL GEOLOGY



#### Wedron Group

- Wadsworth Formation
- Lemont Formation
- Tiskilwa Formation

Modified after Hansel and Johnson (1996)

## Legend

- Qls  
Glacial lake bottom  
(Covered by lacustrine deposits)

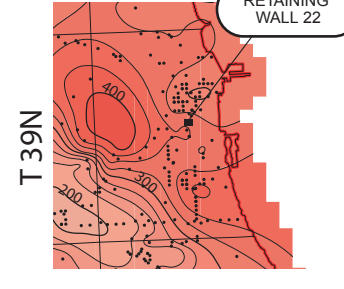
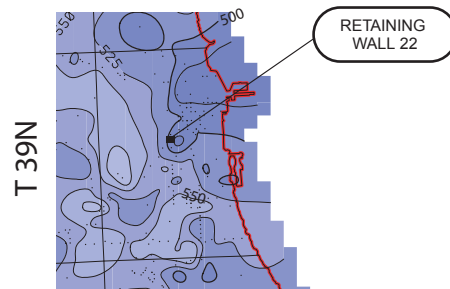
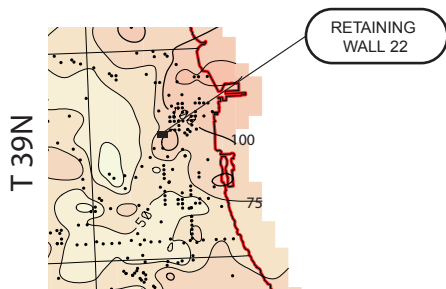
0 0.5 1.0 Miles

Modified after Bretz (1926)

#### DRIFT THICKNESS

#### BEDROCK TOPOGRAPHY

#### BEDROCK THICKNESS



0 2 4 8 miles

Modified after Leetaru et. al. (2004)

SITE AND REGIONAL GEOLOGY: CIRCLE INTERCHANGE RECONSTRUCTION, RETAINING WALL 20, SN 016-1811, CHICAGO, IL

SCALE: GRAPHICAL

EXHIBIT 2

DRAWN BY: RKC  
CHECKED BY: NSB



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1100-04-01



Benchmark: Cut square on center of door entrance to 707 W. Harrison St. (south side of Harrison St., approx. 90' west of west line of Des Plaines St.). Elevation 597.47.

Existing Structure: None. Traffic shall be maintained on the existing Ramp EN Structure (S.N. 016-2453) during construction of the proposed retaining wall. Subsequently, traffic shall be detoured to allow for construction of the remaining portions of the proposed Ramp EN (S.N. 016-1712) approaches.

**HIGHWAY CLASSIFICATION**

Ramp EN  
 Functional Class: Interstate  
 ADT: 26,600 (2012); 31,000 (2040)  
 ADTT: 1,032 (2012); 1,203 (2040)  
 DHV: 1,910 (2040)  
 Design Speed: 30 m.p.h.  
 Posted Speed: 30 m.p.h.  
 One-Way Traffic  
 Directional Distribution: 100%

Elev. 610

Elev. 600

Elev. 590

Elev. 580

Elev. 570

**GENERAL PLAN**  
**RETAINING WALL 20**

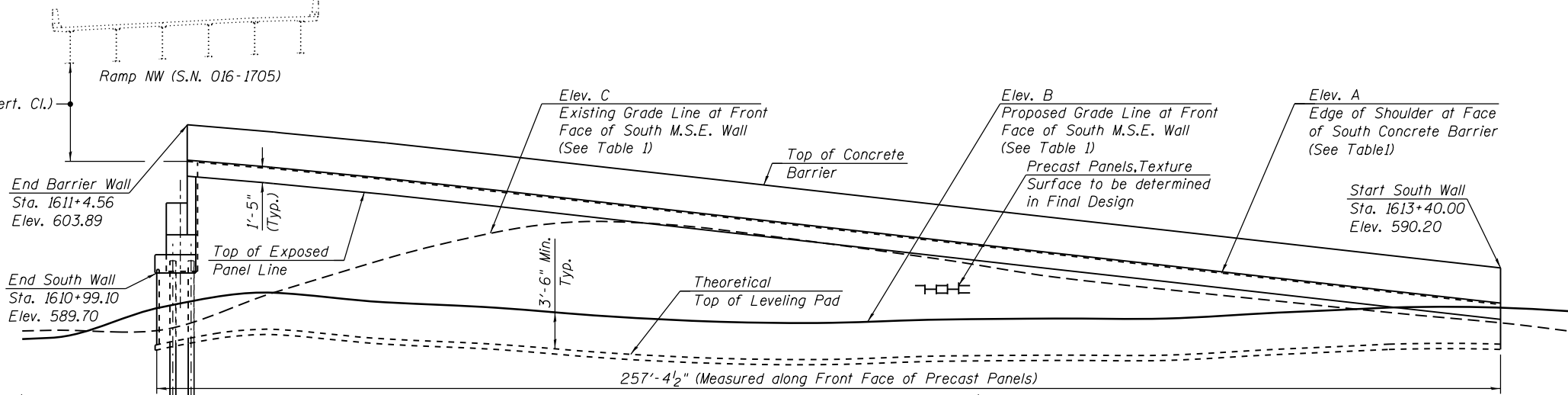
**F.A.I. RTE. 90/94/290 - SECTION 2014-005R&B**  
**COOK COUNTY**  
**STATION 1610+97.82 TO 1613+40.00**  
**STRUCTURE NO. 016-1811**

**SEISMIC DATA**

Seismic Performance Zone (SPZ) = 1  
 Design Spectral Acceleration at 1.0 sec. (SD1) = 0.085g  
 Design Spectral Acceleration at 0.2 sec. (SDS) = 0.144g  
 Soil Site Class = D

**NOTES:**

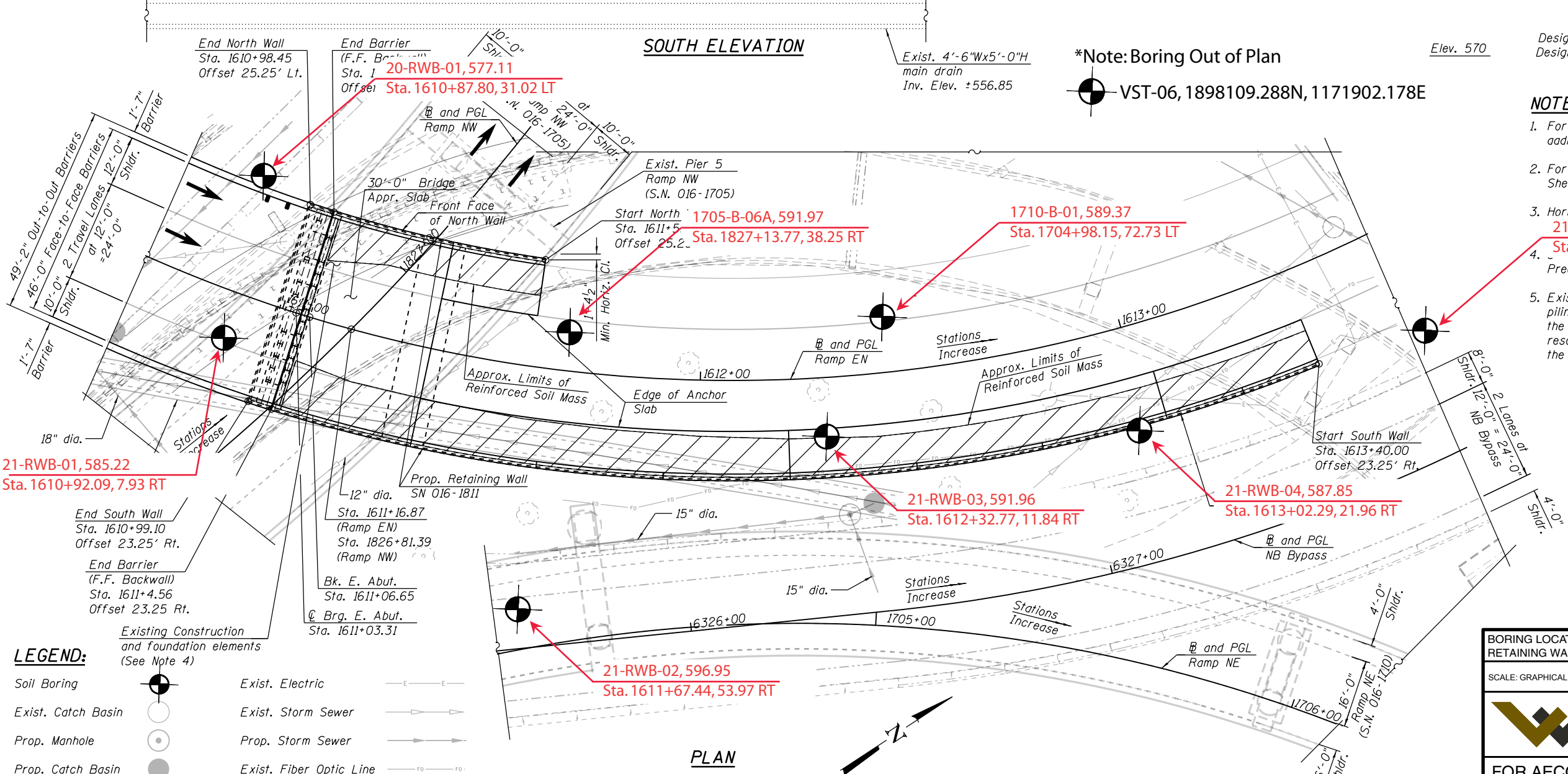
- For North and East Abutment MSE Wall Elevations and additional Highway Classification Data, see Sheet 2.
- For Table 1, Profile Grade Lines and Curve data, see Sheet 3.
- Horizontal dimensions measured along Front Face of 21-RWB-05, 583.31
- Station 1613+69.21, 25.02 RT, Front Face of Precast Panels relative to Ramp EN.
- Existing Construction and foundation elements (sheet piling, drilled shafts, steel piles, etc.) are present at the proposed location of North wall. Methods for resolving potential conflicts will be determined during the design phase.



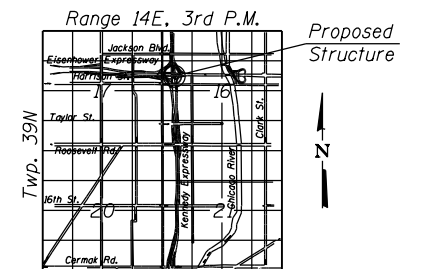
**SOUTH ELEVATION**

\*Note: Boring Out of Plan

VST-06, 1898109.288N, 1171902.178E



**PLAN**



**LOCATION SKETCH**

**LEGEND:**

- |  |  |                         |  |
|--|--|-------------------------|--|
| Existing Construction and foundation elements (See Note 4) |  |                         |  |
| Soil Boring  |  | Exist. Electric         |  |
| Exist. Catch Basin   |  | Exist. Storm Sewer      |  |
| Prop. Manhole  |  | Prop. Storm Sewer       |  |
| Prop. Catch Basin  |  | Exist. Fiber Optic Line |  |

BORING LOCATION PLAN: CIRCLE INTERCHANGE RECONSTRUCTION, RETAINING WALL 20, SN 016-1811, CHICAGO, IL

SCALE: GRAPHICAL EXHIBIT 3 DRAWN BY: RKC CHECKED BY: NSB

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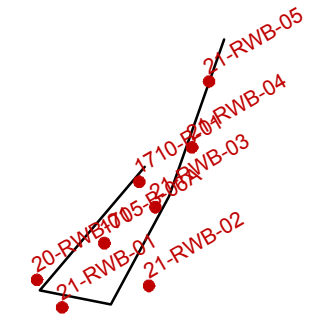
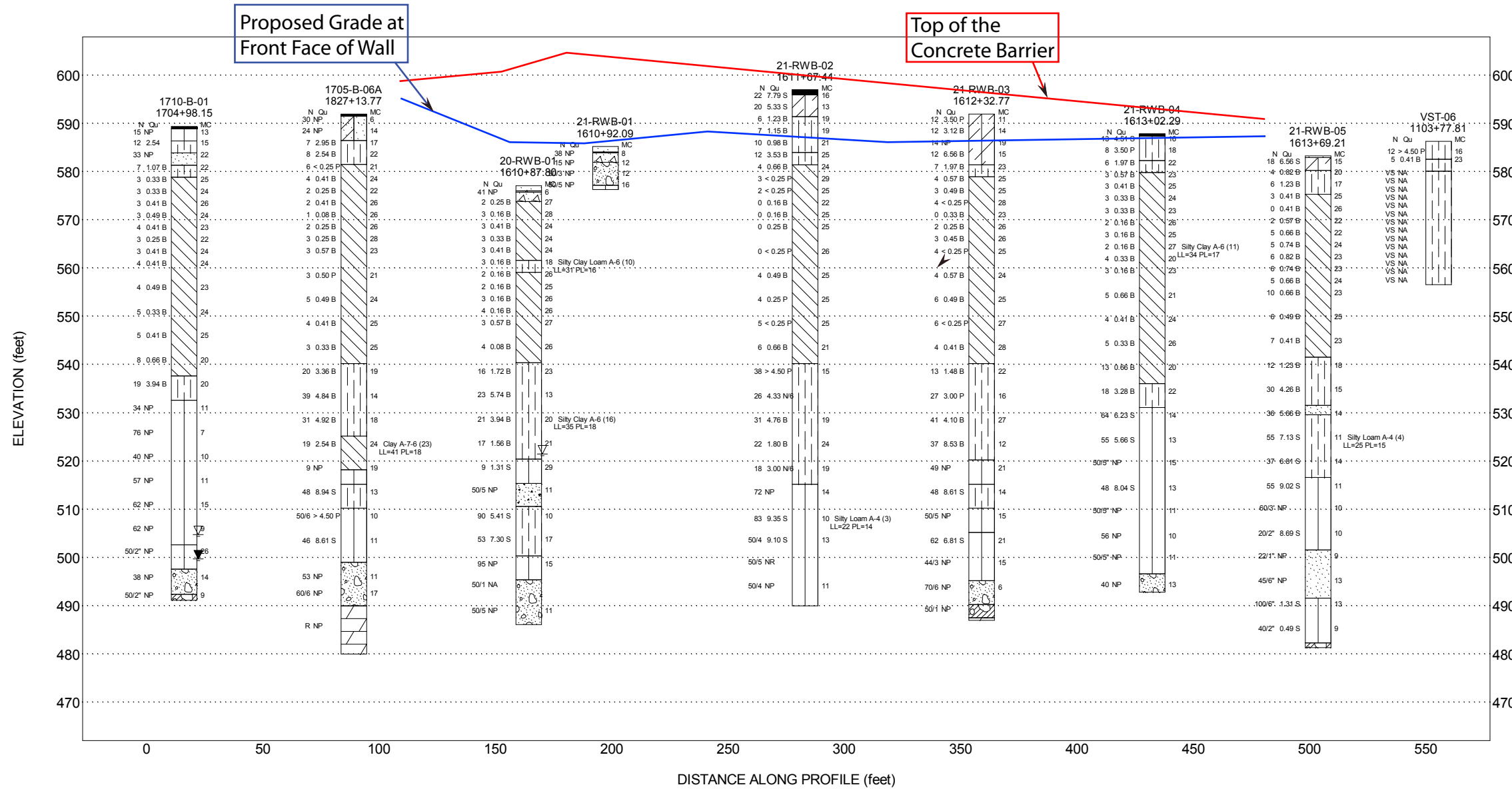
FOR AECOM 1100-04-01

**HBM**  
 ENGINEERING GROUP, LLC  
 CONSULTING & DESIGN  
 INSPECTION & TESTING  
 RESEARCH & TESTING

USER NAME = Ken.drabant	DESIGNED - MI, JJS	REVISED -
DESIGNED - MI, JJS	DRAWN - SK	REVISED -
PLOT SCALE = 28.00' / in.	CHECKED - MAI, MI	REVISED -
PLOT DATE = 9/15/2017	DATE - 08/11/2017	REVISED -

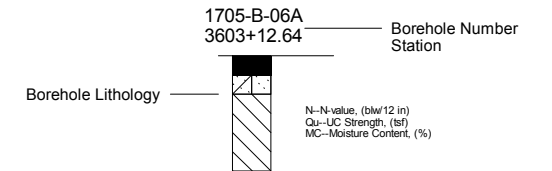
**STATE OF ILLINOIS**  
**DEPARTMENT OF TRANSPORTATION**

<b>STRUCTURE NO. 016-1811</b>		F.A.I. RTE. 90/94/290	SECTION 2014-005R&B	COUNTY COOK	TOTAL SHEETS 3	SHEET NO. 1
SCALE:	SHEET 1 OF 3 SHEETS	STA.	TO STA.	CONTRACT NO. 60X79		
ILLINOIS FED. AID PROJECT						

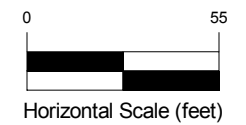


Site Map Scale 1 inch equals 200 feet

### Explanation:



- Water Level Reading at time of drilling.
- Water Level Reading 24-hr after drilling or at end of drilling



Vertical Exaggeration: 2x

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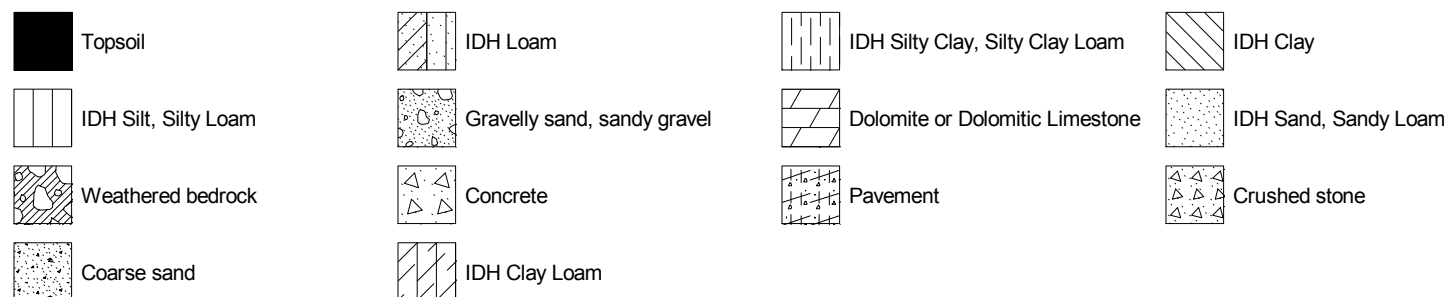
### Subsurface Soil Data Profile Retaining Wall 20, SN 016-1811



Circle Interchange Reconstruction  
Section 17, T39N, R14E of 3rd PM

JOB NUMBER	PLATE NUMBER
1100-04-01	EXHIBIT 4

### Lithology Graphics



## **APPENDIX A**



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# BORING LOG 20-RWB-01

WEI Job No.: 1100-04-01

Client: **AECOM**  
 Project: **Circle Interchange Reconstruction**  
 Location: **Section 17, T39N, R14E of 3rd PM**

Datum: NAVD 88  
 Elevation: 577.12 ft  
 North: 1897711.41 ft  
 East: 1171734.33 ft  
 Station: 1610+87.80  
 Offset: 31.0288 LT

Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)	Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)
		13.5-inch thick CONCRETE --PAVEMENT--									gravel						
	576.0	4.5-inch thick ASPHALT --PAVEMENT--															
	575.8	Dense, white CRUSHED STONE --BASE COURSE--			1	26 30 11	NP	6						9	0 1 1	0.16 B	25
	573.9	Very soft to soft, gray CLAY to SILTY CLAY, trace gravel			2	2 1 1	0.25 B	27				25		10	0 1 2	0.16 B	26
					3	2 2 1	0.16 B	28						11	1 2 2	0.16 B	26
					4	1 1 2	0.41 B	24						12	2 2 1	0.57 B	27
					5	1 2 1	0.33 B	24									
					6	1 1 2	0.41 B	24						13	1 2 2	0.08 B	26
	561.6	SOft, gray SILTY CLAY LOAM, trace gravel --L <sub>L</sub> (%)=31, P <sub>L</sub> (%)=16-- --%Gravel=4.8-- --%Sand=16.1-- --%Silt=54.8-- --%Clay=24.3-- --A-6 (10)--			7	2 1 2	0.16 B	18		540.4	Stiff to hard, gray SILTY CLAY to SILTY CLAY LOAM, trace gravel						
	559.1	Very soft to medium stiff, gray CLAY to SILTY CLAY, trace			8	0 1 1	0.16 B	26						14	3 6 10	1.72 B	23

### GENERAL NOTES

### WATER LEVEL DATA

Begin Drilling **10-28-2013** Complete Drilling **11-03-2013**  
 Drilling Contractor **Wang Testing Services** Drill Rig **CME-55 TMR [85%]**  
 Driller **R&J** Logger **A. Tomaras** Checked by **CLM**  
 Drilling Method **2.25" SSA to 10', mud rotary thereafter, boring backfilled upon completion**

While Drilling  $\nabla$  **56.00 ft**  
 At Completion of Drilling  $\nabla$  **mud in the borehole**  
 Time After Drilling **NA**  
 Depth to Water  $\nabla$  **NA**

The stratification lines represent the approximate boundary between soil types; the actual transition may be gradual.

WANGENGINC 11000401.GPJ WANGENG.GDT 9/14/17



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# BORING LOG 20-RWB-01

WEI Job No.: 1100-04-01

Client: **AECOM**  
 Project: **Circle Interchange Reconstruction**  
 Location: **Section 17, T39N, R14E of 3rd PM**

Datum: NAVD 88  
 Elevation: 577.12 ft  
 North: 1897711.41 ft  
 East: 1171734.33 ft  
 Station: 1610+87.80  
 Offset: 31.0288 LT

Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)	Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)
	520.4	Loose, gray SILT --Saturated--								500.4	Very dense, gray SILTY LOAM, trace gravel						
			45		15	7 8 15	5.74 B	13		515.4	--HARD DRILLING-- --Possible Cobbles-- Very dense, gray, coarse SAND	65		19	48 50/5	NP	11
		--L <sub>L</sub> (%)=35, P <sub>L</sub> (%)=18-- --%Gravel=1.0-- --%Sand=6.7-- --%Silt=53.8-- --%Clay=38.6-- --A-6 (16)--	50		16	6 9 12	3.94 B	20		510.6	--HARD DRILLING-- --Possible Cobbles-- Hard, gray SILTY CLAY LOAM to SILTY LOAM, trace gravel	70		20	32 45 45	5.41 S	10
			55		17	6 8 9	1.56 B	21				75		21	20 18 35	7.30 S	17
			60		18	3 3 6	1.31 S	29				80		22	39 47 48	NP	15

### GENERAL NOTES

Begin Drilling **10-28-2013** Complete Drilling **11-03-2013**  
 Drilling Contractor **Wang Testing Services** Drill Rig **CME-55 TMR [85%]**  
 Driller **R&J** Logger **A. Tomaras** Checked by **CLM**  
 Drilling Method **2.25" SSA to 10', mud rotary thereafter, boring**  
**backfilled upon completion**

### WATER LEVEL DATA

While Drilling  $\nabla$  **56.00 ft**  
 At Completion of Drilling  $\nabla$  **mud in the borehole**  
 Time After Drilling **NA**  
 Depth to Water  $\nabla$  **NA**

The stratification lines represent the approximate boundary between soil types; the actual transition may be gradual.

WANGENGINC 11000401.GPJ WANGENG.GDT 9/14/17





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 1145 N Main Street  
 Lombard, IL 60148  
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# BORING LOG 20-RWB-01

WEI Job No.: 1100-04-01

Client: **AECOM**  
 Project: **Circle Interchange Reconstruction**  
 Location: **Section 17, T39N, R14E of 3rd PM**

Datum: NAVD 88  
 Elevation: 577.12 ft  
 North: 1897711.41 ft  
 East: 1171734.33 ft  
 Station: 1610+87.80  
 Offset: 31.0288 LT

Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)	Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)
		--HARD DRILLING-- --Possible Cobbles--															
	495.4	Very dense, gray GRAVELLY SAND, some cobbles			23	50/1	NA										
			85														
					24	39 50/5	NP	11									
		--HARD DRILLING-- --Possible Boulders--															
	486.1	--ROLLER BIT REFUSAL-- Boring terminated at 91.00 ft															
			95														
			100														

### GENERAL NOTES

Begin Drilling **10-28-2013** Complete Drilling **11-03-2013**  
 Drilling Contractor **Wang Testing Services** Drill Rig **CME-55 TMR [85%]**  
 Driller **R&J** Logger **A. Tomaras** Checked by **CLM**  
 Drilling Method **2.25" SSA to 10', mud rotary thereafter, boring backfilled upon completion**

### WATER LEVEL DATA

While Drilling  $\nabla$  **56.00 ft**  
 At Completion of Drilling  $\nabla$  **mud in the borehole**  
 Time After Drilling **NA**  
 Depth to Water  $\nabla$  **NA**

The stratification lines represent the approximate boundary between soil types; the actual transition may be gradual.

