

STRUCTURE GEOTECHNICAL REPORT

U.S. 20 over Kishwaukee River

Existing S.N. 101-0073 (EB) and 101-0074 (WB)
Proposed S.N. 101-0225 (EB) and S.N. 101-0226 (WB)



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TABLE OF CONTENTS

1.0	Project Description and Scope	1
1.1	Introduction.....	1
1.2	Project Description	1
1.3	Proposed Structure Information	1
2.0	Field Exploration and Generalized Subsurface Conditions	1
2.1	Subsurface Conditions.....	2
	Table 2.1.1 – Boring Information Summary	2
	Table 2.1.2 – Subsurface Profile Summary	2
2.2	Groundwater.....	3
3.0	Geotechnical Evaluations	3
3.1	Settlement	3
3.2	Slope Stability.....	3
	Table 3.2.1 – Slope Stability Critical FOS	4
3.3	Scour	4
3.4	Seismic Considerations	4
	Table 3.4.1 – Summary of Seismic Parameters.....	5
4.0	Foundation Evaluations and Design Recommendations	5
4.1	Driven Piles	5
	Table 4.1.1 - Preliminary Design Loads.....	5
	Table 4.1.2 - Estimated Pile Lengths for Metal Shell 12"Φ w/.25" walls	6
	Table 4.1.3 - Estimated Pile Lengths for Metal Shell 14"Φ w/.312" walls	6
	Table 4.1.4 - Estimated Pile Lengths for Metal Shell 16"Φ w/.312" walls	7
	Table 4.1.5 - Estimated Pile Lengths for HP 10x42 Steel H-Piles	8
	Table 4.1.6 - Estimated Pile Lengths for HP 12x53 Steel H-Piles	8
	Table 4.1.7 - Estimated Pile Lengths for HP 12x63 Steel H-Piles	9
	Table 4.1.8 - Estimated Pile Lengths for HP 14x73 Steel H-Piles	10
4.2	Lateral Pile Response.....	11
	Table 4.2.1 - Soil Parameters for Lateral Pile Load Analysis	11
5.0	Construction Considerations.....	14
5.1	Construction Activities	14
5.2	Temporary Sheet piling and Soil Retention	14
5.3	Cofferdams and Seal Coats.....	14

5.4	Site and Soil Conditions.....	15
6.0	Computations	15
7.0	Geotechnical Data.....	15
8.0	Limitations	15

EXHIBITS

- Exhibit A – Location Map
- Exhibit B – Boring Plan
- Exhibit C – Type, Size, and Location Plan (TS&L)
- Exhibit D – Boring Logs
- Exhibit E – Subsurface Profile
- Exhibit F – Slope/W Slope Stability Analysis
- Exhibit G – Pile Length/Pile Type

1.0 Project Description and Scope

1.1 Introduction

The geotechnical study summarized in this report was performed by Kaskaskia Engineering Group, LLC (KEG) for the replacement and expansion of the dual bridges carrying US 20 over the Kishwaukee River in Winnebago County, Illinois. The purpose of this report is to document subsurface geotechnical conditions, provide analyses of anticipated site conditions as they pertain to the project described herein, and to present design and construction recommendations for the proposed structure.

1.2 Project Description

The project consists of the replacement and widening of the US 20 dual bridges (SN 101-0073 EB and SN-101-0074 WB) over the Kishwaukee River in Winnebago County, Illinois. The structure is located about 3400 feet from the US 20 intersection with I-39. The existing bridges were built in 1962. Each existing structure consisted of a three (3) span with rolled shape steel girders and a concrete deck. Both bridges have a length of 230'-0" back-to-back of abutments and an out-to-out width of 35'-8".

The general location of the proposed structure is shown on a Location Map, Exhibit A. The site lies within the limits of the Rock River Hill Country of the Till Plain Section of the Central Lowland Province.

1.3 Proposed Structure Information

The proposed structures (SN 101-0225 EB and SN 101-0226 WB) will consist of two three-span steel girder bridges, which will be built on a 30° skew. Each bridge will provide three 12 ft.-wide driving lanes, a 10 ft.-wide outer shoulder, an 8.5 ft.-wide interior shoulder with a total width of 57 ft. – 5-inches out-to-out, in each direction. The proposed bridge centerline station will be at 1345+82.83 on US 20. The bridges will consist of three spans; the outer spans will measure 77'-6" and the central span will measure 115'-0", giving a total length of 270 ft. back-to-back of abutments. A Type, Size, and Location Plan (TS&L) is included in Exhibit C.

Further substructure details will be based on the findings of this Structure Geotechnical Report (SGR).

2.0 Field Exploration and Generalized Subsurface Conditions

The site exploration plan was developed and performed by KEG. A KEG representative was on-site to coordinate and log the borings, make site observations, and collect soil samples.

Eight standard penetration test (SPT) borings, designated SB-1, SB-2, SB-3, SB-4, SB-5, SB-6, SB-7, and SB-8 were drilled from July 12 through July 23, 2021. Borings SB-03, SB-04, SB-05 and SB-06 were drilled through the bridge deck and had around 35 to 40 feet of blind drilling to reach the ground surface. Boring Locations are shown on Exhibit B – Boring Plan. Detailed information regarding the nature and thickness of the soils encountered and the results of the field

sampling and laboratory testing are shown on the Boring Logs, Exhibit D. The soil profile for the above-mentioned borings can be found in Subsurface Profile, Exhibit E.

2.1 Subsurface Conditions

The profiles at the eight (8) boring locations exhibited layers of clay, clayey sand, clayey silt, gravelly sand, sand, sandy clay, sandy clay loam, sandy gravel, sandy loam, sandy silt, silt, and silty sand. Bedrock was not encountered in any of the borings, but evidence of a thin limestone layer was found in borings SB-01, SB-03, SB-04, SB-05, SB-06, SB-07, in depths around 30 and 45 feet. Table 2.1.1 shows a summary of the pavement structure and the ground surface elevation (GSE) of the borings. Borings SB-03, SB-04, SB-05, and SB-06, as mentioned, were blind drilling from the bridge deck, therefore the GSE represent the bridge deck elevations not the ground surface. A Summary of the general condition of the subsurface is described in Table 2.1.2.

Table 2.1.1 – Boring Information Summary

Designation	Asphalt (in)	Concrete (in)	Blind Drilling Casing (ft)	Depth (ft)	GSE (ft.)
SB-01	3.0	13.5	-	125.0	739.90
SB-02	4.5	12.0	-	75.00	739.99
SB-03	-	8.00	35.0	100.0	739.81
SB-04	-	8.25	40.0	100.0	739.96
SB-05	-	8.00	35.0	105.0	739.66
SB-06	-	8.25	40.0	100.0	739.91
SB-07	2.0	12.0	-	75.00	739.56
SB-08	4.0	12.0	-	125.0	739.87

Table 2.1.2 – Subsurface Profile Summary

Soil Type	N-Values (bpf)	Q _u (tsf)	WC (%)	Boring
Clay	9 to 59	1.0	18 to 36	SB-04, SB-07, SB-08
Clayey Sand	8 to 32	-	8 to 23	SB-01, SB-02, SB-07
Clayey Silt	10 to 61	0.30 to 1.70	11 to 27	SB-01, SB-02, SB-03, SB-05
Gravelly Sand	9 to 50/2"	-	7 to 20	SB-02, SB-04 through SB-08
Sand	5 to 78	-	4 to 29	All Borings
Sandy Clay	7 to 37	2.0 to 3.0	17 to 36	SB-01, SB-07, SB-08
Sandy Clay Loam	13 to 17	1.0	14 to 32	SB-02
Sandy Gravel	6 to 80	-	6 to 16	SB-01, SB-02, SB-06, SB-08
Sandy Loam	10 to 24	-	15 to 29	SB-02
Sandy Silty	15 to 31	0.40	17 to 22	SB-03, SB-08