WANGENGINC 11000401.GPJ WANGENG.GDT 9/14/17





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 Lombard, IL 60148  
 Telephone: 630 953-9928  
 Fax: 630 953-9938

# BORING LOG 21-RWB-01

WEI Job No.: 1100-04-01

Client: **AECOM**  
 Project: **Circle Interchange Reconstruction**  
 Location: **Section 17, T39N, R14E of 3rd PM**

Datum: NAVD 88  
 Elevation: 585.23 ft  
 North: 1897682.52 ft  
 East: 1171760.80 ft  
 Station: 1610+92.09  
 Offset: 7.9354 RT

Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)	Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)
		13-inch thick CONCRETE --PAVEMENT--															
	584.1	3-inch thick ASPHALT --PAVEMENT--															
	583.9																
		CRUSHED STONE --BASE COURSE--			1	13 20 18	NP	8									
	582.0																
		Medium dense to very dense, brown GRAVELLY SAND --FILL--			2	9 10 5	NP	12									
			5														
					3	25	NP	12									
	577.2																
	576.3	Very dense, brown SILTY LOAM, trace gravel			4	50/3	NP	16									
		--AUGER REFUSAL-- --Obstruction--															
		Boring terminated at 8.90 ft	10														
			15														
			20														

### GENERAL NOTES

Begin Drilling **10-13-2013** Complete Drilling **10-13-2013**  
 Drilling Contractor **Wang Testing Services** Drill Rig **D-50 TMR [78%]**  
 Driller **R&N** Logger **D. Kolpacki** Checked by **L. lordache**  
 Drilling Method **2.25" SSA, boring backfilled upon completion**

### WATER LEVEL DATA

While Drilling  $\nabla$  **DRY**  
 At Completion of Drilling  $\nabla$  **DRY**  
 Time After Drilling **NA**  
 Depth to Water  $\nabla$  **NA**

The stratification lines represent the approximate boundary between soil types; the actual transition may be gradual.



# BORING LOG 21-RWB-02

wangeng@wangeng.com  
 1145 N Main Street  
 Lombard, IL 60148  
 Telephone: 630 953-9928  
 Fax: 630 953-9938

WEI Job No.: 1100-04-01

Client: **AECOM**  
 Project: **Circle Interchange Reconstruction**  
 Location: **Section 17, T39N, R14E of 3rd PM**

Datum: NAVD 88  
 Elevation: 596.95 ft  
 North: 1897705.23 ft  
 East: 1171851.95 ft  
 Station: 1611+67.44  
 Offset: 53.9743 RT

Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)	Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)
	596.0	12-inch thick, brown LOAM, trace gravel --TOPSOIL-- Hard, gray CLAY LOAM, trace gravel --FILL--			1	13 11 11	7.79 S	16						9	1 1 1	< 0.25 P	25
			5		2	5 9 11	5.33 S	13				25		10	0 0 0	0.16 B	22
	591.5	Stiff to medium stiff, gray and brown, SILTY CLAY, trace gravel, slag, brick and wood --FILL--			3	2 2 4	1.23 B	19						11	0 0 0	0.16 B	25
			10		4	2 3 4	1.15 B	19				30		12	0 0 0	0.25 B	25
					5	3 5 5	0.98 B	21									
	584.0	Very stiff, brown and gray SILTY CLAY, trace gravel			6	3 5 7	3.53 B	25						13	0 0 0	< 0.25 P	26
	581.5	Very soft to medium stiff, gray CLAY to SILTY CLAY, trace gravel			7	0 2 2	0.66 B	24									
					8	1 1 2	< 0.25 P	29				40		14	0 1 3	0.49 B	25

### GENERAL NOTES

Begin Drilling **09-25-2013** Complete Drilling **09-30-2013**  
 Drilling Contractor **Wang Testing Services** Drill Rig **CME-55 TMR [85%]**  
 Driller **R&J** Logger **A. Tomaras** Checked by **L. lordache**  
 Drilling Method **2.25" HSA, boring backfilled upon completion**

### WATER LEVEL DATA

While Drilling  **Rotary wash**  
 At Completion of Drilling  **mud in the borehole**  
 Time After Drilling **NA**  
 Depth to Water  **NA**

The stratification lines represent the approximate boundary between soil types; the actual transition may be gradual.

WANGENGINC 11000401.GPJ WANGENG.GDT 9/14/17



# BORING LOG 21-RWB-02

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WEI Job No.: 1100-04-01

Client: **AECOM**  
 Project: **Circle Interchange Reconstruction**  
 Location: **Section 17, T39N, R14E of 3rd PM**

Datum: NAVD 88  
 Elevation: 596.95 ft  
 North: 1897705.23 ft  
 East: 1171851.95 ft  
 Station: 1611+67.44  
 Offset: 53.9743 RT

Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)	Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)
			45		15	2 2 2	0.25 P	25				65		19	11 10 16	4.33 N/6	
			50		16	1 2 3	< 0.25 P	25				70		20	10 12 19	4.76 B	19
			55		17	1 3 3	0.66 B	21				75		21	6 10 12	1.80 B	24
	540.2	Stiff to hard, gray SILTY CLAY LOAM, trace gravel															
			60		18	15 17 21	> 4.50 P	15				80		22	6 8 10	3.00 N/6	19

### GENERAL NOTES

### WATER LEVEL DATA

Begin Drilling **09-25-2013** Complete Drilling **09-30-2013**  
 Drilling Contractor **Wang Testing Services** Drill Rig **CME-55 TMR [85%]**  
 Driller **R&J** Logger **A. Tomaras** Checked by **L. lordache**  
 Drilling Method **2.25" HSA, boring backfilled upon completion**

While Drilling  **Rotary wash**  
 At Completion of Drilling  **mud in the borehole**  
 Time After Drilling **NA**  
 Depth to Water  **NA**

The stratification lines represent the approximate boundary between soil types; the actual transition may be gradual.

WANGENGINC 11000401.GPJ WANGENG.GDT 9/14/17



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# BORING LOG 21-RWB-02

WEI Job No.: 1100-04-01

Client: **AECOM**  
 Project: **Circle Interchange Reconstruction**  
 Location: **Section 17, T39N, R14E of 3rd PM**

Datum: NAVD 88  
 Elevation: 596.95 ft  
 North: 1897705.23 ft  
 East: 1171851.95 ft  
 Station: 1611+67.44  
 Offset: 53.9743 RT

Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)	Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)	
	515.2	Very dense, gray SILTY LOAM, little to some gravel and cobbles									--HARD DRILLING-- --Possible Cobbles--							
				85	23	13 31 41	NP	14				--HARD DRILLING-- --Possible Cobbles--	105	27	50/4	NP	11	
				90	24	18 35 48	9.35 S	10										
				95	25	20 36 50/4	9.10 S	13										
				100	26	50/5	NR											
	490.0										--ROLLER BIT REFUSAL-- Boring terminated at 107.00 ft							

### GENERAL NOTES

Begin Drilling **09-25-2013** Complete Drilling **09-30-2013**  
 Drilling Contractor **Wang Testing Services** Drill Rig **CME-55 TMR [85%]**  
 Driller **R&J** Logger **A. Tomaras** Checked by **L. Iordache**  
 Drilling Method **2.25" HSA, boring backfilled upon completion**

### WATER LEVEL DATA

While Drilling  **Rotary wash**  
 At Completion of Drilling  **mud in the borehole**  
 Time After Drilling **NA**  
 Depth to Water  **NA**

The stratification lines represent the approximate boundary between soil types; the actual transition may be gradual.



# BORING LOG 21-RWB-03

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WEI Job No.: 1100-04-01

Client: **AECOM**  
 Project: **Circle Interchange Reconstruction**  
 Location: **Section 17, T39N, R14E of 3rd PM**

Datum: NAVD 88  
 Elevation: 591.97 ft  
 North: 1897787.89 ft  
 East: 1171858.64 ft  
 Station: 1612+32.77  
 Offset: 11.8407 RT

Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)	Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)	
		Very stiff to hard, brown CLAY LOAM, trace brick fragments --FILL--			1	3 4 8	3.50 P	11										
					2	5 5 7	3.12 B	14						9	0 0 0	0.33 B	23	
			--3-inch thick, red, crushed Brick--			3	13 8 6	NP	19						10	0 0 2	0.25 B	26
						4	5 5 7	6.56 B	15						11	0 1 2	0.45 B	26
	581.5	Stiff, gray SILTY CLAY, trace gravel			5	2 3 4	1.97 B	23						12	2 2 2	< 0.25 P	25	
	579.0		Very soft to medium stiff, gray CLAY, trace gravel			6	2 1 3	0.57 B	25						13	1 2 2	0.57 B	24
					7	2 1 2	0.49 B	25						14	2 3 3	0.49 B	25	
					8	2 2 2	< 0.25 P	28										

### GENERAL NOTES

### WATER LEVEL DATA

Begin Drilling **09-23-2013** Complete Drilling **09-23-2013**  
 Drilling Contractor **Wang Testing Services** Drill Rig **CME-55 TMR [85%]**  
 Driller **R&J** Logger **A. Tomaras** Checked by **L. lordache**  
 Drilling Method **3.25" HSA, boring backfilled upon completion**

While Drilling  **Rotary wash**  
 At Completion of Drilling  **mud in the borehole**  
 Time After Drilling **NA**  
 Depth to Water  **NA**

The stratification lines represent the approximate boundary between soil types; the actual transition may be gradual.

WANGENGINC 11000401.GPJ WANGENG.GDT 9/14/17



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# BORING LOG 21-RWB-03

WEI Job No.: 1100-04-01

Client: **AECOM**  
 Project: **Circle Interchange Reconstruction**  
 Location: **Section 17, T39N, R14E of 3rd PM**

Datum: NAVD 88  
 Elevation: 591.97 ft  
 North: 1897787.89 ft  
 East: 1171858.64 ft  
 Station: 1612+32.77  
 Offset: 11.8407 RT

Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)	Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)
			45		15	2 3 3	< 0.25 P	27				65		19	15 17 24	4.10 B	27
			50		16	0 2 2	0.41 B	28				70		20	16 17 20	8.53 B	12
	540.2	Very stiff to hard, SILTY CLAY to SILTY CLAY LOAM, trace gravel								520.2	Dense, gray SILT						
			55		17	4 5 8	1.48 B	22				75		21	20 26 23	NP	21
			60		18	14 12 15	3.00 P	16		515.2	Hard, gray SILTY CLAY LOAM, trace gravel			22	19 20 28	8.61 S	14

### GENERAL NOTES

### WATER LEVEL DATA

Begin Drilling **09-23-2013** Complete Drilling **09-23-2013**  
 Drilling Contractor **Wang Testing Services** Drill Rig **CME-55 TMR [85%]**  
 Driller **R&J** Logger **A. Tomaras** Checked by **L. lordache**  
 Drilling Method **3.25" HSA, boring backfilled upon completion**

While Drilling  **Rotary wash**  
 At Completion of Drilling  **mud in the borehole**  
 Time After Drilling **NA**  
 Depth to Water  **NA**

The stratification lines represent the approximate boundary between soil types; the actual transition may be gradual.

WANGENGINC 11000401.GPJ WANGENG.GDT 9/14/17



# BORING LOG 21-RWB-03

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WEI Job No.: 1100-04-01

Client: **AECOM**  
 Project: **Circle Interchange Reconstruction**  
 Location: **Section 17, T39N, R14E of 3rd PM**

Datum: NAVD 88  
 Elevation: 591.97 ft  
 North: 1897787.89 ft  
 East: 1171858.64 ft  
 Station: 1612+32.77  
 Offset: 11.8407 RT

Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)	Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)	
	510.2	Very dense, gray SILT --HARD DRILLING--	85		23	31 32 50/5	NP	15		490.2	Very dense, weathered DOLOSTONE fragments --WEATHERED BEDROCK--	27		27	50/1	NP		
	505.2	Very dense, gray SILTY LOAM, trace gravel	90		24	23 33 29	6.81 S	21		487.5	--ROLLER BIT REFUSAL--							
			95		25	66/6 <del>44/3</del>	NP	15		487.0	DOLI	105						
	495.2	--HARD DRILLING-- Very dense, brown SANDY GRAVEL  --possibly underpressure groundwater bearing--	100		26	30 70/6	NP	6			Boring terminated at 104.50 ft							

### GENERAL NOTES

### WATER LEVEL DATA

Begin Drilling **09-23-2013** Complete Drilling **09-23-2013**  
 Drilling Contractor **Wang Testing Services** Drill Rig **CME-55 TMR [85%]**  
 Driller **R&J** Logger **A. Tomaras** Checked by **L. lordache**  
 Drilling Method **3.25" HSA, boring backfilled upon completion**

While Drilling  **Rotary wash**  
 At Completion of Drilling  **mud in the borehole**  
 Time After Drilling **NA**  
 Depth to Water  **NA**

The stratification lines represent the approximate boundary between soil types; the actual transition may be gradual.

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# BORING LOG 21-RWB-04

WEI Job No.: 1100-04-01

Client: **AECOM**  
 Project: **Circle Interchange Reconstruction**  
 Location: **Section 17, T39N, R14E of 3rd PM**

Datum: NAVD 88  
 Elevation: 587.85 ft  
 North: 1897850.59 ft  
 East: 1171897.08 ft  
 Station: 1613+02.29  
 Offset: 21.9615 RT

Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)	Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)
	587.45	-inch thick, black SILTY LOAM --TOPSOIL-- Very stiff to hard, brown SILTY CLAY LOAM, trace gravel --FILL--			1	5 6 7	4.51 S	16						9	1 1 2	0.16 B	25
			5		2	5 3 5	3.50 P	18				25		10	1 1 1	0.16 B	27
	582.4	Stiff, brown and gray SILTY CLAY, trace gravel			3	3 3 3	1.97 B	22						11	1 2 2	0.33 B	20
	579.9	Very soft to medium stiff, brown CLAY to SILTY CLAY, trace gravel			4	1 1 2	0.57 B	23						12	1 1 2	0.16 B	23
					5	1 1 2	0.41 B	25									
			15		6	1 1 2	0.33 B	24				35		13	1 2 3	0.66 B	21
					7	1 1 2	0.33 B	23									
			20		8	0 1 1	0.16 B	26				40		14	2 2 2	0.41 B	24

### GENERAL NOTES

Begin Drilling **09-23-2013** Complete Drilling **09-23-2013**  
 Drilling Contractor **K&S** Drill Rig **D-120 TMR**  
 Driller **R&E** Logger **F. Bozga** Checked by **L. lordache**  
 Drilling Method **4.25" HSA, boring backfilled upon completion**

### WATER LEVEL DATA

While Drilling  **Rotary wash**  
 At Completion of Drilling  **mud in the borehole**  
 Time After Drilling **NA**  
 Depth to Water  **NA**

The stratification lines represent the approximate boundary between soil types; the actual transition may be gradual.

WANGENGINC 11000401.GPJ WANGENG.GDT 9/14/17





# BORING LOG 21-RWB-04

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WEI Job No.: 1100-04-01

Client: **AECOM**  
 Project: **Circle Interchange Reconstruction**  
 Location: **Section 17, T39N, R14E of 3rd PM**

Datum: NAVD 88  
 Elevation: 587.85 ft  
 North: 1897850.59 ft  
 East: 1171897.08 ft  
 Station: 1613+02.29  
 Offset: 21.9615 RT

Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)	Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)
			45		15	1 2 3	0.33 B	26				65		19	26 25 30	5.66 S	13
			50		16	3 5 8	0.66 B	20			--HARD DRILLING-- --Possible Cobbles--	70		20	38 50/5"	NP	15
	536.1	Very stiff, gray SILTY CLAY, trace gravel	55		17	4 7 11	3.28 B	22				75		21	12 19 29	8.04 S	13
	531.1	Dense to very dense, gray SILTY LOAM to SILTY CLAY LOAM, trace to little gravel	60		18	16 26 38	6.23 S	14				80		22	22 50/5"	NP	11

### GENERAL NOTES

### WATER LEVEL DATA

Begin Drilling **09-23-2013** Complete Drilling **09-23-2013**  
 Drilling Contractor **K&S** Drill Rig **D-120 TMR**  
 Driller **R&E** Logger **F. Bozga** Checked by **L. lordache**  
 Drilling Method **4.25" HSA, boring backfilled upon completion**

While Drilling  **Rotary wash**  
 At Completion of Drilling  **mud in the borehole**  
 Time After Drilling **NA**  
 Depth to Water  **NA**

The stratification lines represent the approximate boundary between soil types; the actual transition may be gradual.

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# BORING LOG 21-RWB-04

WEI Job No.: 1100-04-01

Client: **AECOM**  
 Project: **Circle Interchange Reconstruction**  
 Location: **Section 17, T39N, R14E of 3rd PM**

Datum: NAVD 88  
 Elevation: 587.85 ft  
 North: 1897850.59 ft  
 East: 1171897.08 ft  
 Station: 1613+02.29  
 Offset: 21.9615 RT

Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)	Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)
			85		23	19 25 31	NP	10									
			90		24	50/5"	NP	11									
	496.6	Dense, gray SANDY GRAVEL															
			95		25	11 21 19	NP	13									
	492.9	Boring terminated at 95.00 ft															

### GENERAL NOTES

Begin Drilling **09-23-2013** Complete Drilling **09-23-2013**  
 Drilling Contractor **K&S** Drill Rig **D-120 TMR**  
 Driller **R&E** Logger **F. Bozga** Checked by **L. lordache**  
 Drilling Method **4.25" HSA, boring backfilled upon completion**

### WATER LEVEL DATA

While Drilling  **Rotary wash**  
 At Completion of Drilling  **mud in the borehole**  
 Time After Drilling **NA**  
 Depth to Water  **NA**

The stratification lines represent the approximate boundary between soil types; the actual transition may be gradual.



# BORING LOG 21-RWB-05

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WEI Job No.: 1100-04-01

Client **AECOM**  
 Project **Circle Interchange Reconstruction**  
 Location **Section 17, T39N, R14E of 3rd PM**

Datum: NAVD 88  
 Elevation: 583.32 ft  
 North: 1897919.78 ft  
 East: 1171915.09 ft  
 Station: 1613+69.21  
 Offset: 25.0245 RT

Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)	Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)
	582.95	5-inch thick, white CRUSHED STONE															
		--FILL--															
		Hard, gray and brown CLAY LOAM, trace gravel			1	6 9 9	6.56 S	15						9	2 2 4	0.82 B	23
		--FILL--															
	580.3	Medium stiff to stiff, gray SILTY CLAY, trace gravel			2	2 2 2	0.82 B	20				25		10	2 3 3	0.74 B	23
					3	1 3 3	1.23 B	17						11	2 2 3	0.66 B	24
	575.3	Soft to medium stiff, gray CLAY to SILTY CLAY, trace gravel			4	0 2 1	0.41 B	25						12	3 4 6	0.66 B	23
					5	0 0 0	0.41 B	26									
					6	0 0 2	0.57 B	22						13	2 3 3	0.49 B	25
					7	2 3 2	0.66 B	22									
					8	0 2 3	0.74 B	24						14	3 3 4	0.41 B	23

### GENERAL NOTES

Begin Drilling **09-24-2013** Complete Drilling **09-25-2013**  
 Drilling Contractor **Wang Testing Services** Drill Rig **CME-55 TMR [85%]**  
 Driller **R&J** Logger **A. Tomaras** Checked by **L. lordache**  
 Drilling Method **2.25" HSA to 10', mud rotary thereafter, boring backfilled upon completion**

### WATER LEVEL DATA

While Drilling  **Rotary wash**  
 At Completion of Drilling  **mud in the borehole**  
 Time After Drilling **NA**  
 Depth to Water  **NA**

The stratification lines represent the approximate boundary between soil types; the actual transition may be gradual.

WANGENGINC 11000401.GPJ WANGENG.GDT 9/14/17



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# BORING LOG 21-RWB-05

WEI Job No.: 1100-04-01

Client: **AECOM**  
 Project: **Circle Interchange Reconstruction**  
 Location: **Section 17, T39N, R14E of 3rd PM**

Datum: NAVD 88  
 Elevation: 583.32 ft  
 North: 1897919.78 ft  
 East: 1171915.09 ft  
 Station: 1613+69.21  
 Offset: 25.0245 RT

Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)	Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)
	541.6	Stiff to hard, gray SILTY CLAY LOAM, trace gravel	45	X	15	2 4 8	1.23 B	18				65	X	19	10 16 21	6.81 S	14
			50	X	16	6 12 18	4.26 B	15				70	X	20	15 25 30	9.02 S	11
	531.6	Gray, coarse SAND															
	529.6	Hard, gray SILTY CLAY LOAM, trace gravel	55	X	17	13 15 21	5.66 B	14				75	X	21	41 <del>60/3"</del>	NP	10
			60	X	18	16 24 31	7.13 S	11				80	X	22	34 45 <del>20/2"</del>	8.69 S	10

### GENERAL NOTES

### WATER LEVEL DATA

Begin Drilling **09-24-2013** Complete Drilling **09-25-2013**  
 Drilling Contractor **Wang Testing Services** Drill Rig **CME-55 TMR [85%]**  
 Driller **R&J** Logger **A. Tomaras** Checked by **L. lordache**  
 Drilling Method **2.25" HSA to 10', mud rotary thereafter, boring backfilled upon completion**

While Drilling  **Rotary wash**  
 At Completion of Drilling  **mud in the borehole**  
 Time After Drilling **NA**  
 Depth to Water  **NA**

The stratification lines represent the approximate boundary between soil types; the actual transition may be gradual.

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# BORING LOG 21-RWB-05

WEI Job No.: 1100-04-01

Client: **AECOM**  
 Project: **Circle Interchange Reconstruction**  
 Location: **Section 17, T39N, R14E of 3rd PM**

Datum: NAVD 88  
 Elevation: 583.32 ft  
 North: 1897919.78 ft  
 East: 1171915.09 ft  
 Station: 1613+69.21  
 Offset: 25.0245 RT

Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)	Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)
	501.6	Very dense, gray SANDY LOAM, trace gravel								482.3	--WEATHERED BEDROCK--						
										481.3	--ROLLER BIT REFUSAL--						
			85	X	23	78/6" 22/1"	NP	9			Boring terminated at 102.00 ft	105					
		--HARD DRILLING-- --Possible Cobbles--															
			90	X	24	64 45/6"	NP	13				110					
	491.6	Very dense, gray GRAVELLY SILTY LOAM, trace to some cobbles															
				95	X	25	100/6"	1.31 S	13				115				
		--HARD DRILLING-- --Possible Cobbles--															
			100	X	26	64 40/2"	0.49 S	9				120					

### GENERAL NOTES

Begin Drilling **09-24-2013** Complete Drilling **09-25-2013**  
 Drilling Contractor **Wang Testing Services** Drill Rig **CME-55 TMR [85%]**  
 Driller **R&J** Logger **A. Tomaras** Checked by **L. lordache**  
 Drilling Method **2.25" HSA to 10', mud rotary thereafter, boring backfilled upon completion**

### WATER LEVEL DATA

While Drilling  **Rotary wash**  
 At Completion of Drilling  **mud in the borehole**  
 Time After Drilling **NA**  
 Depth to Water  **NA**

The stratification lines represent the approximate boundary between soil types; the actual transition may be gradual.

WANGENGINC 11000401.GPJ WANGENG.GDT 9/14/17



# BORING LOG 1705-B-06A

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WEI Job No.: 1100-04-01

Client: **AECOM**  
 Project: **Circle Interchange Reconstruction**  
 Location: **Section 17, T39N, R14E of 3rd PM**

Datum: NAVD 88  
 Elevation: 591.98 ft  
 North: 1897749.88 ft  
 East: 1171805.18 ft  
 Station: 1827+13.77  
 Offset: 38.2558 RT

Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)	Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)	
	591.5	6-inch thick, black SILTY LOAM --TOPSOIL-- Medium dense to dense, brown LOAM, little gravel and brick fragments --FILL--			1	9 17 13	NP	6							0 0 1	0.08 B	26	
			5		2	2 15 9	NP	14				25		10	0 0 2	0.25 B	26	
	586.5	Very stiff, gray SILTY CLAY LOAM, trace gravel			3	2 3 4	2.95 B	17						11	0 0 3	0.25 B	28	
			10		4	2 4 4	2.54 B	22				30		12	0 1 2	0.57 B	23	
	581.5	Very soft to medium stiff, gray CLAY to SILTY CLAY, trace gravel			5	3 3 3	< 0.25 P	21										
			15		6	0 2 2	0.41 B	24				35		13	0 1 2	0.50 P	21	
					7	0 1 1	0.25 B	22										
			20		8	0 0 2	0.41 B	26				40		14	0 3 2	0.49 B	24	

### GENERAL NOTES

### WATER LEVEL DATA

Begin Drilling **07-25-2013** Complete Drilling **07-26-2013**  
 Drilling Contractor **Wang Testing Services** Drill Rig **CME-55 TMR [85%]**  
 Driller **R&J** Logger **A. Tomaras** Checked by **C. Marin**  
 Drilling Method **2.25" SSA to 10', mud rotary thereafter, boring backfilled upon completion**

While Drilling  **Rotary wash**  
 At Completion of Drilling  **mud in the borehole**  
 Time After Drilling **NA**  
 Depth to Water  **NA**

The stratification lines represent the approximate boundary between soil types; the actual transition may be gradual.

WANGENGINC 11000401.GPJ WANGENG.GDT 9/14/17



# BORING LOG 1705-B-06A

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WEI Job No.: 1100-04-01

Client: **AECOM**  
 Project: **Circle Interchange Reconstruction**  
 Location: **Section 17, T39N, R14E of 3rd PM**

Datum: NAVD 88  
 Elevation: 591.98 ft  
 North: 1897749.88 ft  
 East: 1171805.18 ft  
 Station: 1827+13.77  
 Offset: 38.2558 RT

Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)	Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)
			45		15	0 2 2	0.41 B	25				65		19	10 12 19	4.92 B	18
			50		16	1 1 2	0.33 B	25		525.2	Very stiff, gray CLAY, trace gravel	70		20	6 9 10	2.54 B	24
	540.2	Very stiff to hard, gray SILTY CLAY, trace gravel	55		17	6 7 13	3.36 B	19		518.2	Loose, gray SILT --Wet--	75		21	2 4 5	NP	19
			60		18	13 18 21	4.84 B	14		515.2	Hard, gray SILTY CLAY, trace gravel	80		22	13 20 28	8.94 S	13

### GENERAL NOTES

Begin Drilling **07-25-2013** Complete Drilling **07-26-2013**  
 Drilling Contractor **Wang Testing Services** Drill Rig **CME-55 TMR [85%]**  
 Driller **R&J** Logger **A. Tomaras** Checked by **C. Marin**  
 Drilling Method **2.25" SSA to 10', mud rotary thereafter, boring backfilled upon completion**

### WATER LEVEL DATA

While Drilling  **Rotary wash**  
 At Completion of Drilling  **mud in the borehole**  
 Time After Drilling **NA**  
 Depth to Water  **NA**

The stratification lines represent the approximate boundary between soil types; the actual transition may be gradual.

WANGENGINC 11000401.GPJ WANGENG.GDT 9/14/17



# BORING LOG 1705-B-06A

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WEI Job No.: 1100-04-01

Client: **AECOM**  
 Project: **Circle Interchange Reconstruction**  
 Location: **Section 17, T39N, R14E of 3rd PM**

Datum: NAVD 88  
 Elevation: 591.98 ft  
 North: 1897749.88 ft  
 East: 1171805.18 ft  
 Station: 1827+13.77  
 Offset: 38.2558 RT

Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)	Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)		
	510.2	Very dense to hard, gray SILTY LOAM to SILTY CLAY LOAM, trace gravel								490.0	Strong, fair to good rock quality, light gray, fresh, joint breaks with little to no infill, slightly vuggy DOLOSTONE with stylolites  --Run 1 - RECOVERY=100%-- --RQD (top 5ft)=45%-- --RQD= (10ft)=62%--			26	60/6	NP	17		
	85				23	33 46 50/6	4.50 P	10											
	90		--HARD DRILLING--  --Possible Cobbles--			24	13 20 26	8.61 S	11					110		1			NP
	499.0	Very dense, SANDY GRAVEL, with rock fragments								480.0	Boring terminated at 112.00 ft								
	95					25	21 24 29	NP	11				115						
	100	--HARD DRILLING-- --Possible Cobbles--										120							

### GENERAL NOTES

Begin Drilling **07-25-2013** Complete Drilling **07-26-2013**  
 Drilling Contractor **Wang Testing Services** Drill Rig **CME-55 TMR [85%]**  
 Driller **R&J** Logger **A. Tomaras** Checked by **C. Marin**  
 Drilling Method **2.25" SSA to 10', mud rotary thereafter, boring backfilled upon completion**

### WATER LEVEL DATA

While Drilling  **Rotary wash**  
 At Completion of Drilling  **mud in the borehole**  
 Time After Drilling **NA**  
 Depth to Water  **NA**

The stratification lines represent the approximate boundary between soil types; the actual transition may be gradual.

WANGENGINC 11000401.GPJ WANGENG.GDT 9/14/17





# BORING LOG 1710-B-01

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WEI Job No.: 1100-04-01

Client **AECOM**  
 Project **Circle Interchange Reconstruction**  
 Location **Section 17, T39N, R14E of 3rd PM**

Datum: NAVD 88  
 Elevation: 589.38 ft  
 North: 1897814.39 ft  
 East: 1171841.78 ft  
 Station: 1704+98.15  
 Offset: 72.7367 LT

Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)	Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)	
	589.05	5-inch thick, brown SILTY CLAY LOAM --TOPSOIL-- Medium dense, brown SILTY LOAM, trace gravel --FILL--			1	5 7 8	NP	13						9	1 2 2	0.41 B	23	
	586.4	Very stiff, brown SILTY CLAY LOAM, trace gravel, brick fragments --FILL--			2	5 7 5	2.54	15				25		10	1 1 2	0.25 B	22	
	583.9	Dense, brown, SANDY LOAM, trace gravel, brick fragments --FILL--			3	10 16 17	NP	22						11	1 1 2	0.41 B	24	
	581.4	Stiff, gray SILTY CLAY LOAM, trace gravel			4	3 3 4	1.07 B	22						12	1 2 2	0.41 B	24	
	578.9	Soft to medium stiff, CLAY to SILTY CLAY, trace gravel			5	1 1 2	0.33 B	25										
					6	1 1 2	0.33 B	24						13	1 1 3	0.49 B	23	
					7	1 1 2	0.41 B	26										
					8	1 1 2	0.49 B	24						14	1 2 3	0.33 B	24	

### GENERAL NOTES

Begin Drilling **09-24-2013** Complete Drilling **09-25-2013**  
 Drilling Contractor **K&S** Drill Rig **D-120 TMR**  
 Driller **R&E** Logger **F. Bozga** Checked by **L. lordache**  
 Drilling Method **4.25" HSA, boring backfilled upon completion**

### WATER LEVEL DATA

While Drilling  $\nabla$  **85.00 ft**  
 At Completion of Drilling  $\nabla$  **90.00 ft**  
 Time After Drilling **NA**  
 Depth to Water  $\nabla$  **NA**

The stratification lines represent the approximate boundary between soil types; the actual transition may be gradual.

WANGENGINC 11000401.GPJ WANGENG.GDT 9/14/17



# BORING LOG 1710-B-01

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WEI Job No.: 1100-04-01

Client: **AECOM**  
 Project: **Circle Interchange Reconstruction**  
 Location: **Section 17, T39N, R14E of 3rd PM**

Datum: NAVD 88  
 Elevation: 589.38 ft  
 North: 1897814.39 ft  
 East: 1171841.78 ft  
 Station: 1704+98.15  
 Offset: 72.7367 LT

Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)	Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)
			45		15	1 2 3	0.41 B	25				65		19	23 39 37	NP	7
			50		16	2 3 5	0.66 B	20				70		20	12 20 20	NP	10
	537.6	Very stiff, gray SILTY CLAY, trace gravel	55		17	4 7 12	3.94 B	20				75		21	13 20 37	NP	11
	532.6	Dense to very dense, gray SILTY LOAM, trace gravel	60		18	11 14 20	NP	11				80		22	10 22 40	NP	15

### GENERAL NOTES

Begin Drilling **09-24-2013** Complete Drilling **09-25-2013**  
 Drilling Contractor **K&S** Drill Rig **D-120 TMR**  
 Driller **R&E** Logger **F. Bozga** Checked by **L. lordache**  
 Drilling Method **4.25" HSA, boring backfilled upon completion**

### WATER LEVEL DATA

While Drilling  $\nabla$  **85.00 ft**  
 At Completion of Drilling  $\nabla$  **90.00 ft**  
 Time After Drilling **NA**  
 Depth to Water  $\nabla$  **NA**

The stratification lines represent the approximate boundary between soil types; the actual transition may be gradual.

WANGENGINC 11000401.GPJ WANGENG.GDT 9/14/17



# BORING LOG 1710-B-01

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WEI Job No.: 1100-04-01

Client: **AECOM**  
 Project: **Circle Interchange Reconstruction**  
 Location: **Section 17, T39N, R14E of 3rd PM**

Datum: NAVD 88  
 Elevation: 589.38 ft  
 North: 1897814.39 ft  
 East: 1171841.78 ft  
 Station: 1704+98.15  
 Offset: 72.7367 LT

Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)	Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)
	502.6	Very dense, gray SILT	85		23	17 25 37	NP	9									
	497.6	Dense, gray GRAVELLY SAND	90		24	13 50/2"	NP	26									
	492.4	--HARD DRILLING-- Very dense, gray DOLOSTONE fragments	95		25	10 18 20	NP	14									
	491.2	--WEATHERED BEDROCK-- --AUGER REFUSAL-- Boring terminated at 98.20 ft	100		26	50/2"	NP	9									

### GENERAL NOTES

Begin Drilling **09-24-2013** Complete Drilling **09-25-2013**  
 Drilling Contractor **K&S** Drill Rig **D-120 TMR**  
 Driller **R&E** Logger **F. Bozga** Checked by **L. lordache**  
 Drilling Method **4.25" HSA, boring backfilled upon completion**

### WATER LEVEL DATA

While Drilling  $\nabla$  **85.00 ft**  
 At Completion of Drilling  $\blacktriangledown$  **90.00 ft**  
 Time After Drilling **NA**  
 Depth to Water  $\nabla$  **NA**

The stratification lines represent the approximate boundary between soil types; the actual transition may be gradual.

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# BORING LOG VST-06

WEI Job No.: 1100-04-01

Client: **AECOM**  
 Project: **Circle Interchange Reconstruction**  
 Location: **Section 17, T39N, R14E of 3rd PM**

Datum: NAVD 88  
 Elevation: 585.69 ft  
 North: 1898109.29 ft  
 East: 1171902.18 ft  
 Station: 1103+77.81  
 Offset: 27.3835 RT

Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)	Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)
	580.2	Hard, brown SILTY CLAY LOAM, trace gravel --FILL--	5		1	7 6 6	4.50 P	16			--In-Situ Vane Shear, 20.5 feet-- --S <sub>u undis</sub> = 775.4 psf-- --S <sub>u remold</sub> = 360.4 psf-- --Sensitivity = 2.2--	5		5			
	576.7	Soft, gray SILTY CLAY LOAM	25		2	1 2 3	0.41 B	23			--In-Situ Vane Shear, 23.0 feet-- --S <sub>u undis</sub> = 600.6 psf-- --S <sub>u remold</sub> = 305.8 psf-- --Sensitivity = 2.0--	6		6			
			30		7						--In-Situ Vane Shear, 25.5 feet-- --S <sub>u undis</sub> = 578.8 psf-- --S <sub>u remold</sub> = 316.7 psf-- --Sensitivity = 1.8--	7		7			
			35		8						--In-Situ Vane Shear, 28.0 feet-- --S <sub>u undis</sub> = 611.6 psf-- --S <sub>u remold</sub> = 338.5 psf-- --Sensitivity = 1.8--	8		8			
		--In-Situ Vane Shear, 10.5 feet-- --S <sub>u undis</sub> = 972.0 psf-- --S <sub>u remold</sub> = 611.6 psf-- --Sensitivity = 1.6--	10		1						--In-Situ Vane Shear, 30.5 feet-- --S <sub>u undis</sub> = 786.3 psf-- --S <sub>u remold</sub> = 382.2 psf-- --Sensitivity = 2.1--	9		9			
		--In-Situ Vane Shear, 13.0 feet-- --S <sub>u undis</sub> = 982.9 psf-- --S <sub>u remold</sub> = 589.7 psf-- --Sensitivity = 1.7--	15		2						--In-Situ Vane Shear, 33.0 feet-- --S <sub>u undis</sub> = 698.9 psf-- --S <sub>u remold</sub> = 404.1 psf-- --Sensitivity = 1.7--	10		10			
		--In-Situ Vane Shear, 15.5 feet-- --S <sub>u undis</sub> = 873.7 psf-- --S <sub>u remold</sub> = 513.3 psf-- --Sensitivity = 1.7--	20		3						--In-Situ Vane Shear, 35.5 feet-- --S <sub>u undis</sub> = 808.1 psf-- --S <sub>u remold</sub> = 502.4 psf-- --Sensitivity = 1.6--	11		11			
		--In-Situ Vane Shear, 18.0 feet-- --S <sub>u undis</sub> = 928.3 psf-- --S <sub>u remold</sub> = 360.4 psf-- --Sensitivity = 2.6--	25		4						--In-Situ Vane Shear, 38.0 feet-- --S <sub>u undis</sub> = 982.9 psf-- --S <sub>u remold</sub> = 546.0 psf-- --Sensitivity = 1.8--	12		12			

### GENERAL NOTES

Begin Drilling **12-09-2015** Complete Drilling **12-14-2015**  
 Drilling Contractor **Wang Testing Services** Drill Rig **CME-55 TMR [85%]**  
 Driller **R&N** Logger **F. Bozga** Checked by **A. Kurnia**  
 Drilling Method **2.25" HSA to 10', mud rotary thereafter, boring backfilled upon completion**

### WATER LEVEL DATA

While Drilling  **Rotary wash**  
 At Completion of Drilling  **mud in the borehole**  
 Time After Drilling **NA**  
 Depth to Water  **NA**

The stratification lines represent the approximate boundary between soil types; the actual transition may be gradual.

WANGENGINC 11000401.GPJ WANGENG.GDT 9/14/17



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# BORING LOG VST-06

WEI Job No.: 1100-04-01

Client: **AECOM**  
 Project: **Circle Interchange Reconstruction**  
 Location: **Section 17, T39N, R14E of 3rd PM**

Datum: NAVD 88  
 Elevation: 585.69 ft  
 North: 1898109.29 ft  
 East: 1171902.18 ft  
 Station: 1103+77.81  
 Offset: 27.3835 RT

Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)	Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)
		--In-Situ Vane Shear, 40.5 feet-- -- $S_{u\ undis}$ = 906.4 psf-- -- $S_{u\ remold}$ = 524.2 psf-- --Sensitivity = 1.7--	40.5	VS	13	VS											
	542.2	--In-Situ Vane Shear, 43.0 feet-- -- $S_{u\ undis}$ = 677.1 psf-- -- $S_{u\ remold}$ = 393.1 psf-- --Sensitivity = 1.7-- Boring terminated at 43.50 ft	43.0	VS	14	VS											
			45														
			50														
			55														
			60														

### GENERAL NOTES

### WATER LEVEL DATA

Begin Drilling **12-09-2015** Complete Drilling **12-14-2015**  
 Drilling Contractor **Wang Testing Services** Drill Rig **CME-55 TMR [85%]**  
 Driller **R&N** Logger **F. Bozga** Checked by **A. Kurnia**  
 Drilling Method **2.25" HSA to 10', mud rotary thereafter, boring backfilled upon completion**

While Drilling  $\nabla$  **Rotary wash**  
 At Completion of Drilling  $\nabla$  **mud in the borehole**  
 Time After Drilling **NA**  
 Depth to Water  $\nabla$  **NA**

The stratification lines represent the approximate boundary between soil types; the actual transition may be gradual.



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# BORING LOG VST-06

WEI Job No.: 1100-04-01

Client: **AECOM**  
 Project: **Circle Interchange Reconstruction**  
 Location: **Section 17, T39N, R14E of 3rd PM**

Datum: NAVD 88  
 Elevation: 585.69 ft  
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 Station: 1103+77.81  
 Offset: 27.3835 RT

Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)	Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)
	580.2	Hard, brown SILTY CLAY LOAM, trace gravel --FILL--	5		1	7 6 6	4.50 P	16			--In-Situ Vane Shear, 20.5 feet-- --S <sub>u undis</sub> = 775.4 psf-- --S <sub>u remold</sub> = 360.4 psf-- --Sensitivity = 2.2--	5		5			
	576.7	Soft, gray SILTY CLAY LOAM	25		2	1 2 3	0.41 B	23			--In-Situ Vane Shear, 23.0 feet-- --S <sub>u undis</sub> = 600.6 psf-- --S <sub>u remold</sub> = 305.8 psf-- --Sensitivity = 2.0--	6		6			
			30								--In-Situ Vane Shear, 25.5 feet-- --S <sub>u undis</sub> = 578.8 psf-- --S <sub>u remold</sub> = 316.7 psf-- --Sensitivity = 1.8--	7		7			
			10								--In-Situ Vane Shear, 28.0 feet-- --S <sub>u undis</sub> = 611.6 psf-- --S <sub>u remold</sub> = 338.5 psf-- --Sensitivity = 1.8--	8		8			
		--In-Situ Vane Shear, 10.5 feet-- --S <sub>u undis</sub> = 972.0 psf-- --S <sub>u remold</sub> = 611.6 psf-- --Sensitivity = 1.6--	15		1						--In-Situ Vane Shear, 30.5 feet-- --S <sub>u undis</sub> = 786.3 psf-- --S <sub>u remold</sub> = 382.2 psf-- --Sensitivity = 2.1--	9		9			
		--In-Situ Vane Shear, 13.0 feet-- --S <sub>u undis</sub> = 982.9 psf-- --S <sub>u remold</sub> = 589.7 psf-- --Sensitivity = 1.7--	35		2						--In-Situ Vane Shear, 33.0 feet-- --S <sub>u undis</sub> = 698.9 psf-- --S <sub>u remold</sub> = 404.1 psf-- --Sensitivity = 1.7--	10		10			
		--In-Situ Vane Shear, 15.5 feet-- --S <sub>u undis</sub> = 873.7 psf-- --S <sub>u remold</sub> = 513.3 psf-- --Sensitivity = 1.7--	20		3						--In-Situ Vane Shear, 35.5 feet-- --S <sub>u undis</sub> = 808.1 psf-- --S <sub>u remold</sub> = 502.4 psf-- --Sensitivity = 1.6--	11		11			
		--In-Situ Vane Shear, 18.0 feet-- --S <sub>u undis</sub> = 928.3 psf-- --S <sub>u remold</sub> = 360.4 psf-- --Sensitivity = 2.6--			4						--In-Situ Vane Shear, 38.0 feet-- --S <sub>u undis</sub> = 982.9 psf-- --S <sub>u remold</sub> = 546.0 psf-- --Sensitivity = 1.8--	12		12			

### GENERAL NOTES

Begin Drilling **12-09-2015** Complete Drilling **12-14-2015**  
 Drilling Contractor **Wang Testing Services** Drill Rig **CME-55 TMR [85%]**  
 Driller **R&N** Logger **F. Bozga** Checked by **A. Kurnia**  
 Drilling Method **2.25" HSA to 10', mud rotary thereafter, boring backfilled upon completion**

### WATER LEVEL DATA

While Drilling  **Rotary wash**  
 At Completion of Drilling  **mud in the borehole**  
 Time After Drilling **NA**  
 Depth to Water  **NA**

The stratification lines represent the approximate boundary between soil types; the actual transition may be gradual.

WANGENGINC 11000401.GPJ WANGENG.GDT 9/13/17



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 Lombard, IL 60148  
 Telephone: 630 953-9928  
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# BORING LOG VST-06

WEI Job No.: 1100-04-01

Client: **AECOM**  
 Project: **Circle Interchange Reconstruction**  
 Location: **Section 17, T39N, R14E of 3rd PM**

Datum: NAVD 88  
 Elevation: 585.69 ft  
 North: 1898109.29 ft  
 East: 1171902.18 ft  
 Station: 1103+77.81  
 Offset: 27.3835 RT

Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)	Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)
		--In-Situ Vane Shear, 40.5 feet-- -- $S_{u\text{ undis}} = 906.4$ psf-- -- $S_{u\text{ remold}} = 524.2$ psf-- --Sensitivity = 1.7--			13	VS											
	542.2	--In-Situ Vane Shear, 43.0 feet-- -- $S_{u\text{ undis}} = 677.1$ psf-- -- $S_{u\text{ remold}} = 393.1$ psf-- --Sensitivity = 1.7--			14	VS											
		Boring terminated at 43.50 ft	45														
			50														
			55														
			60														

### GENERAL NOTES

Begin Drilling **12-09-2015** Complete Drilling **12-14-2015**  
 Drilling Contractor **Wang Testing Services** Drill Rig **CME-55 TMR [85%]**  
 Driller **R&N** Logger **F. Bozga** Checked by **A. Kurnia**  
 Drilling Method **2.25" HSA to 10', mud rotary thereafter, boring backfilled upon completion**

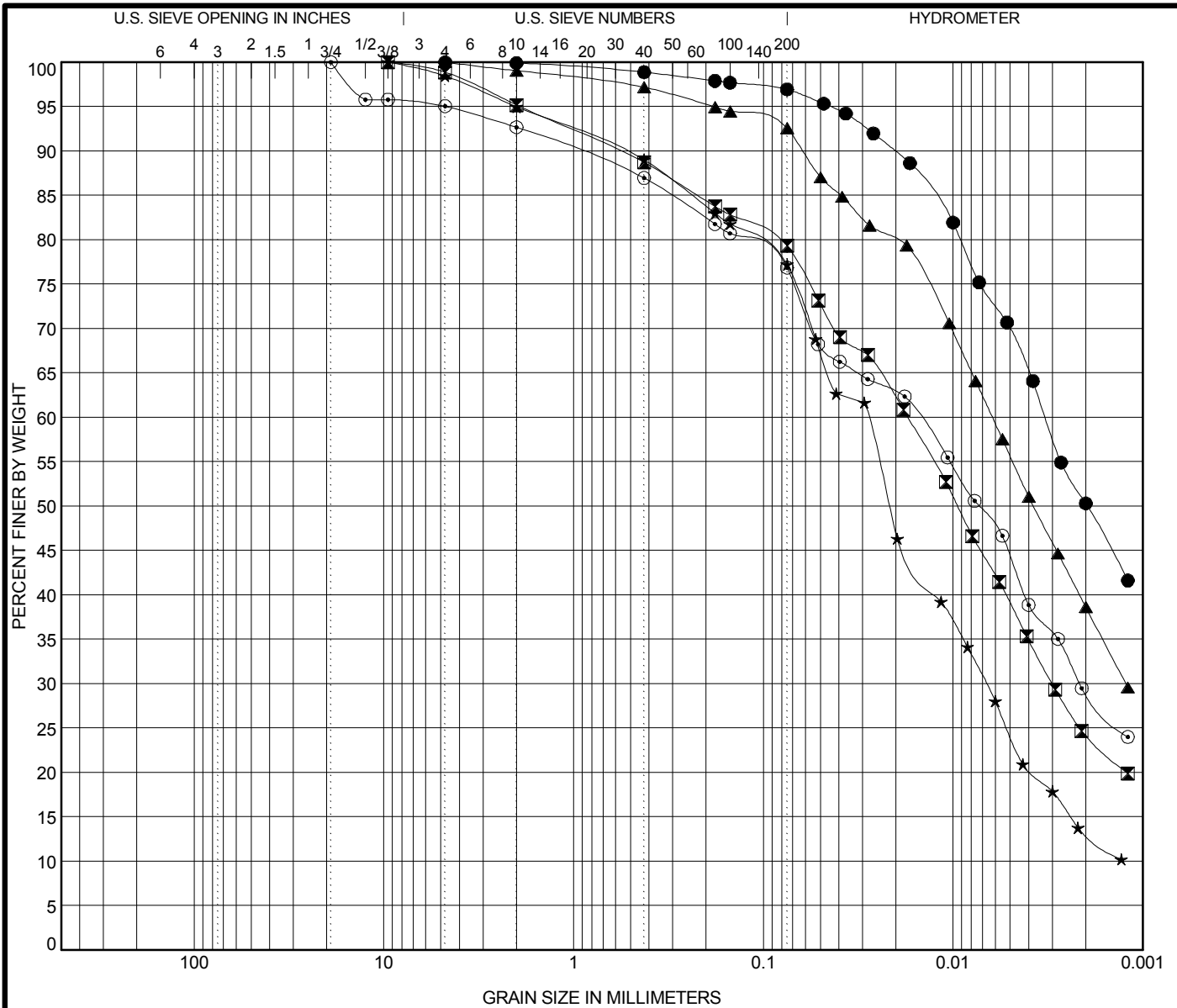
### WATER LEVEL DATA

While Drilling **Rotary wash**  
 At Completion of Drilling **mud in the borehole**  
 Time After Drilling **NA**  
 Depth to Water **NA**

The stratification lines represent the approximate boundary between soil types; the actual transition may be gradual.