Soil Type	N-Values (bpf)	Q _u (tsf)	WC (%)	Boring
Silt	22 to 48	0.5 to 1.0	17 to 23	SB-01 through SB-07
Silty Sand	40 to 52	-	14 to 18	SB-04, SB-07, SB-08

2.2 Groundwater

Due to the sandy nature of the natural soil, mud rotary wash was used during drilling, making it difficult to measure the groundwater table. Therefore, no groundwater level was obtained. It should be noted that the groundwater level is subject to seasonal and climatic variations, including fluctuations of the river. In addition, without extended periods of observation, measurement of true groundwater levels may not be possible.

3.0 Geotechnical Evaluations

3.1 Settlement

Since no significant grading or changes to the existing embankments are expected at the proposed structure, it is estimated that the existing embankments will experience no settlement. Therefore, no settlement calculations were performed for the proposed structure.

3.2 Slope Stability

A stability analysis using SLOPE/W was performed using the proposed bridge geometry on the TS&L and soil characteristics from Boring SB-01, SB-02, SB-07, and SB-08. Two conditions were modeled for each scenario: end-of-construction and long-term stability. A critical factor of safety (FOS) was calculated for each condition. According to the current standard of practice, the target FOS is 1.5 for end-of-construction and long-term slope stability. The slope stability analyses indicated that the required minimum FOS for all conditions were met.

In order to model the end-of-construction condition, full cohesion and a friction angle of 0 degrees were assumed, for cohesion soils. Nominal values for cohesion were used with full friction angle to model the long-term condition to analyze the theoretical condition where pore water pressure has dissipated. Nominal value was 100 and 150 psf for the cohesive soils, with friction angles between 26 and 30 degrees. $N_{60}-\phi'$ correlation by Wolff (1989) was used to determine the friction angles of cohesionless soils.

The Bishop Circular Method, which generates circular-shaped failure surfaces, was used to calculate the critical failure surfaces and FOS for the proposed conditions. The FOS obtained in the analysis is shown in Table 3.2.1. SLOPE/W program output from this analysis can be found in SLOPE/W Slope Stability Analysis, Exhibit F.

Table 3.2.1 – Slope Stability Critical FOS

Location (2H:1V Slope)	Critical FOS	
	End-of Construction	Long Term
WB West Abutment (SB-01)	2.3	1.6
WB East Abutment (SB-07)	2.2	1.5
EB West Abutment (SB-02)	1.6	1.5
WB West Abutment (SB-08)	1.8	1.5

3.3 Scour

The design scour elevations for the proposed structures are shown in Table 3.3.1 and Table 3.3.2. To reduce the potential for future scour, Stone Riprap Class A5 will be placed on the surface of the proposed abutments end slopes and Type II Cofferdams will be required around the piers.

Table 3.3.1 – Design Scour Elevations EB SN 101-0225 and WB SN 101-0226

Event/Limit State	Design Scour Elevations (ft.)				Item 113
	West Abutment	Pier 1	Pier 2	East Abutment	
Q ₁₀₀	731.14	704.52	704.52	730.77	5
Q ₂₀₀	731.14	701.84	701.84	730.77	
Design	731.14	704.52	704.52	730.77	
Check	731.14	701.84	701.84	730.77	

3.4 Seismic Considerations

The estimate of Seismic Site Class was based on the method described by IDOT AGMU Memo 09.1 - Seismic Site Class Definition and the IDOT provided spreadsheet titled: '*Seismic Site Class Determination*.' Using these resources, the controlling global site class for this project is Soil Site Class D.

Additional seismic parameters were calculated for use in the design of the structure. Published information and mapping from the USGS, including software directly applicable to the AASHTO Guide Specifications for LRFD Seismic Bridge Design, was used to develop the parameters for the bridge location. The values, based on Soil Site Class D, are summarized below.