## **APPENDIX B**





COBBLES	GRAVEL	SAND		SILT AND CLAY
		coarse	fine	

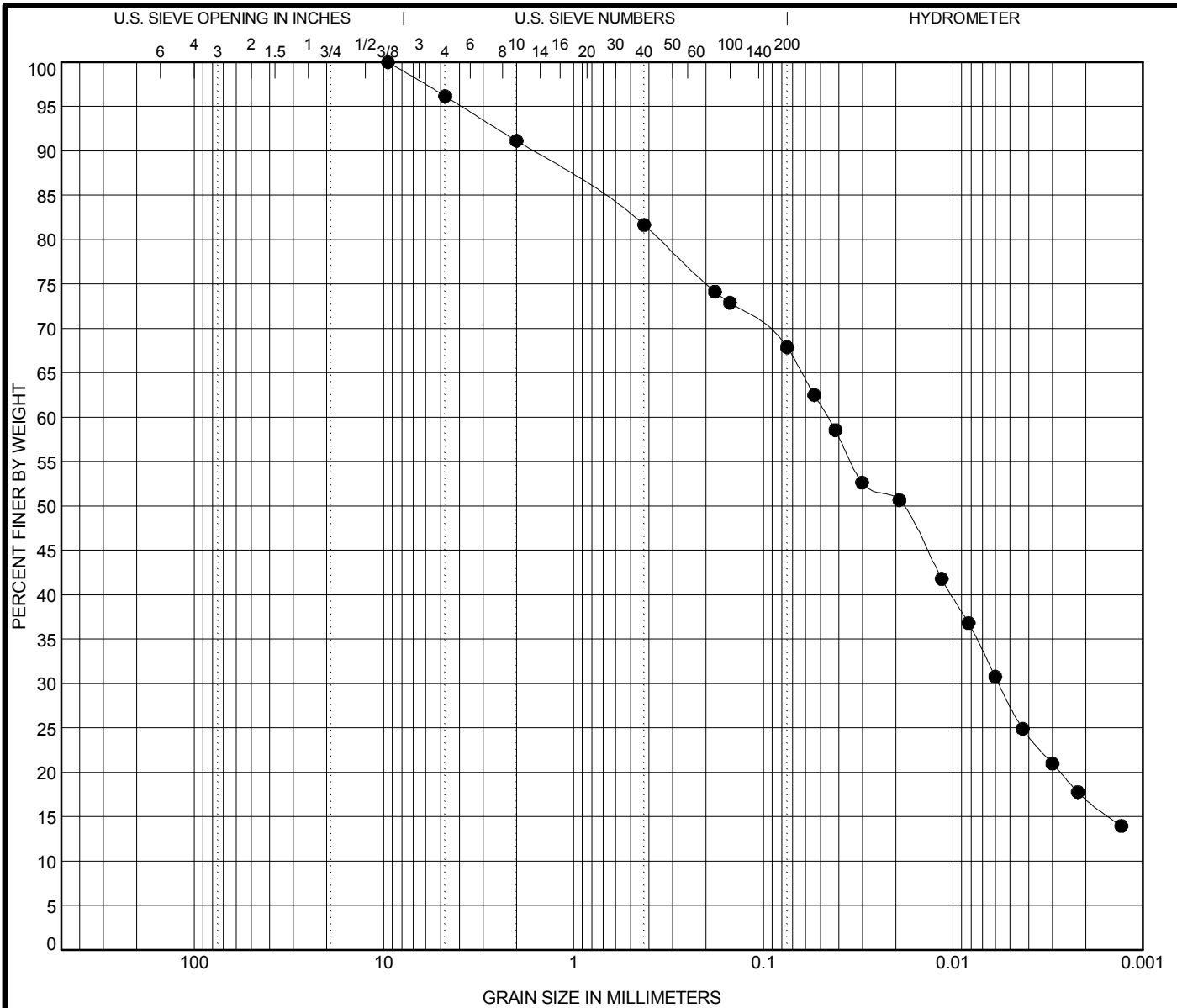
Specimen Identification			IDH Classification					LL	PL	PI	Cc	Cu
●	1705-B-06A#20	68.5 ft	Clay					41	18	23		
☒	20-RWB-01#7	16.0 ft	Silty Clay Loam					31	16	15		
▲	20-RWB-01#16	48.5 ft	Silty Clay					35	18	17		
★	21-RWB-02#24	89.0 ft	Silty Loam					22	14	8		
◎	21-RWB-04#10	23.5 ft	Silty Clay					34	17	17		
Specimen Identification			D100	D60	D30	D10	%Gravel	%Sand	%Silt	%Clay		
●	1705-B-06A#20	68.5 ft	4.75	0.003			0.1	3.0	46.6	50.3		
☒	20-RWB-01#7	16.0 ft	9.5	0.017	0.003		4.8	16.1	54.8	24.3		
▲	20-RWB-01#16	48.5 ft	4.75	0.006	0.001		1.0	6.7	53.8	38.6		
★	21-RWB-02#24	89.0 ft	9.5	0.028	0.007		5.0	18.1	63.8	13.1		
◎	21-RWB-04#10	23.5 ft	19	0.015	0.002		7.3	16.1	47.5	29.0		



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**GRAIN SIZE DISTRIBUTION**  
 Project: Circle Interchange Reconstruction  
 Location: Section 17, T39N, R14E of 3rd PM  
 Number: 1100-04-01

WEI GRAIN SIZE IDH 11000401.GPJ US\_LAB.GDT 9/14/17



COBBLES	GRAVEL	SAND		SILT AND CLAY
		coarse	fine	

Specimen Identification	IDH Classification	LL	PL	PI	Cc	Cu
● 21-RWB-05#18 58.5 ft	<b>Silty Loam</b>	<b>25</b>	<b>15</b>	<b>10</b>		

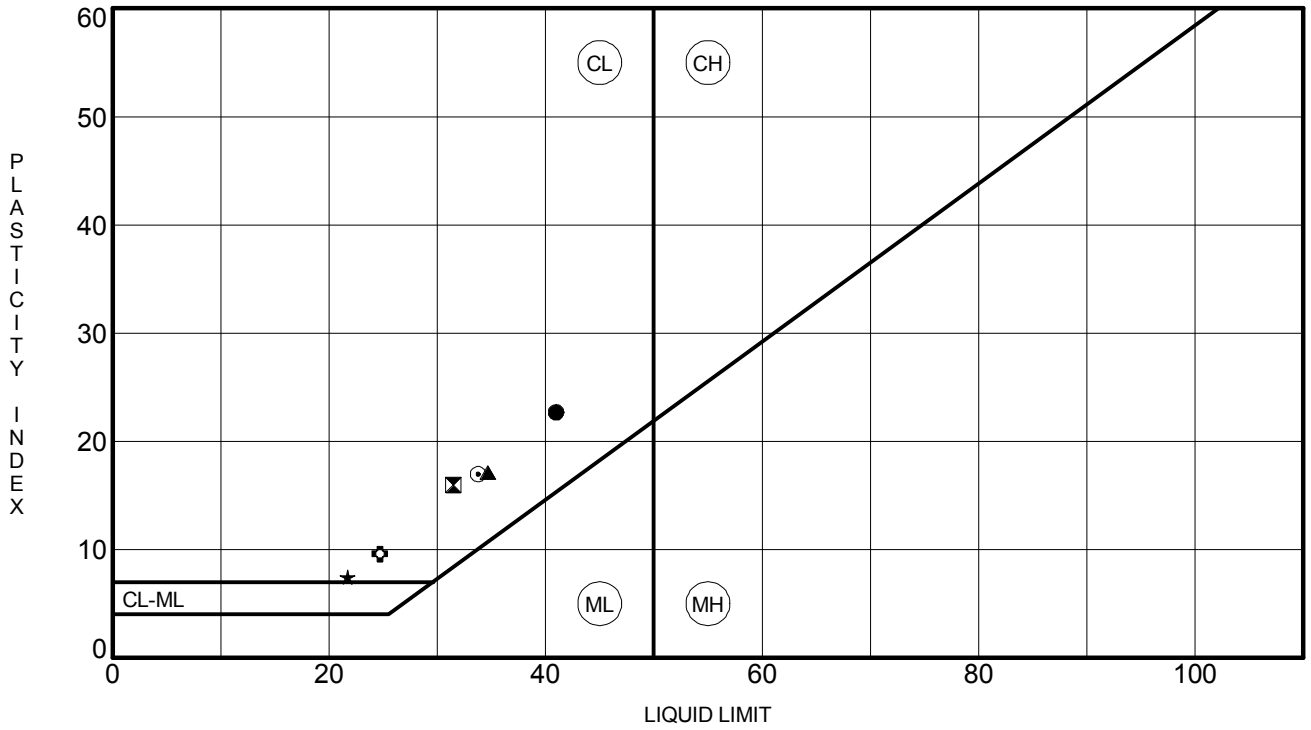
Specimen Identification	D100	D60	D30	D10	%Gravel	%Sand	%Silt	%Clay
● 21-RWB-05#18 58.5 ft	<b>9.5</b>	<b>0.046</b>	<b>0.006</b>		<b>8.8</b>	<b>23.5</b>	<b>50.6</b>	<b>17.1</b>



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**GRAIN SIZE DISTRIBUTION**  
 Project: Circle Interchange Reconstruction  
 Location: Section 17, T39N, R14E of 3rd PM  
 Number: 1100-04-01

WEI GRAIN SIZE IDH 11000401.GPJ US LAB.GDT 9/14/17



Specimen Identification	LL	PL	PI	Fines	IDH Classification	
● 1705-B-06A#20	68.5 ft	41	18	23	97	<b>Clay</b>
⊠ 20-RWB-01#7	16.0 ft	31	16	15	79	<b>Silty Clay Loam</b>
▲ 20-RWB-01#16	48.5 ft	35	18	17	93	<b>Silty Clay</b>
★ 21-RWB-02#24	89.0 ft	22	14	8	77	<b>Silty Loam</b>
⊙ 21-RWB-04#10	23.5 ft	34	17	17	77	<b>Silty Clay</b>
⊕ 21-RWB-05#18	58.5 ft	25	15	10	68	<b>Silty Loam</b>

WEI ATTERBERG LIMITS IDH 11000401.GPJ US LAB.GDT 9/14/17

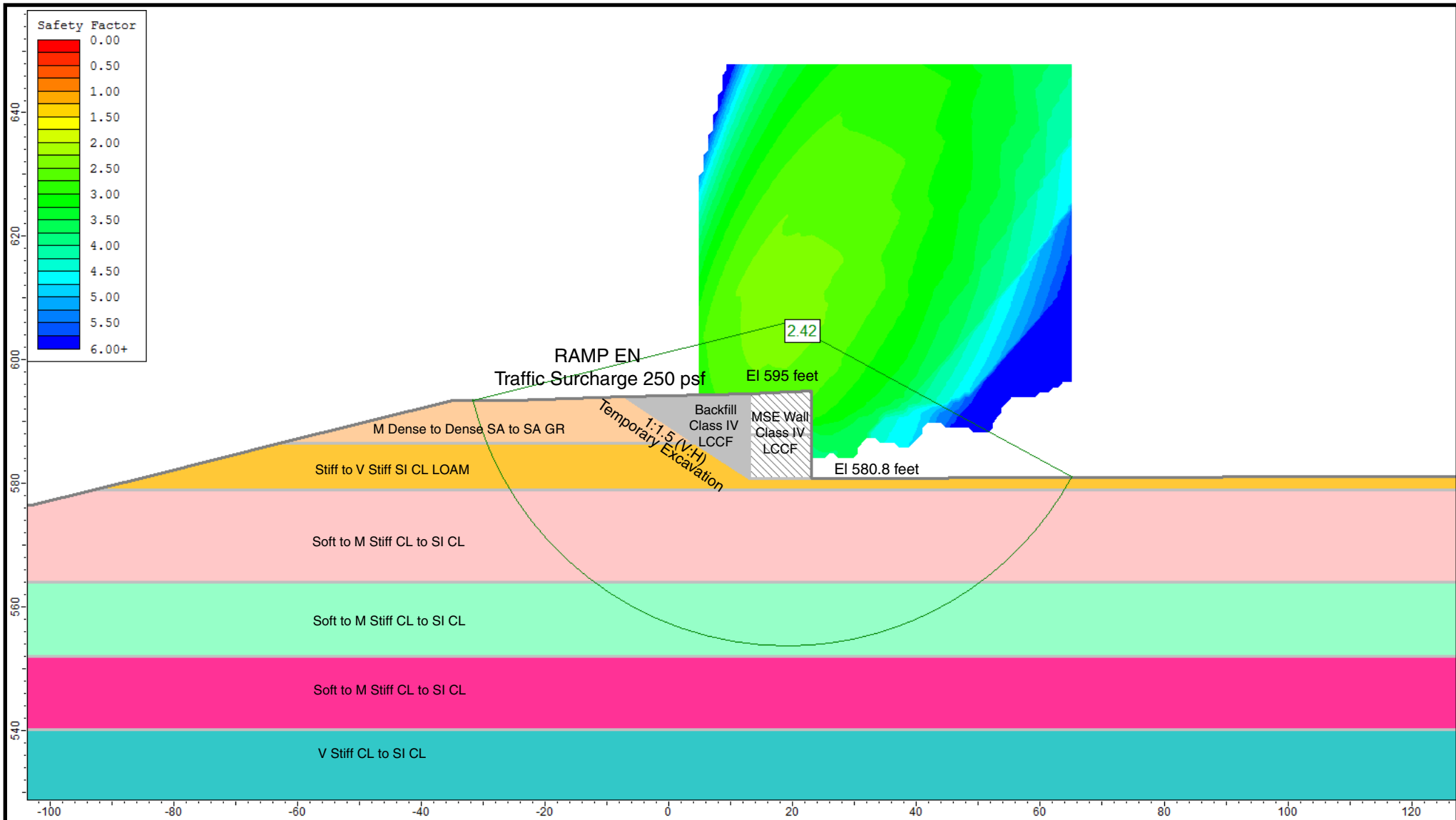


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**ATTERBERG LIMITS' RESULTS**

Project: Circle Interchange Reconstruction  
 Location: Section 17, T39N, R14E of 3rd PM  
 Number: 1100-04-01

## **APPENDIX C**



Undrained Analysis for MSE Wall at Station 1612+00, Ref Borings 1705-B-06A and VST-06

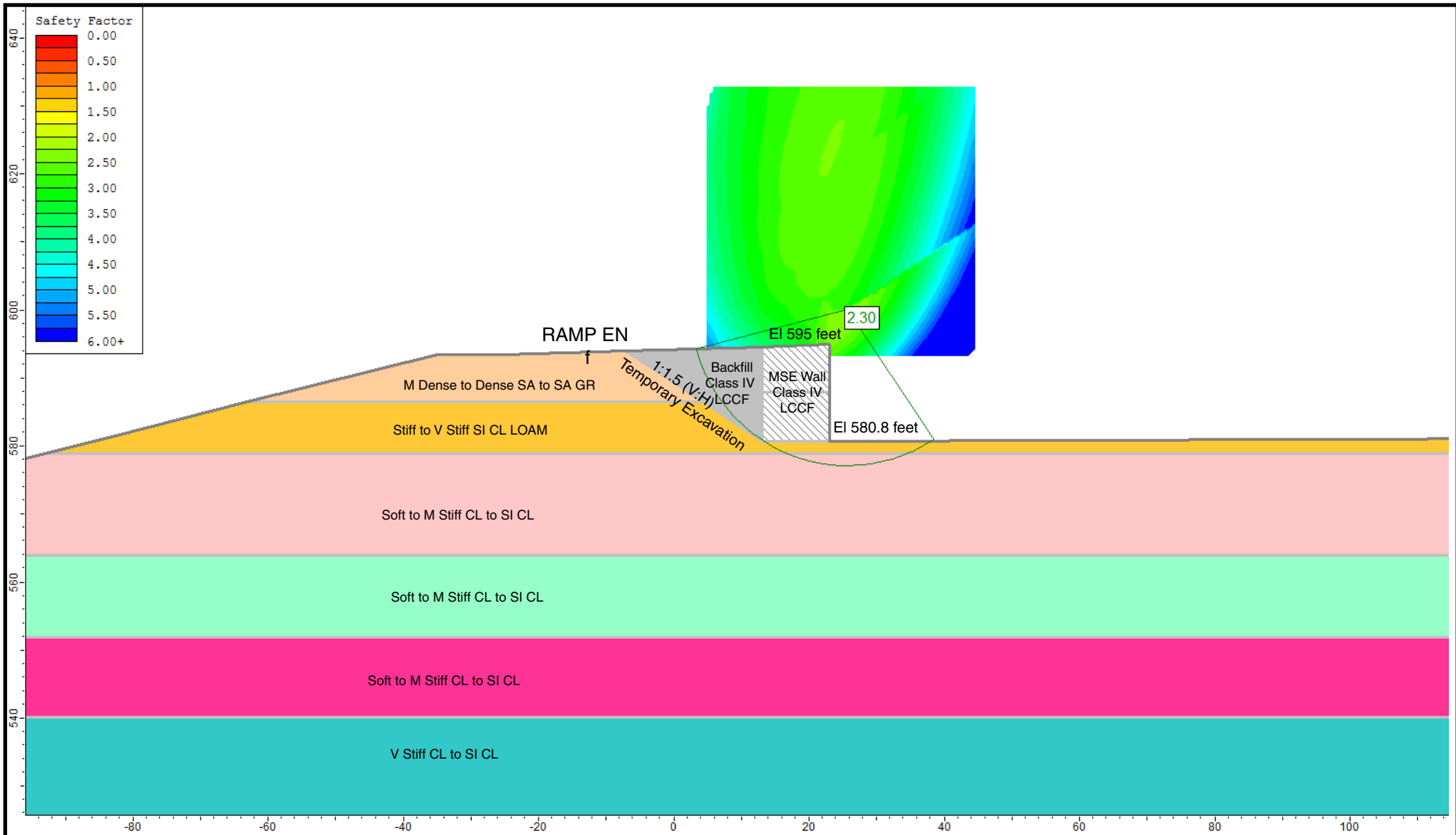
Layer ID	Description	Unit Weight (pcf)	Undrained Cohesion (psf)	Undrained Friction Angle (degrees)
1	M Dense to Dense LOAM	125	0	32
2	Stiff to V Stiff SI CL	120	2000	0
3	Soft to M Stiff CL to SI CL	110	600	0
4	Soft to M Stiff CL to SI CL	110	700	0
5	Soft to M Stiff CL to SI CL	110	900	0
6	V Stiff CL to SI CL	120	3000	0

GLOBAL STABILITY ANALYSIS: CIRCLE INTERCHANGE RECONSTRUCTION, RETAINING WALL 20, SN 016-1811, CHICAGO, IL

SCALE: GRAPHICAL | APPENDIX C-1 | DRAWN BY: NSB | CHECKED BY: MWS

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FOR AECOM | 1100-04-01



Drained Analysis for MSE Wall at Station 1612+00, Ref Borings 1705-B-06A and VST-06

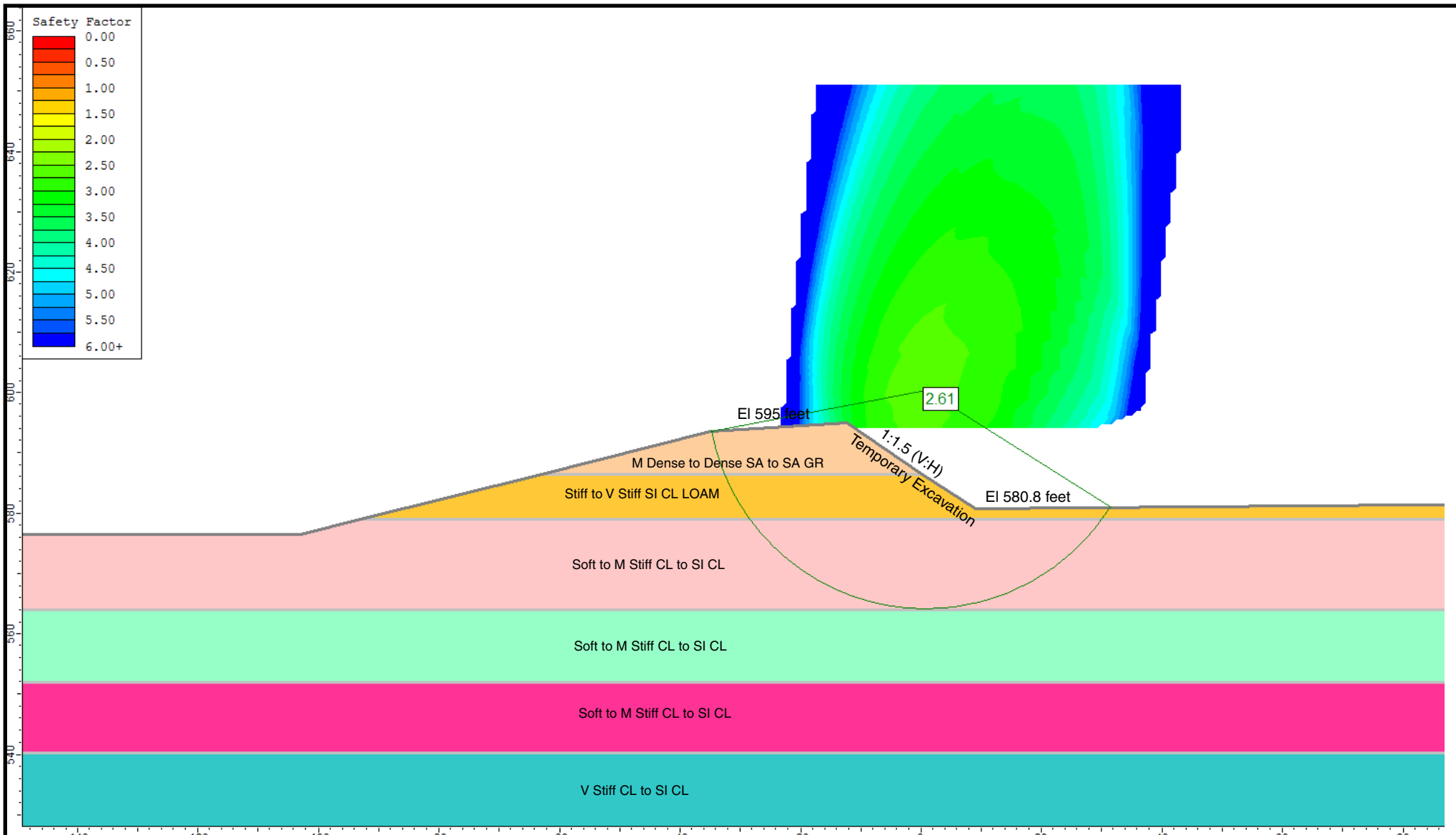
Layer ID	Description	Unit Weight (pcf)	Drained Cohesion (psf)	Drained Friction Angle (degrees)
1	M Dense to Dense LOAM	125	0	32
2	Stiff to V Stiff SI CL	120	2000	0
3	Soft to M Stiff CL to SI CL	110	600	0
4	Soft to M Stiff CL to SI CL	110	700	0
5	Soft to M Stiff CL to SI CL	110	900	0
6	V Stiff CL to SI CL	120	3000	0

GLOBAL STABILITY ANALYSIS: CIRCLE INTERCHANGE RECONSTRUCTION, RETAINING WALL 20, SN 016-1811, CHICAGO, IL

SCALE: GRAPHICAL      APPENDIX C-2      DRAWN BY: NSB  
CHECKED BY: MWS

 **Wang Engineering**  
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www.wangeng.com

FOR AECOM      1100-04-01



Undrained Analysis for Temporary Excavation, Ref Borings 1705-B-06A and VST-06

Layer ID	Description	Unit Weight (pcf)	Undrained Cohesion (psf)	Undrained Friction Angle (degrees)
1	M Dense to Dense LOAM	125	0	32
2	Stiff to V Stiff SI CL	120	2000	0
3	Soft to M Stiff CL to SI CL	110	600	0
4	Soft to M Stiff CL to SI CL	110	700	0
5	Soft to M Stiff CL to SI CL	110	900	0
6	V Stiff CL to SI CL	120	3000	0

GLOBAL STABILITY ANALYSIS: CIRCLE INTERCHANGE RECONSTRUCTION, RETAINING WALL 20, SN 016-1811, CHICAGO, IL

SCALE: GRAPHICAL | APPENDIX C-3 | DRAWN BY: NSB  
CHECKED BY: MWS

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FOR AECOM | 1100-04-01

## **APPENDIX D**



Benchmark: Cut square on center of door entrance to 707 W. Harrison St. (south side of Harrison St., approx. 90' west of west line of Des Plaines St.). Elevation 597.47.

Existing Structure: None. Traffic shall be maintained on the existing Ramp EN Structure (S.N. 016-2453) during construction of the proposed retaining wall. Subsequently, traffic shall be detoured to allow for construction of the remaining portions of the proposed Ramp EN (S.N. 016-1712) approaches and bridge structure.

### HIGHWAY CLASSIFICATION

Ramp EN  
 Functional Class: Interstate  
 ADT: 26,600 (2012); 31,000 (2040)  
 ADTT: 1,032 (2012); 1,203 (2040)  
 DHV: 1.910 (2040)  
 Design Speed: 30 m.p.h.  
 Posted Speed: 30 m.p.h.  
 One-Way Traffic  
 Directional Distribution: 100%

### DESIGN SPECIFICATIONS

2014 AASHTO LRFD Bridge  
 Design Specifications, 7th Edition  
 with 2015 and 2016 Interim Revisions

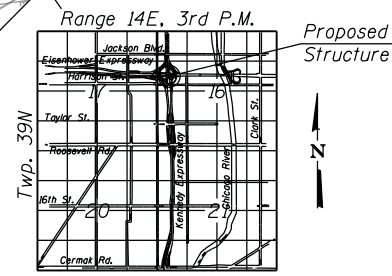
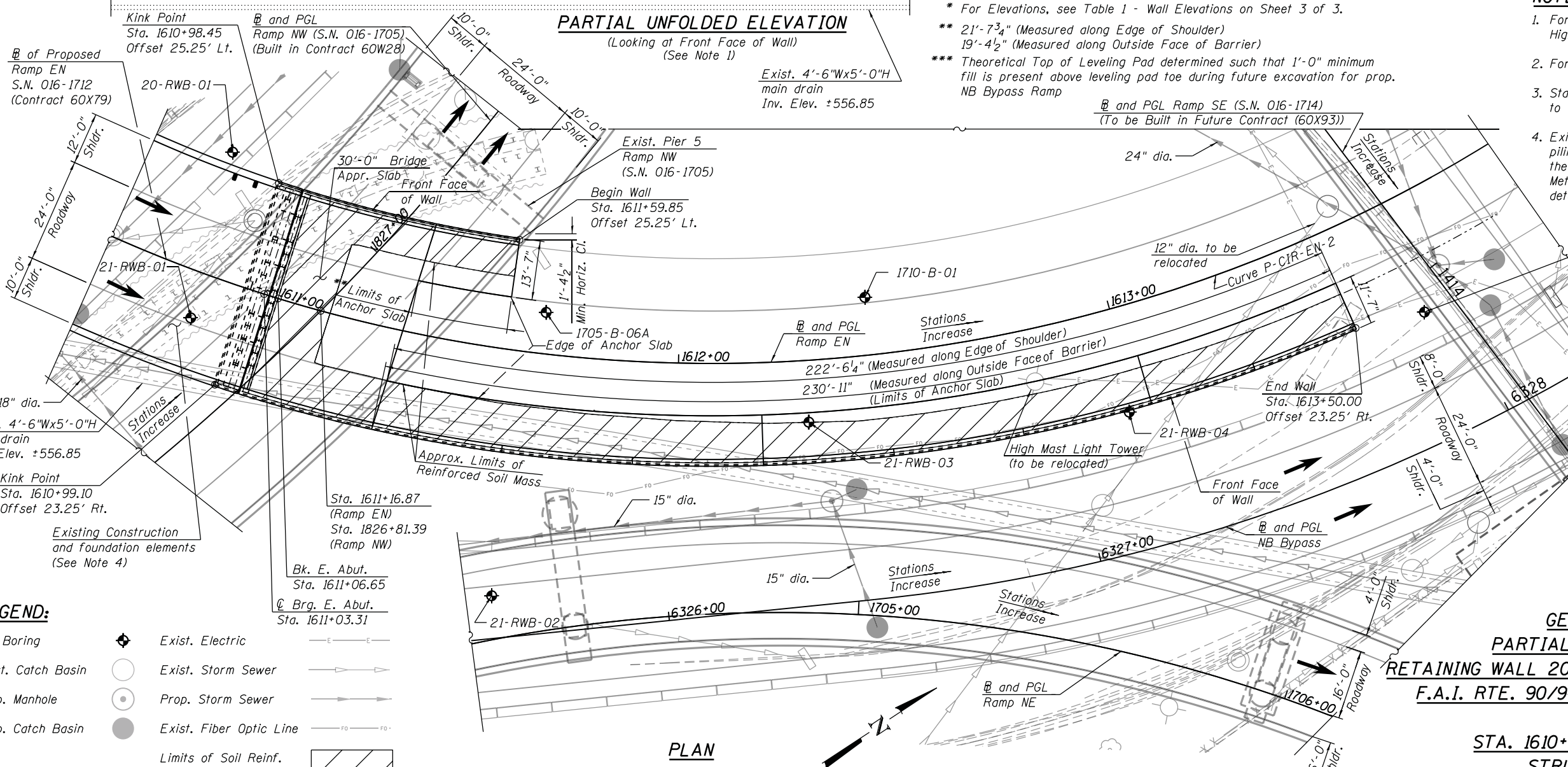
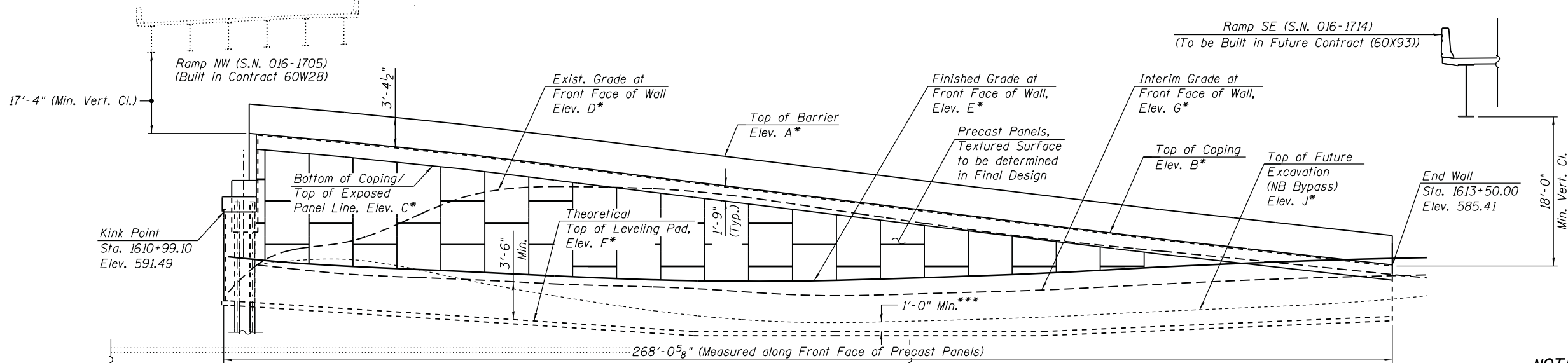
### DESIGN STRESSES

#### FIELD UNITS

$f'_c = 3,500 \text{ psi}$   
 $f_y = 60,000 \text{ psi (Reinforcement)}$   
**PRECAST UNITS**  
 $f'_c = 4,500 \text{ psi}$

### NOTES:

- For remaining portions of Unfolded Elevation and Highway Classification Data, see Sheet 2.
- For Table 1 - Wall Elevations, see Sheet 3.
- Stations and offsets are measured along  $\varnothing$  Ramp EN to the front face of precast panels.
- Existing construction and foundation elements (sheet piling, drilled shafts, steel piles, etc.) are present at the north portion of proposed Retaining Wall 20. Methods for resolving potential conflicts will be determined during the design phase.



**GENERAL PLAN AND  
 PARTIAL UNFOLDED ELEVATION  
 RETAINING WALL 20 ALONG RAMP EN EAST ABUTMENT  
 F.A.I. RTE. 90/94/290 - SECTION 2014-005R&B  
 COOK COUNTY  
 STA. 1610+99.10 TO STA. 1613+50.00  
 STRUCTURE NO. 016-1811**

### LEGEND:

- |                    |  |                         |  |
|--------------------|--|-------------------------|--|
| Soil Boring        |  | Exist. Electric         |  |
| Exist. Catch Basin |  | Exist. Storm Sewer      |  |
| Prop. Manhole      |  | Prop. Storm Sewer       |  |
| Prop. Catch Basin  |  | Exist. Fiber Optic Line |  |
|                    |  | Limits of Soil Reinf.   |  |

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 HILLSIDE, IL 60162  
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 FAX: (708) 236-0901

USER NAME = will.merdeaus	DESIGNED - MI, JJS	REVISED -
DRAWN - SK	REVISIONS -	
CHECKED - MAI, MI	REVISIONS -	
DATE - 03/23/2018	REVISIONS -	

STATE OF ILLINOIS  
 DEPARTMENT OF TRANSPORTATION

STRUCTURE NO. 016-1811

SCALE: SHEET 1 OF 3 SHEETS STA. TO STA.

F.A.I. RTE.	SECTION	COUNTY	TOTAL SHEETS	SHEET NO.
90/94/290	2014-005R&B	COOK	3	1
CONTRACT NO. 60X79			ILLINOIS FED. AID PROJECT	

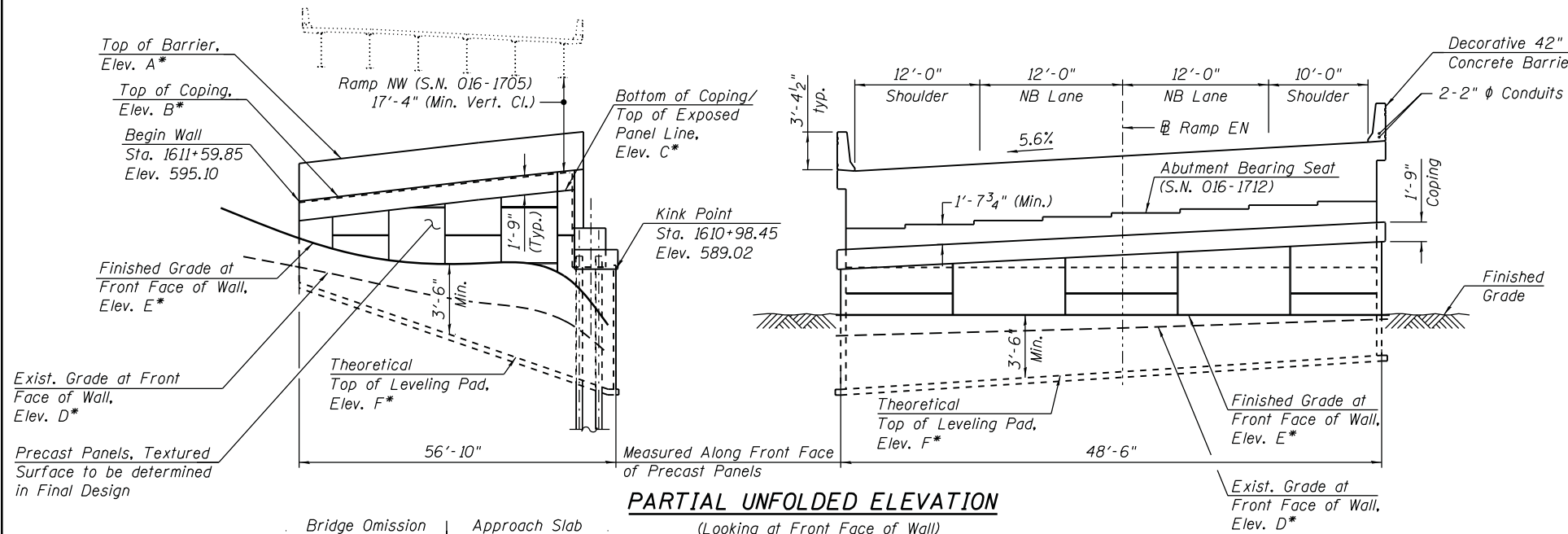
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**HIGHWAY CLASSIFICATION**

Ramp NW	NB Bypass	Ramp SE
Functional Class: Interstate	Functional Class: Interstate	Functional Class: Interstate
ADT: 32,500 (2012); 36,000 (2040)	ADT: NA (2012); 17,000 (2040)	ADT: 4,600 (2010); 5,000 (2040)
ADTT: 2,483 (2012); 2,730 (2040)	ADTT: NA (2012); 442 (2040)	ADTT: 123 (2012); 134 (2040)
DHV: 2,790 (2040)	DHV: 1,680 (2040)	DHV: 440 (2040)
Design Speed: 35 m.p.h.	Design Speed: 30 m.p.h.	Design Speed: 25 m.p.h.
Posted Speed: 35 m.p.h.	Posted Speed: 30 m.p.h.	Posted Speed: 25 m.p.h.
One-Way Traffic	One-Way Traffic	One-Way Traffic
Directional Distribution: N/A	Directional Distribution: NA	Directional Distribution: 100%

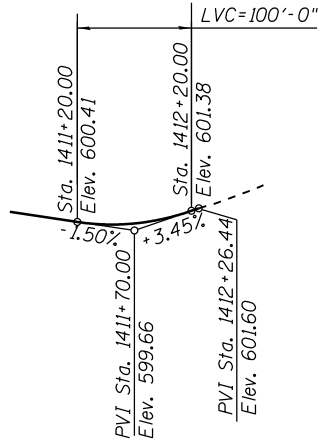
**NOTES:**

- All Lightweight Cellular Concrete Fill shall be Class III.
- For additional Notes, see Sheet 1.
- For Elevations, see Table 1 - Wall Elevations on Sheet 3 of 3.
- Abutment soil reinforcement to resist lateral loads in lieu of steel piles.
- Size, spacing, depth and number as required by design.
- The MSE Wall supplier's internal stability design shall account for the anchorage slab's bearing pressure surcharge of 1 ksf and horizontal sliding force of 0.83 kips/ft of wall.



**CURVE DATA**

(RAMP SE)  
 PROP. CURVE P-CIR-SE-2  
 PI STA. = 1415+83.08  
 $\Delta = 157^\circ 44' 18" (LT)$   
 $D = 24^\circ 48' 12"$   
 $R = 231.00'$   
 $T = 1,174.08'$   
 $L = 635.96'$   
 $E = 965.59'$   
 $e = 5.60\%$   
 T.R. = NA  
 S.E. RUN = 128'  
 P.C. STA. = 1404+09.00  
 P.T. STA. = 1410+44.95  
 DS = 25  
 PS = 25

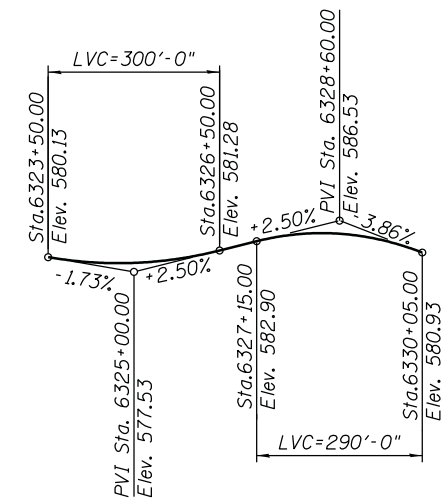


**PROFILE GRADE**

(Along @ RAMP SE)

**CURVE DATA**

(RAMP NB Bypass)  
 (Prop. Curve P-NCD-NX-4)  
 P.I. Sta. = 6328+76.78  
 $\Delta = 59^\circ 05' 41" (LT)$   
 $D = 14^\circ 08' 50"$   
 $R = 405.00'$   
 $T = 229.58'$   
 $L = 417.72'$   
 $E = 60.54'$   
 $e = 5.40\%$   
 T.R. = 36'  
 S.E. Run = 98'  
 P.C. Sta. = 6326+47.20  
 P.T. Sta. = 6330+64.91  
 DS = 30  
 PS = 30



**PROFILE GRADE**

(Along @ NB Bypass)

**PARTIAL UNFOLDED ELEVATIONS, SECTIONS, AND DETAILS**

**RETAINING WALL 20 ALONG RAMP EN EAST ABUTMENT**

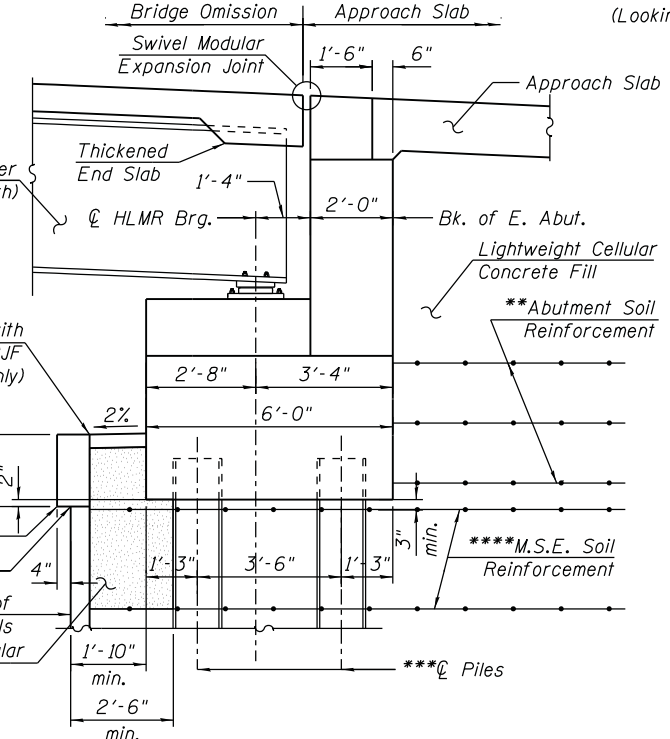
**F.A.I. RTE. 90/94/290 - SECTION 2014-005R&B**

**COOK COUNTY**

**STA. 1610+99.10 TO STA. 1613+50.00**

**STRUCTURE NO. 016-1811**

FILE PATH = p:\61779-P\INT\pccom\line\local\BCE\0502\_NA\Documents\01\_Americas\1\000\_CAD\008\_Structural\RetainingWall\_20\Sheet\0161811-0079-000-TSL-002

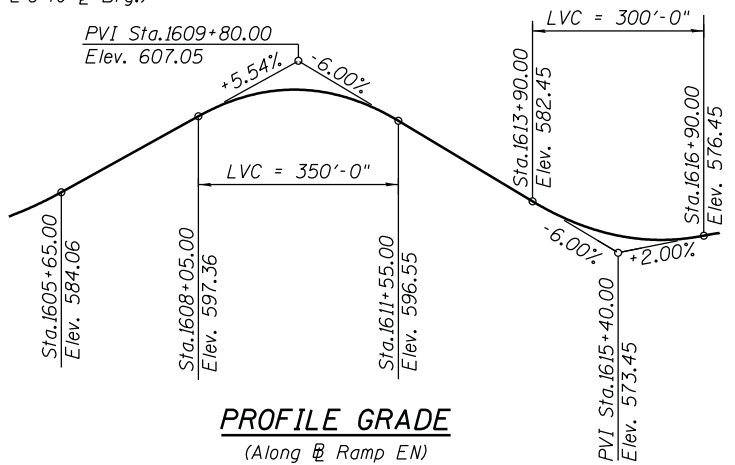


**SECTION THRU EAST ABUTMENT**

(Horiz. Dims. @ Rt. L's to φ Brg.)

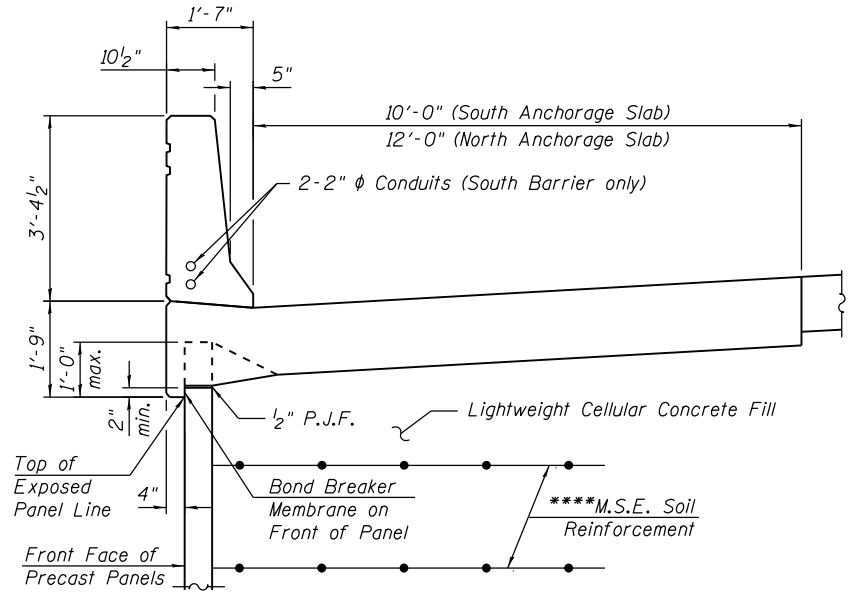
**CURVE DATA**

(RAMP EN)  
 (PROP. CURVE P-CIR-EN-2)  
 PI STA. = 1624+41.43  
 $\Delta = 158^\circ 32' 09" (LT)$   
 $D = 16^\circ 51' 06"$   
 $R = 340.00'$   
 $T = 1,793.89'$   
 $L = 940.77'$   
 $E = 1,485.82'$   
 $e = 5.60\%$   
 T.R. = 36'  
 S.E. RUN = 102'  
 P.C. STA. = 1606+47.54  
 P.T. STA. = 1615+88.31  
 DS = 30  
 PS = 30



**PROFILE GRADE**

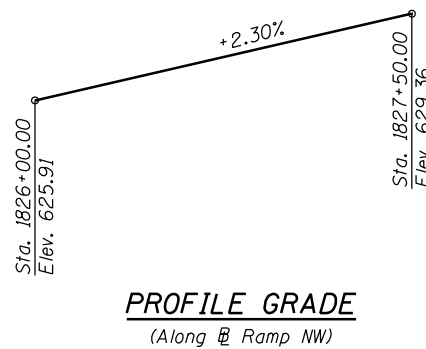
(Along @ Ramp EN)



**SECTION THROUGH BARRIER AND ANCHORAGE SLAB**

**CURVE DATA**

(RAMP NW)  
 (Prop. Curve P-CIR-NW-6)  
 P.I. Sta. = 1831+44.22  
 $\Delta = 88^\circ 30' 25" (LT)$   
 $D = 10^\circ 36' 37"$   
 $R = 540.00'$   
 $T = 526.11'$   
 $L = 834.16'$   
 $E = 213.92'$   
 $e = 5.40\%$   
 T.R. = 39'  
 S.E. Run = 105'  
 P.C. Sta. = 1826+18.11  
 P.T. Sta. = 1834+52.27  
 DS = 35  
 PS = 35



**PROFILE GRADE**

(Along @ Ramp NW)

USER NAME = will.merdauss	DESIGNED - MI, JJS	REVISED -
PLOT SCALE = 28.00' / in.	DRAWN - SK	REVISED -
PLOT DATE = 3/24/2018	CHECKED - MAI, MI	REVISED -
	DATE - 03/23/2018	REVISED -

**STATE OF ILLINOIS  
 DEPARTMENT OF TRANSPORTATION**

**STRUCTURE NO. 016-1811**

SCALE: SHEET 2 OF 3 SHEETS STA. TO STA.

F.A.I. RTE. 90/94/290	SECTION 2014-005R&B	COUNTY COOK	TOTAL SHEETS 3	SHEET NO. 2
CONTRACT NO. 60X79			ILLINOIS FED. AID PROJECT	

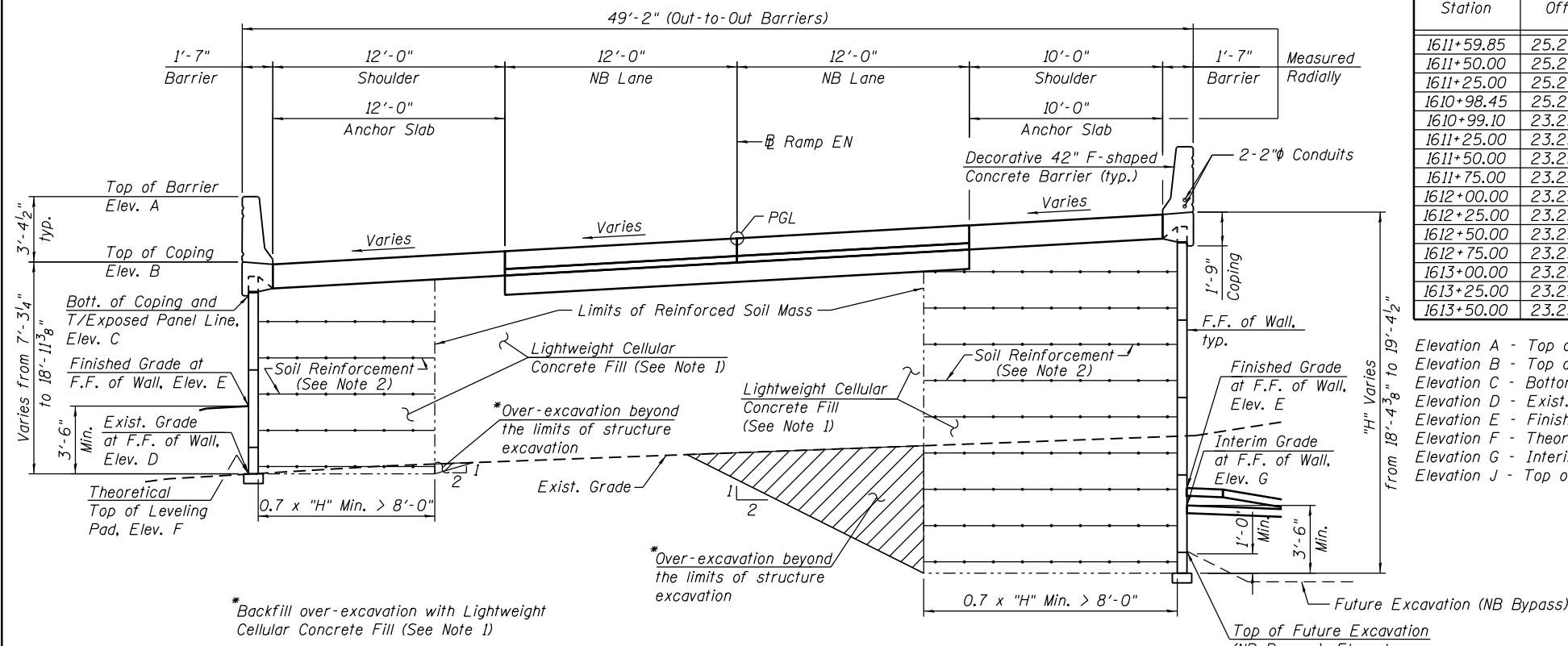
**HBM**  
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**TABLE 1 - WALL ELEVATIONS**

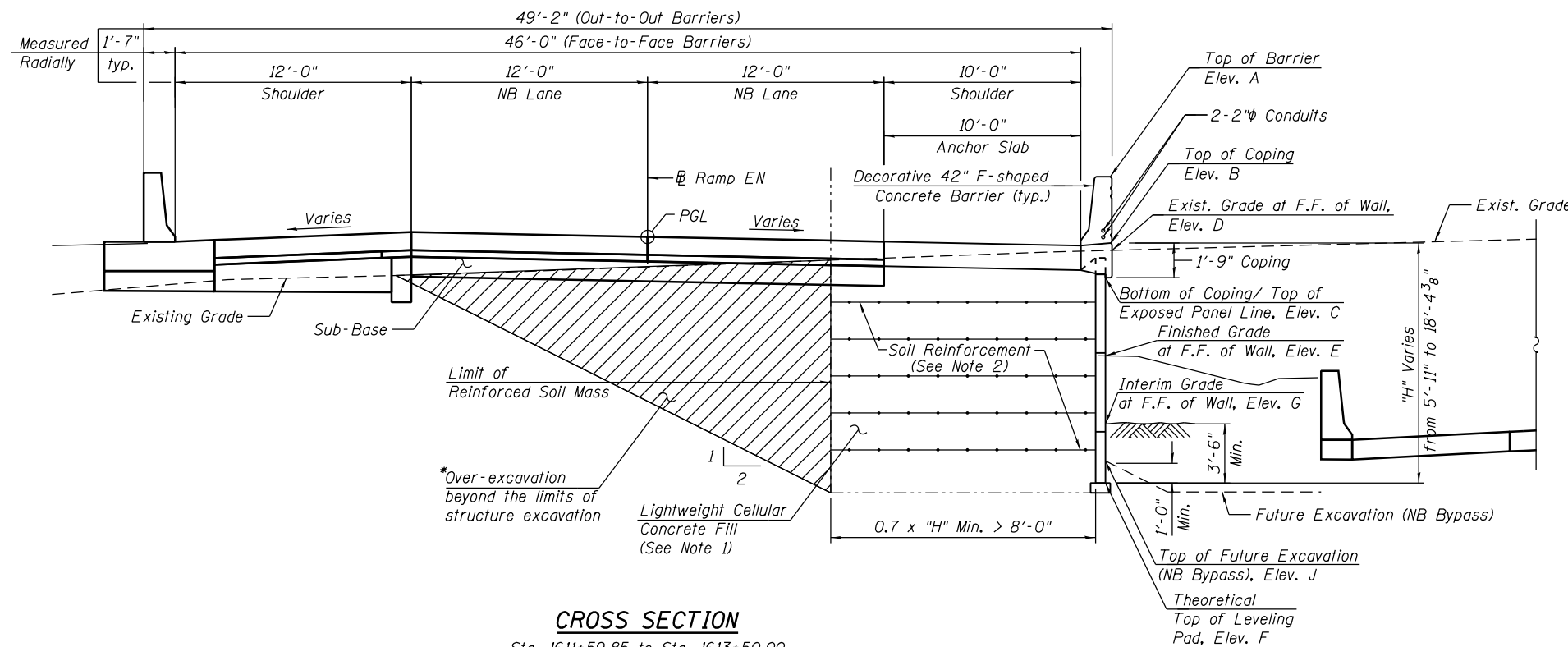
Station	Offset	Elevation A	Elevation B	Elevation C	Elevation D	Elevation E	Elevation F	Elevation G	Elevation J
1611+59.85	25.25 LT.	598.48	595.11	593.36	589.19	591.78	587.83	-	-
1611+50.00	25.25 LT.	599.01	595.64	593.89	586.02	589.53	586.26	-	-
1611+25.00	25.25 LT.	600.36	596.99	595.24	583.99	587.86	582.25	-	-
1610+98.45	25.25 LT.	-	-	-	-	-	-	-	-
1610+99.10	23.25 RT.	-	-	-	-	-	-	-	-
1611+25.00	23.25 RT.	602.94	599.57	597.82	587.99	585.29	580.42	584.40	586.07
1611+50.00	23.25 RT.	601.58	598.21	596.46	593.08	584.68	579.54	583.78	583.82
1611+75.00	23.25 RT.	599.95	596.58	594.83	594.40	584.04	578.66	583.14	581.46
1612+00.00	23.25 RT.	598.31	594.94	593.19	593.85	583.61	577.78	582.71	579.62
1612+25.00	23.25 RT.	596.68	593.31	591.56	592.13	583.60	577.78	581.93	578.81
1612+50.00	23.25 RT.	595.04	591.67	589.92	590.16	583.97	577.78	582.13	579.00
1612+75.00	23.25 RT.	593.41	590.04	588.29	588.41	584.46	577.78	582.54	579.42
1613+00.00	23.25 RT.	591.79	588.42	586.67	587.02	585.16	578.35	583.21	580.08
1613+25.00	23.25 RT.	590.29	586.92	585.17	585.69	585.75	578.93	583.79	580.66
1613+50.00	23.25 RT.	588.79	585.42	583.67	584.32	586.17	579.50	584.18	581.50

Elevation A - Top of Barrier  
 Elevation B - Top of Coping  
 Elevation C - Bottom of Coping/Top of Exposed Panel Line  
 Elevation D - Exist. Grade at Front Face of Wall  
 Elevation E - Finished Grade at Front Face of Wall  
 Elevation F - Theoretical Top of Leveling Pad  
 Elevation G - Interim Grade at Front Face of Wall  
 Elevation J - Top of Future Excavation (NB Bypass)



**CROSS SECTION**

Sta. 1610+98.45 to Sta. 1611+59.85  
 (Looking Up-station)



**CROSS SECTION**

Sta. 1611+59.85 to Sta. 1613+50.00  
 (Looking Up-station)

**NOTES:**

- All lightweight cellular concrete fill shall be Class III.
- The MSE wall supplier's internal stability design shall account for the anchorage slab's bearing pressure surcharge of 1.0 ksf and horizontal sliding force of 0.83 kips/ft. of wall.
- F.F. denotes Front Face.
- For additional notes, see Sheet 1.

**SECTIONS**  
**RETAINING WALL 20 ALONG RAMP EN EAST ABUTMENT**  
**F.A.I. RTE. 90/94/290 - SECTION 2014-005R&B**  
**COOK COUNTY**  
**STA. 1610+99.10 TO STA. 1613+50.00**  
**STRUCTURE NO. 016-1811**

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 USER = will.merdeaus  
 DESIGNED - MI, JJS  
 DRAWN - SK  
 CHECKED - MAI, MI  
 DATE - 03/23/2018  
 REVISIONS  
 REVISED -  
 REVISED -  
 REVISED -  
 REVISED -  
 STATE OF ILLINOIS  
 DEPARTMENT OF TRANSPORTATION  
 STRUCTURE NO. 016-1811  
 SCALE: SHEET 3 OF 3 SHEETS STA. TO STA.  
 F.A.I. RTE. 90/94/290 SECTION 2014-005R&B COUNTY COOK TOTAL SHEETS 3 SHEET NO. 3 CONTRACT NO. 60X79 ILLINOIS FED. AID PROJECT

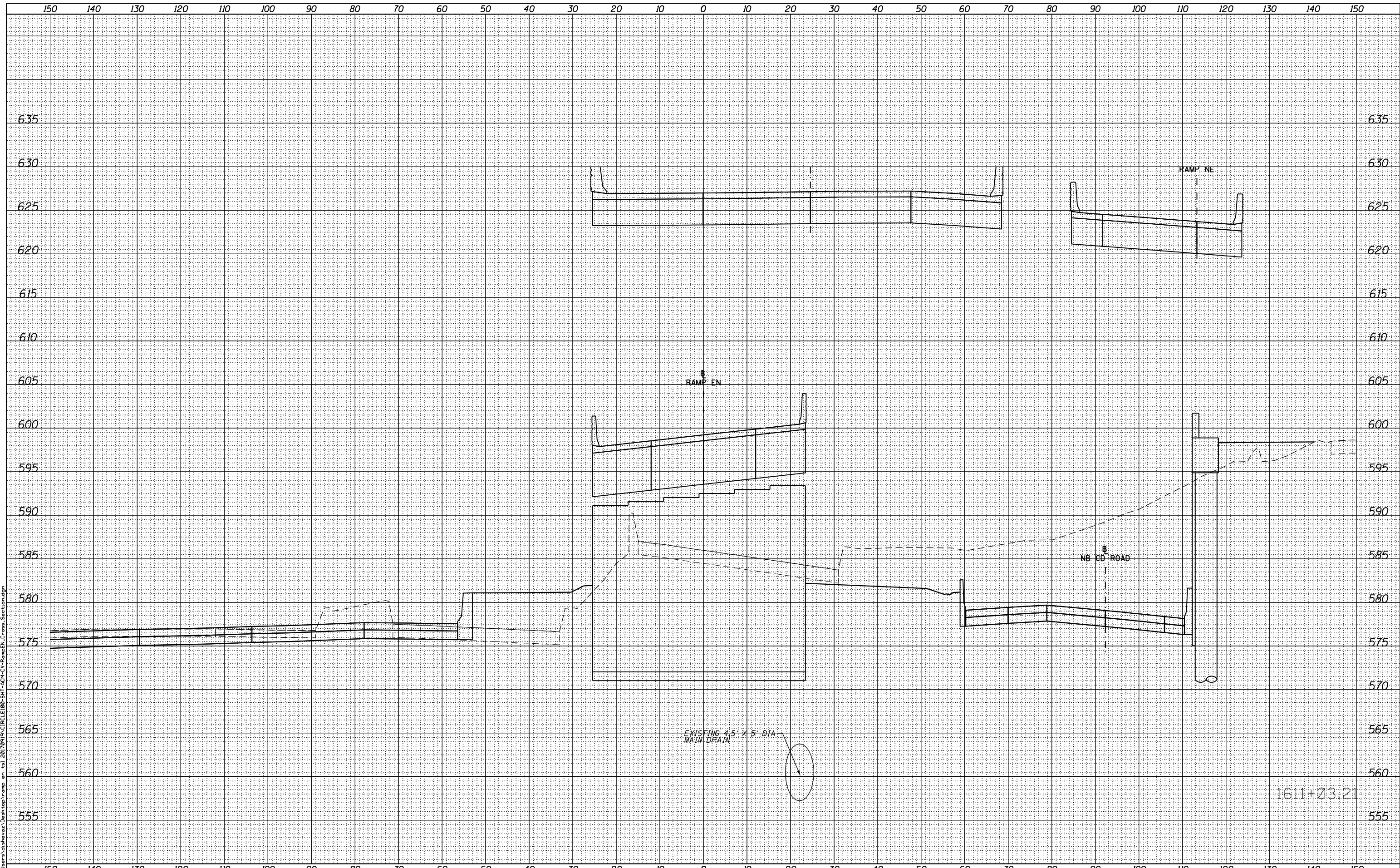
## **APPENDIX E**



DATE	
BY	
ORIGINAL SURVEY NO.	
SURVEYED PLOTTED AREAS CHECKED	
NOTE BOOK NO.	
TEMPLATE AREAS CHECKED	

DATE	
BY	
ORIGINAL SURVEY NO.	
SURVEYED PLOTTED AREAS CHECKED	
NOTE BOOK NO.	
TEMPLATE AREAS CHECKED	

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**STATE OF ILLINOIS  
DEPARTMENT OF TRANSPORTATION**

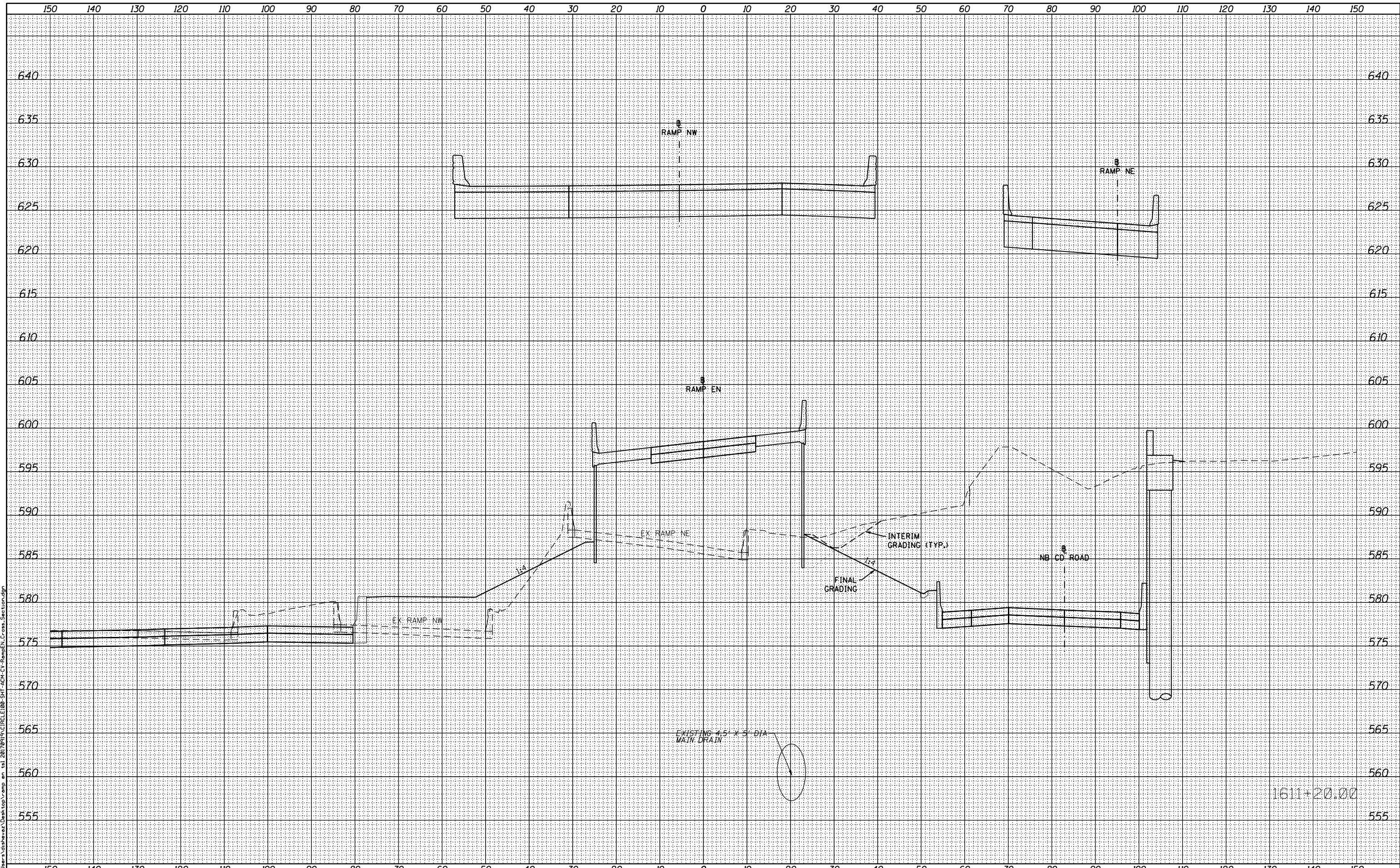
SCALE:	SHEET 21 OF 36 SHEETS	STA. 1611+03.21 TO STA. 1611+03.21
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F.A. RTE.	SECTION	COUNTY	TOTAL SHEETS	SHEET NO.
			36	
CONTRACT NO.			ILLINOIS FED. AID PROJECT	

DATE	
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FINAL SURVEY NO.	
SURVEYED	
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**STATE OF ILLINOIS  
DEPARTMENT OF TRANSPORTATION**

CROSS SECTIONS - RAMP EN

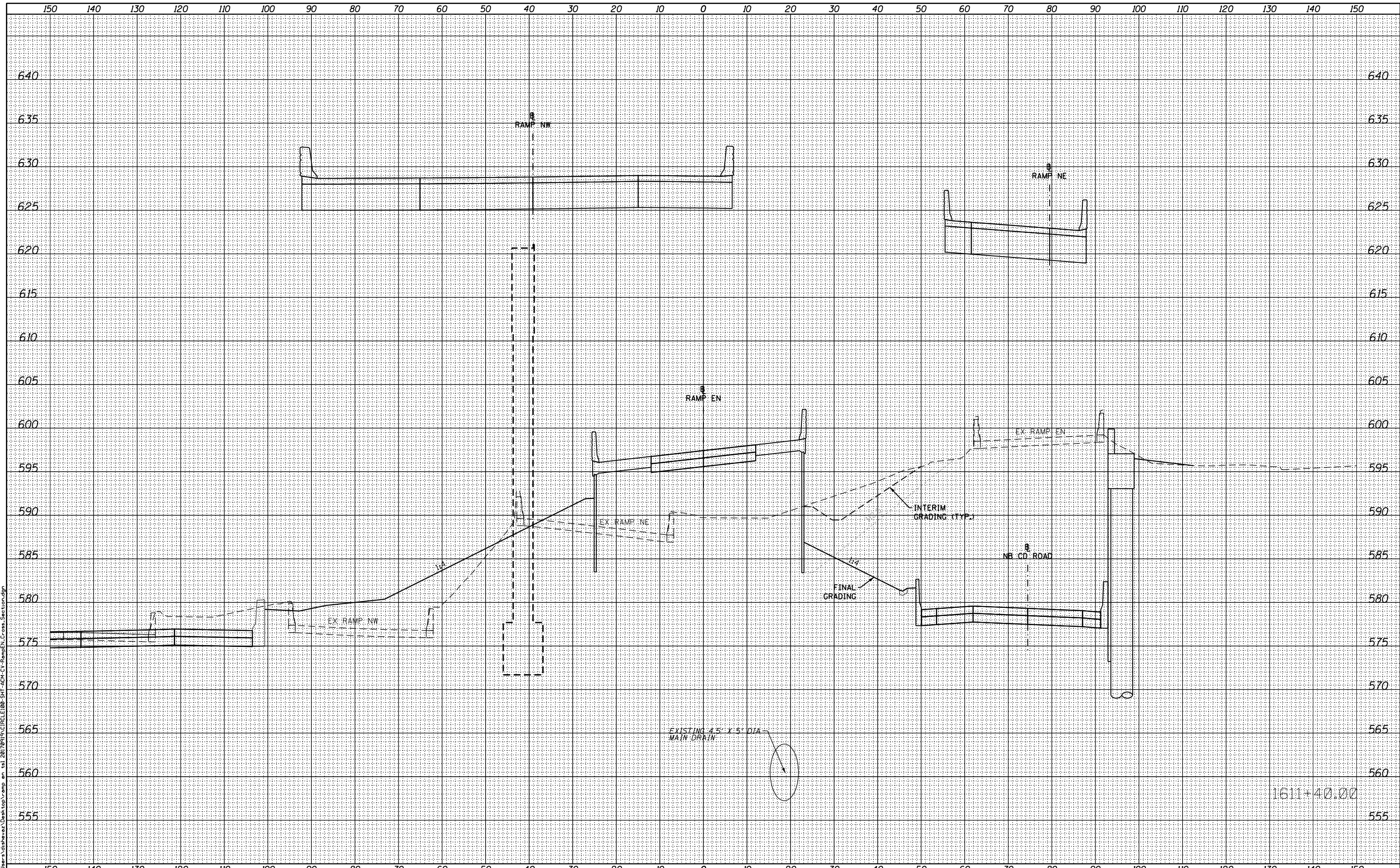
SCALE: SHEET 22 OF 36 SHEETS STA. 1611+20.00 TO STA. 1611+20.00

F.A. RTE.	SECTION	COUNTY	TOTAL SHEETS	SHEET NO.
			36	
CONTRACT NO.				
ILLINOIS FED. AID PROJECT				

DATE	
BY	
FINAL SURVEY NO.	
SURVEYED AREAS CHECKED	
PLOTTED TEMPLATE	
NOTE BOOK	
AREAS CHECKED	

DATE	
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**STATE OF ILLINOIS  
DEPARTMENT OF TRANSPORTATION**

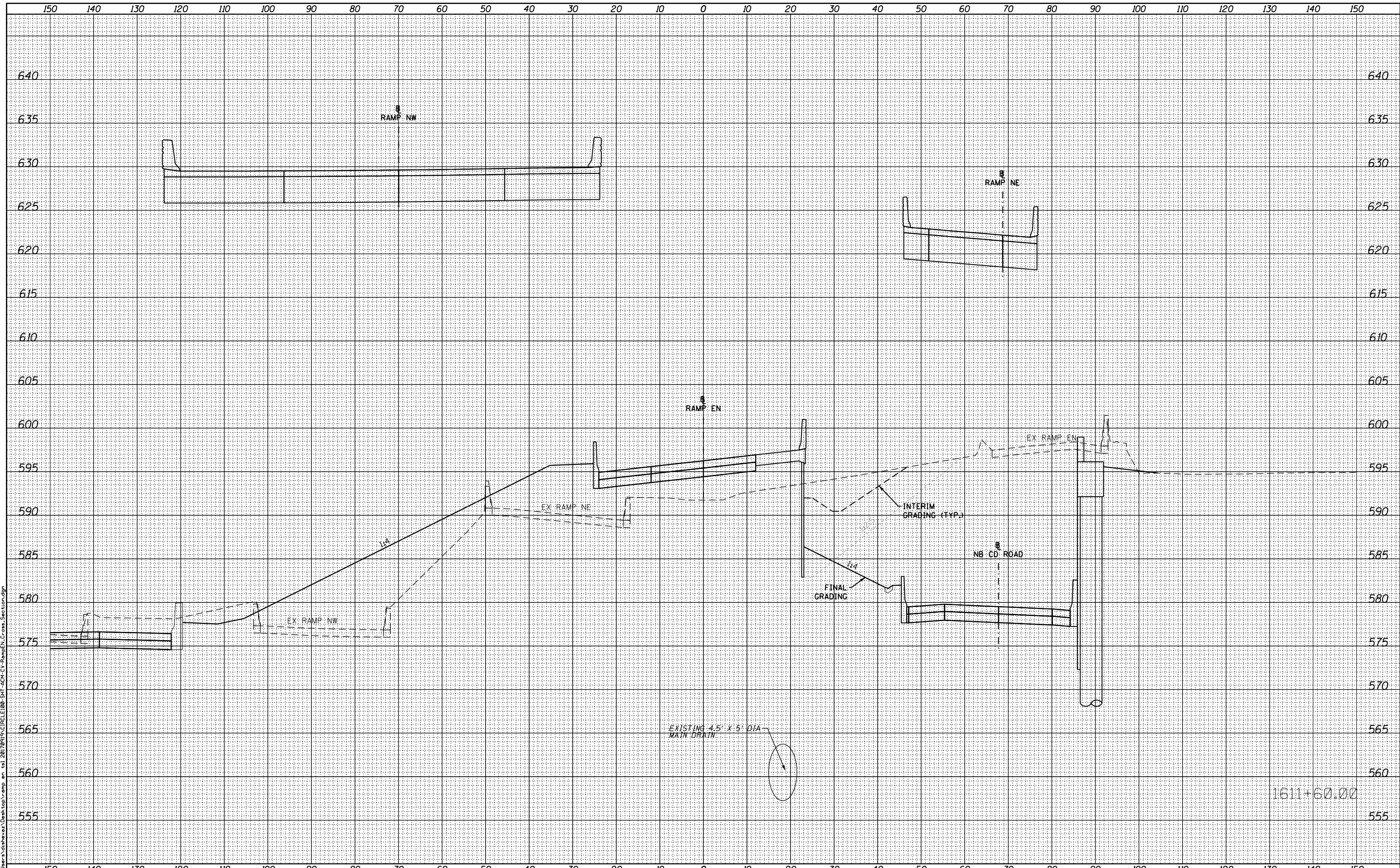
SCALE:	SHEET 23 OF 36 SHEETS	STA. 1611+40.00 TO STA. 1611+40.00
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F.A. RTE.	SECTION	COUNTY	TOTAL SHEETS	SHEET NO.
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CONTRACT NO.				
ILLINOIS FED. AID PROJECT				

DATE	
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PLOT DATE = 9/19/2017	DATE -	REVISED -

STATE OF ILLINOIS  
DEPARTMENT OF TRANSPORTATION

CROSS SECTIONS - RAMP EN  
SCALE: SHEET 24 OF 36 SHEETS STA. 1611+60.00 TO STA. 1611+60.00

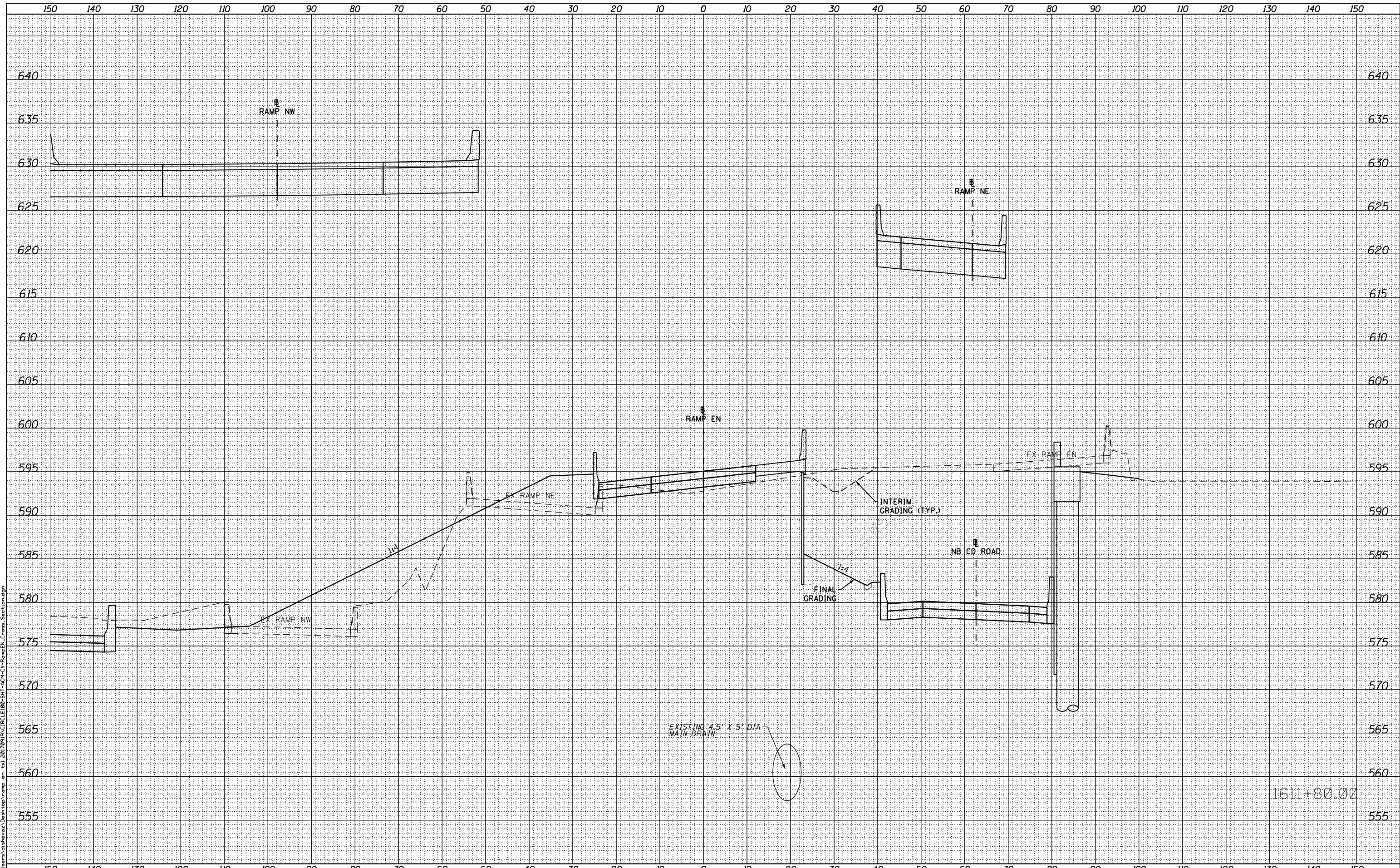
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CONTRACT NO.				
ILLINOIS FED. AID PROJECT				



DATE	
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FINAL SURVEY NO.	
SURVEYED PLOTTED AREAS CHECKED	
NOTE BOOK NO.	
TEMPLATE AREAS CHECKED	

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NOTE BOOK NO.	
TEMPLATE AREAS CHECKED	

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STATE OF ILLINOIS  
DEPARTMENT OF TRANSPORTATION

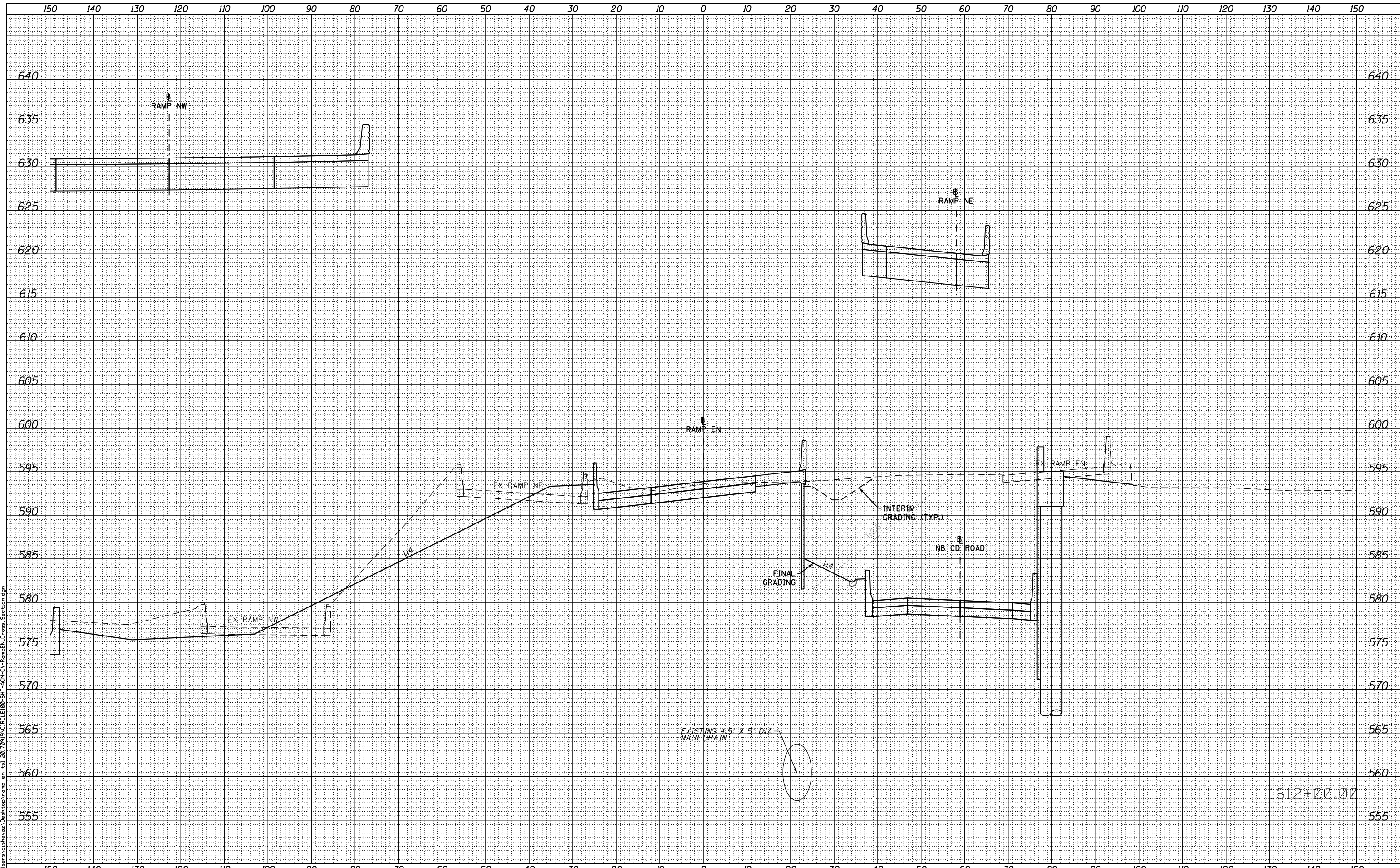
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F.A. RTE.	SECTION	COUNTY	TOTAL SHEETS	SHEET NO.
			36	
CONTRACT NO.				
ILLINOIS FED. AID PROJECT				

DATE	
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NOTE BOOK	

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PLOT SCALE = 20.0000' / in.	CHECKED -	REVISED -
PLOT DATE = 9/19/2017	DATE -	REVISED -

STATE OF ILLINOIS  
DEPARTMENT OF TRANSPORTATION

CROSS SECTIONS - RAMP EN

SCALE: SHEET 26 OF 36 SHEETS STA. 1612+00.00 TO STA. 1612+00.00

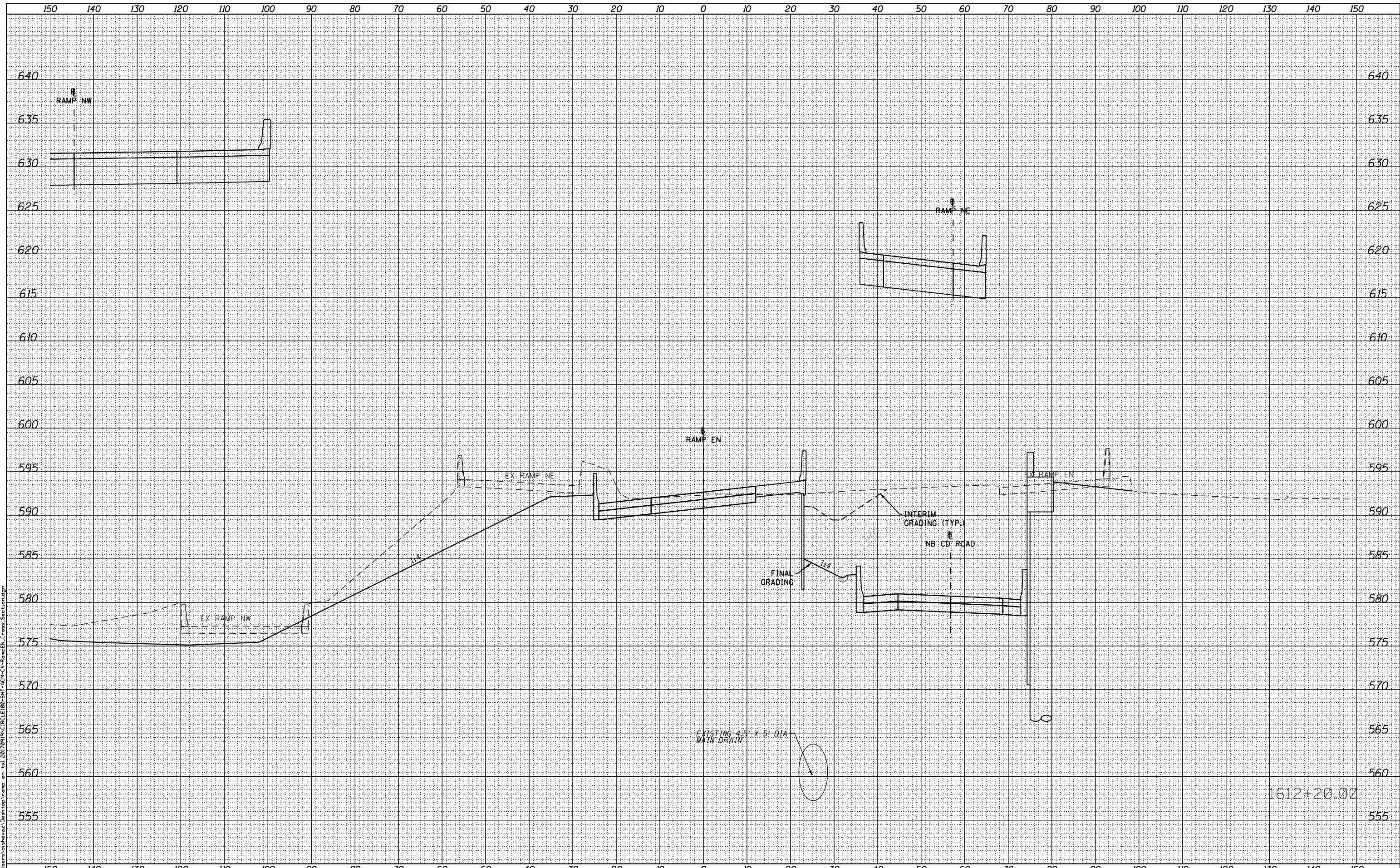
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CONTRACT NO.				
ILLINOIS FED. AID PROJECT				

1612+00.00

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**STATE OF ILLINOIS  
DEPARTMENT OF TRANSPORTATION**

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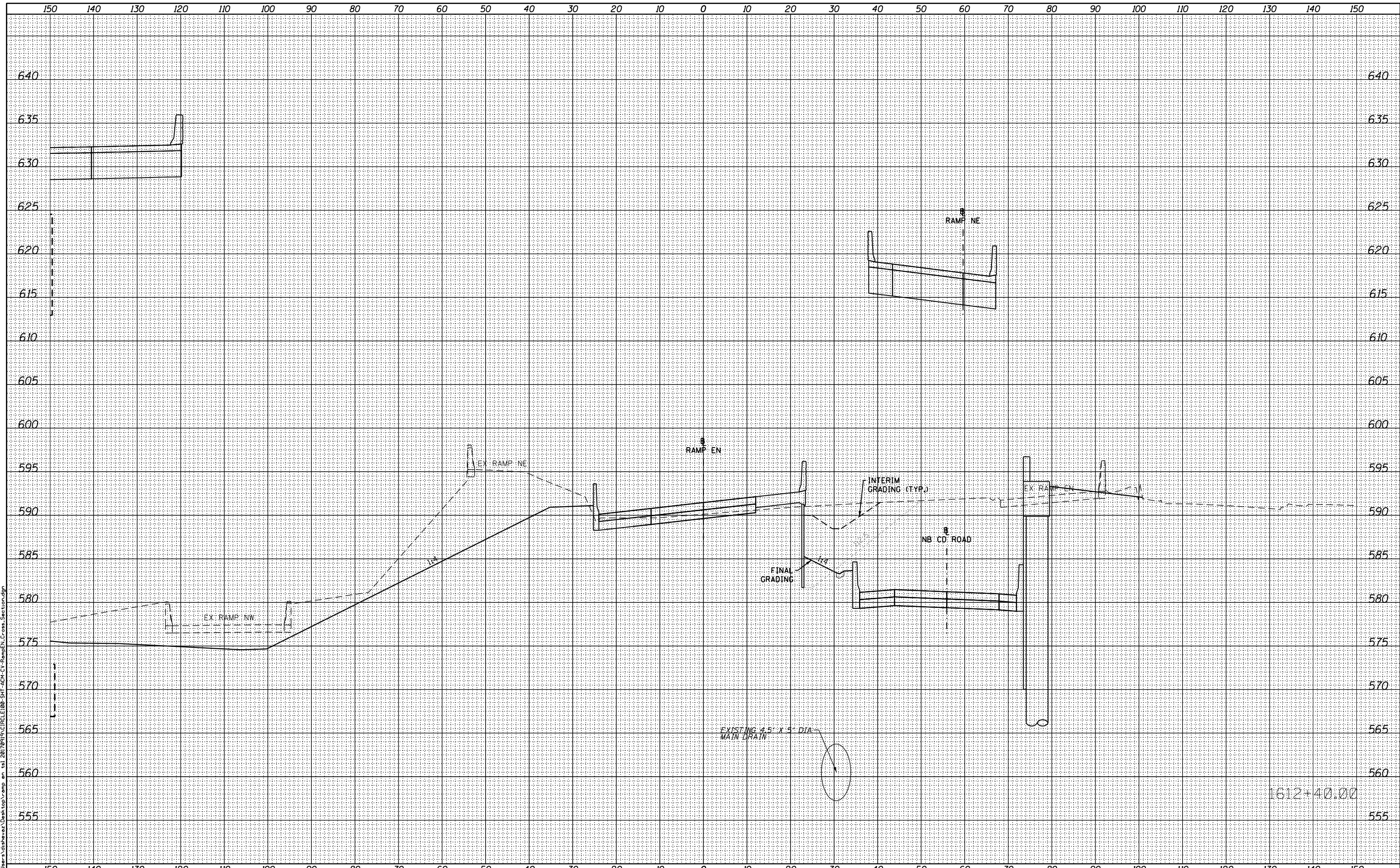
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CONTRACT NO.				
ILLINOIS FED. AID PROJECT				

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**STATE OF ILLINOIS  
DEPARTMENT OF TRANSPORTATION**

CROSS SECTIONS - RAMP EN

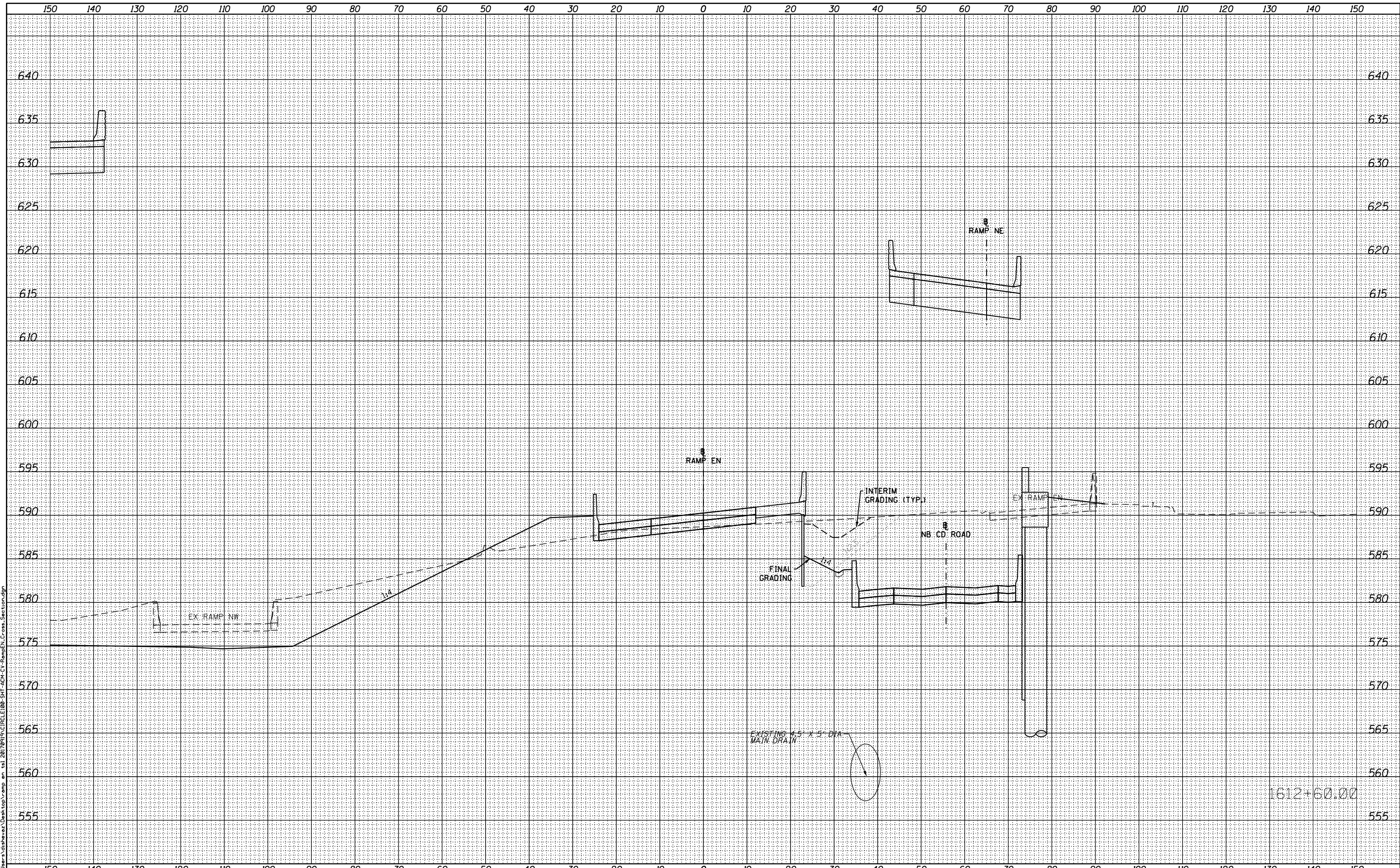
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F.A. RTE.	SECTION	COUNTY	TOTAL SHEETS	SHEET NO.
			36	
CONTRACT NO.				
ILLINOIS FED. AID PROJECT				

DATE	
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ORIGINAL SURVEY NO.	
SURVEYED PLOTTED AREAS CHECKED	
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ORIGINAL SURVEY NO.	
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**STATE OF ILLINOIS  
DEPARTMENT OF TRANSPORTATION**

CROSS SECTIONS - RAMP EN

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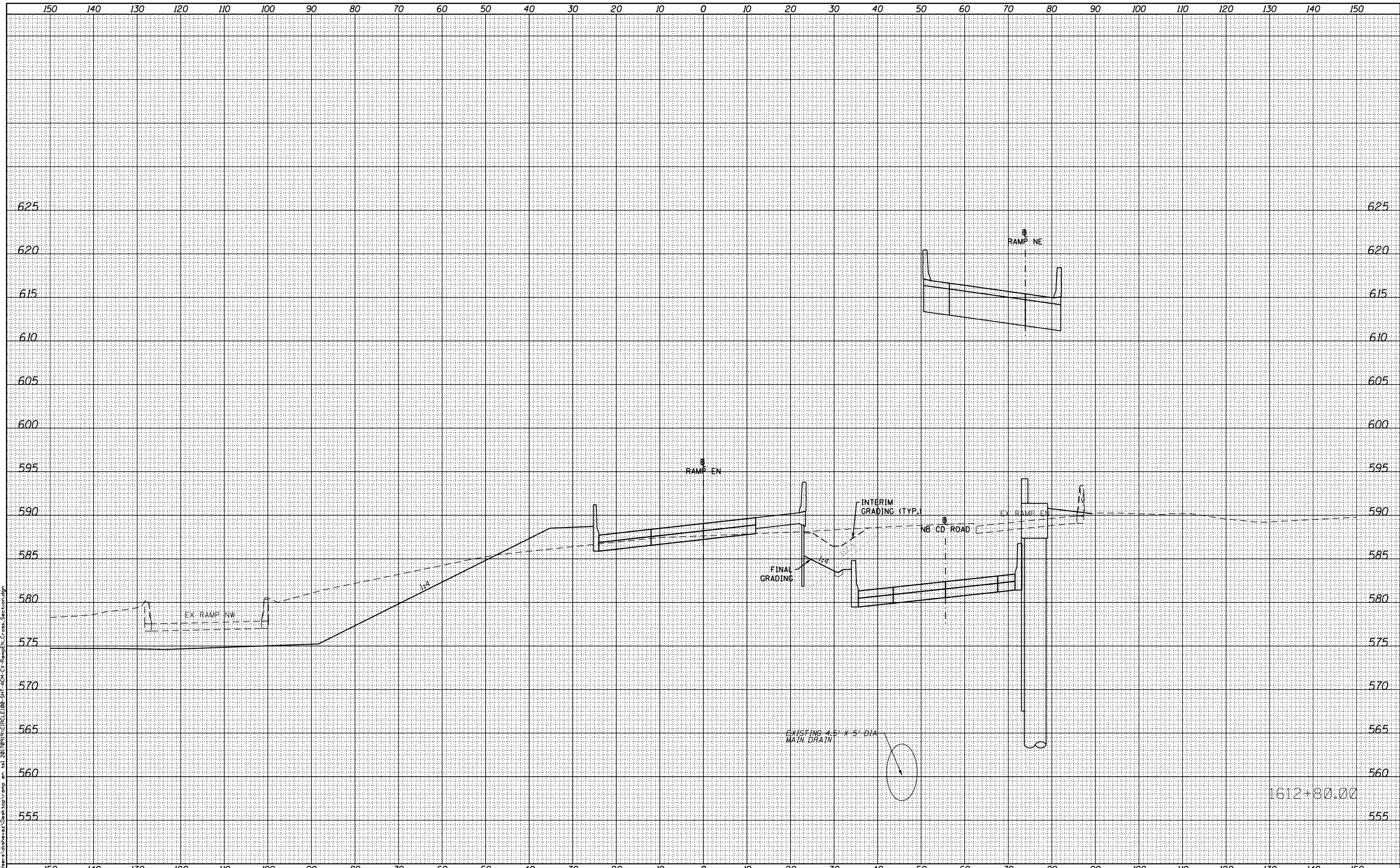
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CONTRACT NO.				
ILLINOIS FED. AID PROJECT				



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**STATE OF ILLINOIS  
DEPARTMENT OF TRANSPORTATION**

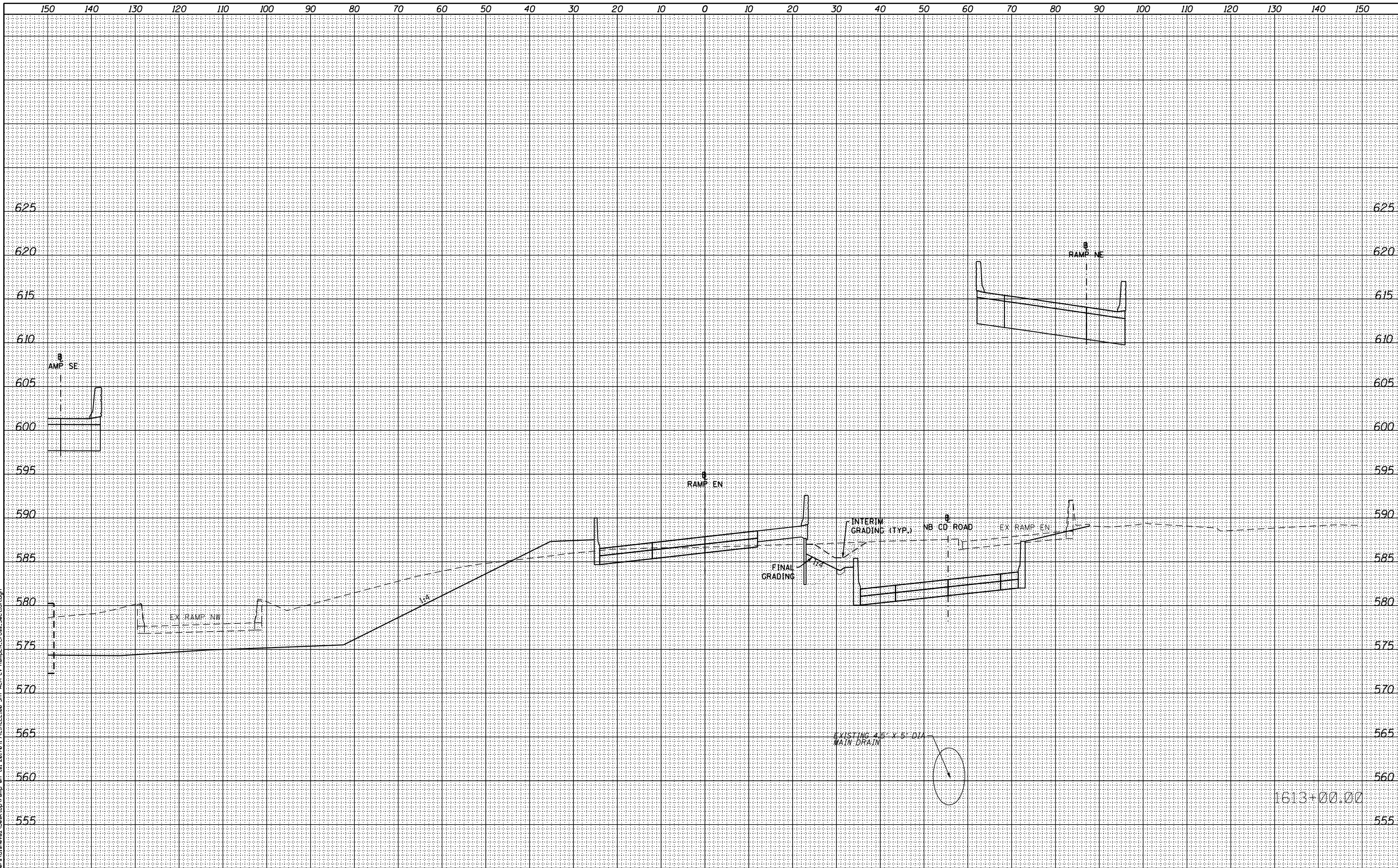
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CONTRACT NO.				
ILLINOIS FED. AID PROJECT				

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	NOTE BOOK TEMPLATE AREAS CHECKED

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1613+00.00



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**STATE OF ILLINOIS  
DEPARTMENT OF TRANSPORTATION**

**CROSS SECTIONS - RAMP EN**

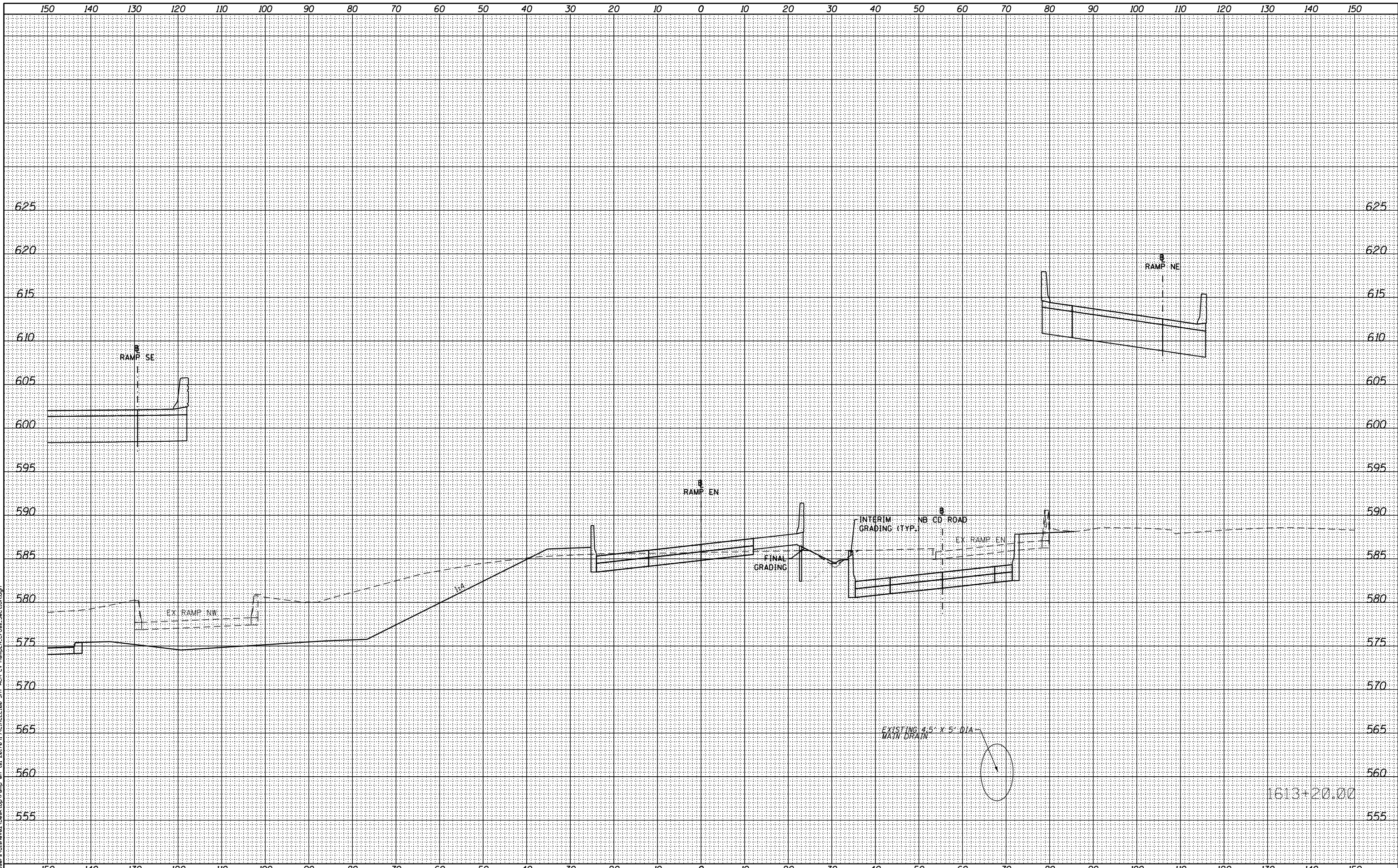
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F.A. RTE.	SECTION	COUNTY	TOTAL SHEETS	SHEET NO.
			36	
CONTRACT NO.				
ILLINOIS FED. AID PROJECT				

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NOTE BOOK	PLOTTED
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NOTE BOOK	PLOTTED
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**STATE OF ILLINOIS  
DEPARTMENT OF TRANSPORTATION**

**CROSS SECTIONS - RAMP EN**

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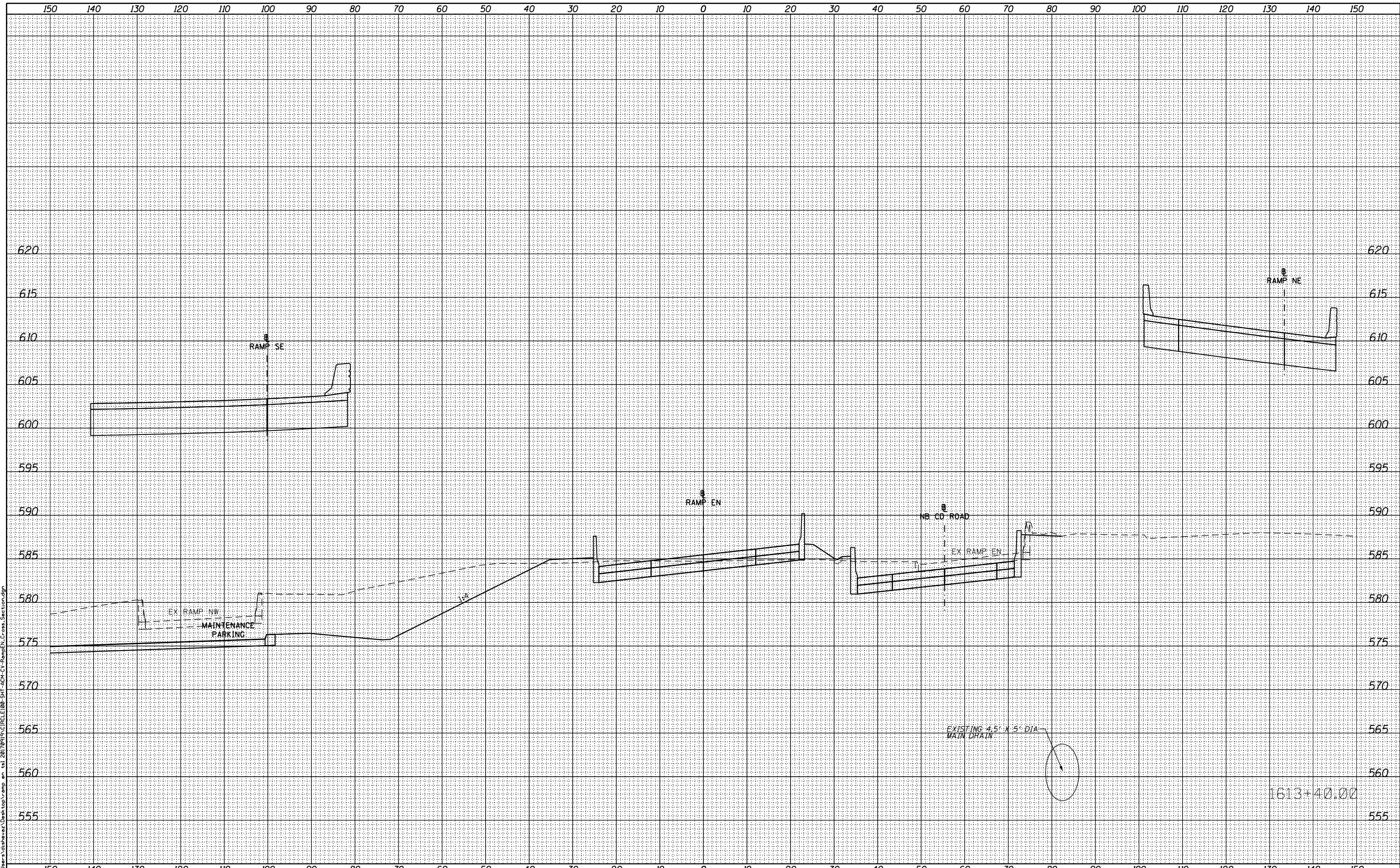
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CONTRACT NO.				
ILLINOIS FED. AID PROJECT				



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STATE OF ILLINOIS  
DEPARTMENT OF TRANSPORTATION

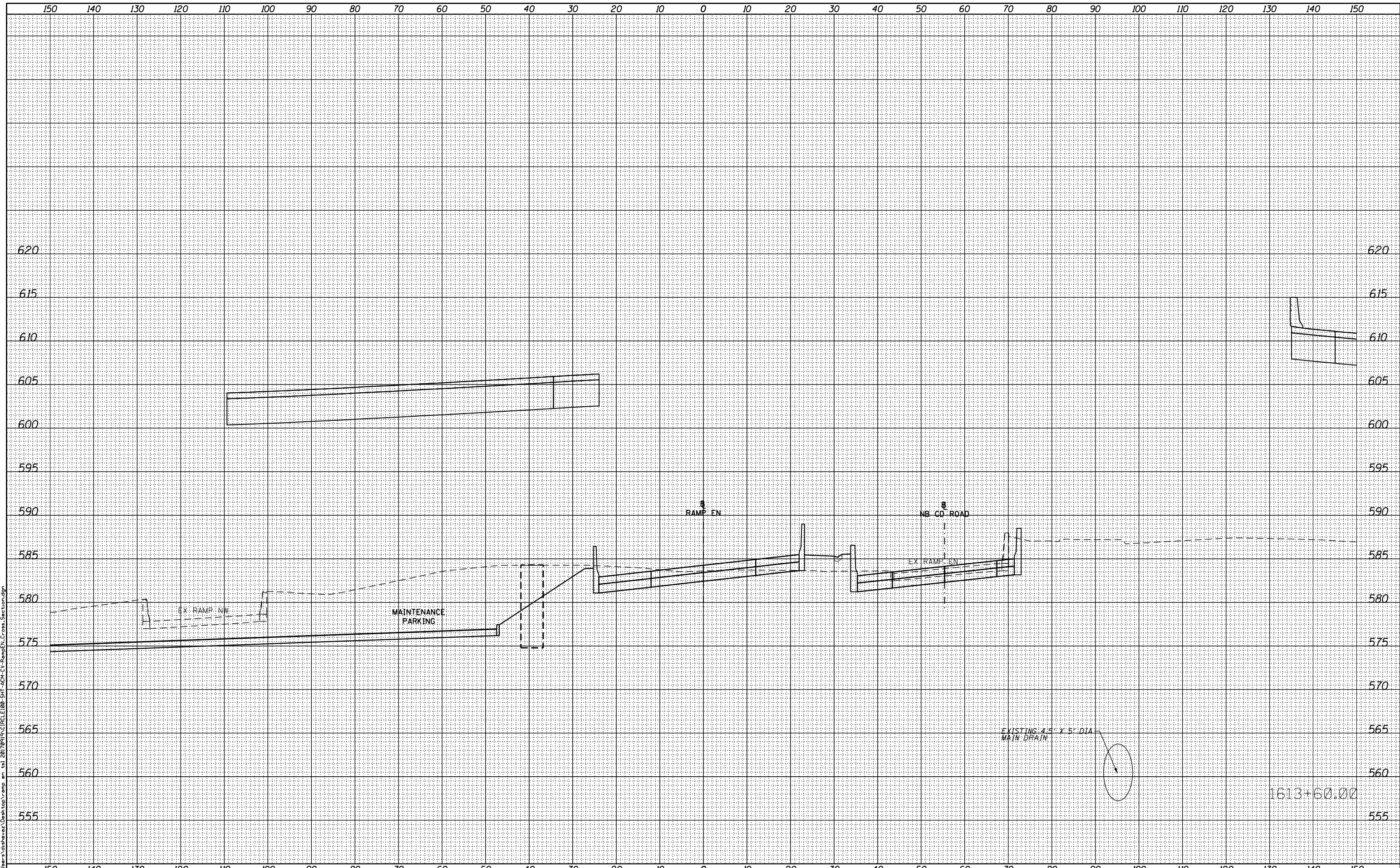
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CONTRACT NO.				
ILLINOIS FED. AID PROJECT				

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**STATE OF ILLINOIS  
DEPARTMENT OF TRANSPORTATION**

**CROSS SECTIONS - RAMP EN**

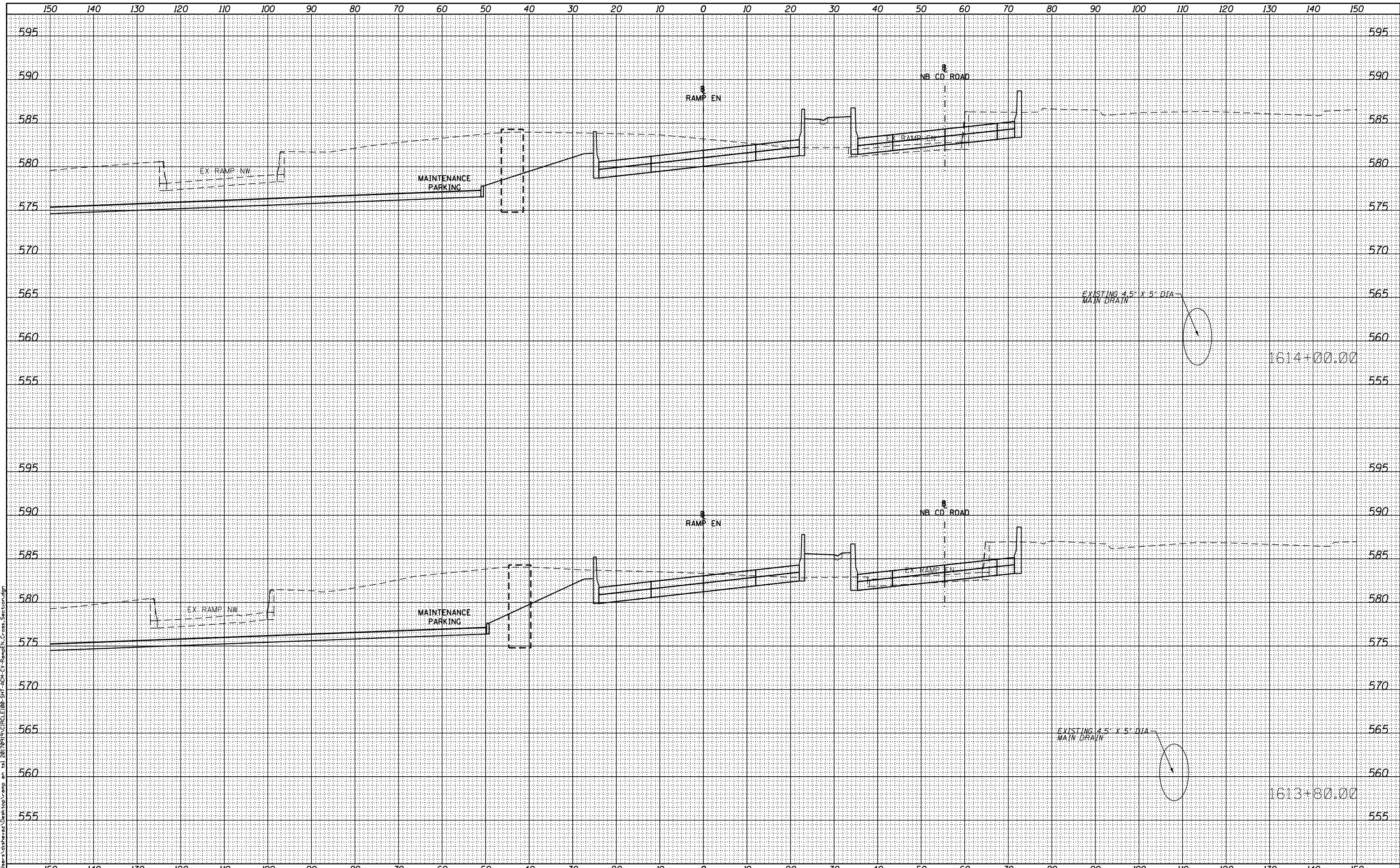
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F.A. RTE.	SECTION	COUNTY	TOTAL SHEETS 36	SHEET NO.
		CONTRACT NO.		
ILLINOIS FED. AID PROJECT				

DATE	
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ORIGINAL SURVEY	
NOTE BOOK NO.	
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NOTE BOOK NO.	
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**STATE OF ILLINOIS  
DEPARTMENT OF TRANSPORTATION**

CROSS SECTIONS - RAMP EN

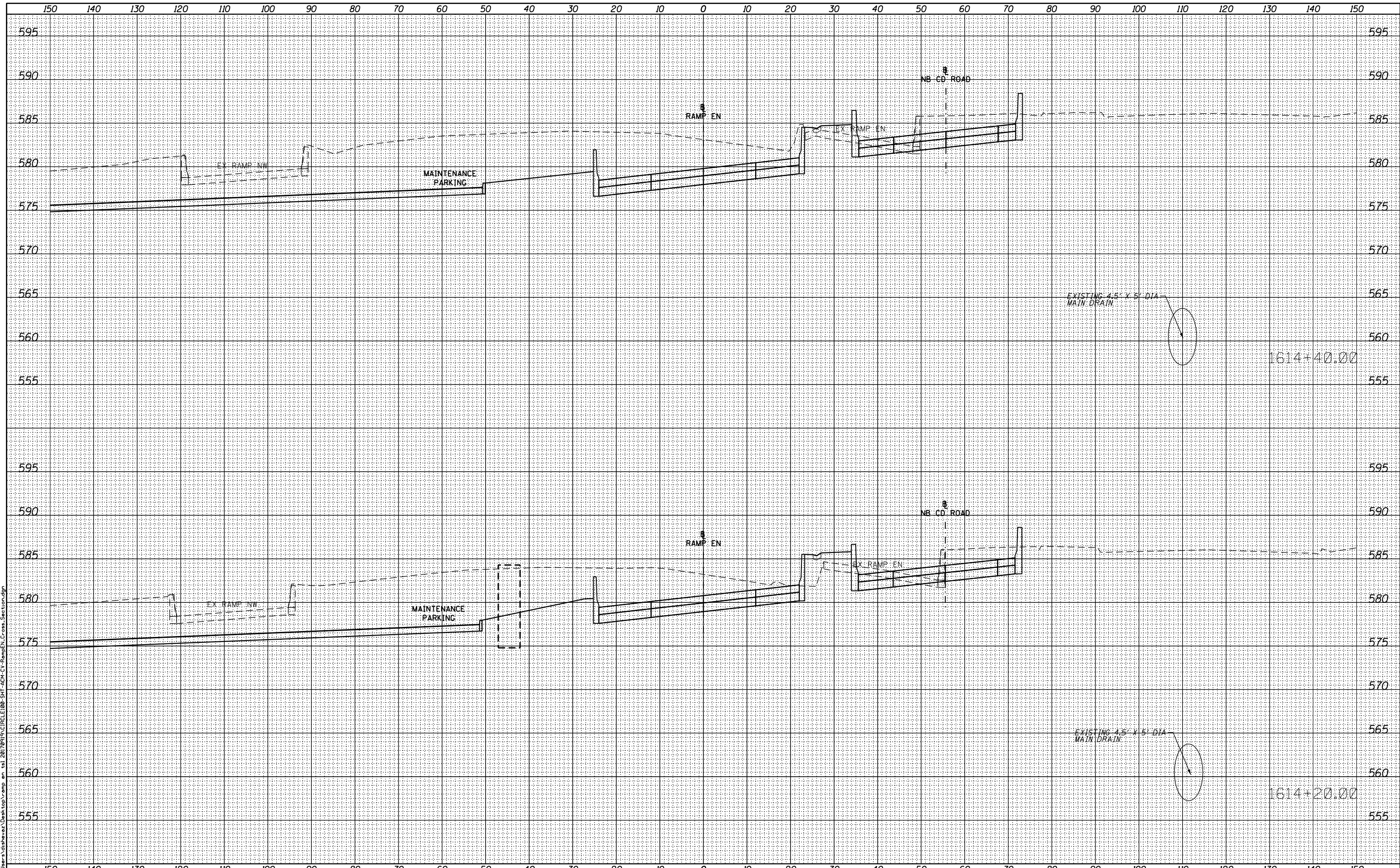
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F.A. RTE.	SECTION	COUNTY	TOTAL SHEETS	SHEET NO.
			36	
CONTRACT NO.				
ILLINOIS FED. AID PROJECT				

DATE	
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FINAL SURVEY	
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DATE	
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**STATE OF ILLINOIS  
DEPARTMENT OF TRANSPORTATION**

CROSS SECTIONS - RAMP EN

SCALE: SHEET 36 OF 36 SHEETS STA. 1614+20.00 TO STA. 1614+40.00

F.A. RTE.	SECTION	COUNTY	TOTAL SHEETS	SHEET NO.
			36	
CONTRACT NO.				
ILLINOIS FED. AID PROJECT				