Table 3.4.1 – Summary of Seismic Parameters

Parameter	Value
Soil Site Class	D
Spectral Response Acceleration, 0.2 Sec, S_{DS}	0.135g (Site Class D)
Spectral Response Acceleration, 1.0 Sec, S_{D1}	0.079g (Site Class D)
Seismic Performance Zone	1

As indicated in the table above, the Seismic Performance Zone is 1, based on S_{D1} and Table 3.15.2 in the IDOT Bridge Manual, the Soil Site Class D, and Figure 2.3.10-2 in the IDOT Bridge Manual.

4.0 Foundation Evaluations and Design Recommendations

4.1 Driven Piles

The foundations supporting the proposed bridge must provide sufficient support to resist dead and live loads. The IDOT Static Method uses the LRFD Pile Design Guide Procedure to estimate the pile lengths (Pile Length/Pile Type, Exhibit G).

The preliminary design loads, as provided by Alfred Benesch & Company are provided in Table 4.1.1 below.

Table 4.1.1 - Preliminary Design Loads

Structure	Substructure Unit	Factored Reactions (kips)
Westbound	West Abutment (SB-01)	1,500
	Pier 1 (SB-03)	3,630
	Pier 2 (SB-05)	3,630
	East Abutment (SB-07)	1,500
Eastbound	West Abutment (SB-02)	1,500
	Pier 1 (SB-04)	3,630
	Pier 2 (SB-06)	3,630
	East Abutment (SB-08)	1,500

The estimated pile lengths for applicable H-pile types and Metal Shell pile types are shown in Tables 4.1.2 through 4.1.8 below. The Nominal Required Bearing (R_N) represents the resistance the pile will experience during driving and will assist the contractor in selecting a proper hammer size. The Factored Resistance Available (R_F) documents the net long-term axial factored pile capacity available at the top of the pile to support factored substructure loadings.

Table 4.1.2 - Estimated Pile Lengths for Metal Shell 12"Φ w/.25" walls

Substructure Unit	R _n Nominal Required Bearing (kips)	R _F Factored Resistance Available (LRFD) (kips)	Estimated Pile Length (ft.)	Assumed Pile Cut-off Elevation (ft.)
WB - West Abutment (SB-01)	392	216	35	732.78
WB - Pier 1 (SB-03)	392	216	17	711.50
WB - Pier 2 (SB-05)	392	216	52	711.50
WB - East Abutment (SB-07)	392	216	25	732.41
EB - West Abutment (SB-02)	392	216	33	732.87
EB - Pier 1 (SB-04)	392	216	17	711.50
EB - Pier 2 (SB-06)	392	216	10	711.50
EB - East Abutment (SB-08)	392	216	30	732.50

Table 4.1.3 - Estimated Pile Lengths for Metal Shell 14"Φ w/.312" walls

Substructure Unit	R _n Nominal Required Bearing (kips)	R _F Factored Resistance Available (LRFD) (kips)	Estimated Pile Length (ft.)	Assumed Pile Cut-off Elevation (ft.)
WB - West Abutment (SB-01)	570	314	37	732.78
WB - Pier 1 (SB-03)	570	314	18	711.50
WB - Pier 2 (SB-05)	570	314	54	711.50
WB - East Abutment (SB-07)	570	314	26	732.41
EB - West Abutment (SB-02)	570	314	39	732.87

Substructure Unit	R _n Nominal Required Bearing (kips)	R _F Factored Resistance Available (LRFD) (kips)	Estimated Pile Length (ft.)	Assumed Pile Cut-off Elevation (ft.)
EB - Pier 1 (SB-04)	570	314	18	711.50
EB - Pier 2 (SB-06)	570	314	10	711.50
EB - East Abutment (SB-08)	570	314	33	732.50

Table 4.1.4 - Estimated Pile Lengths for Metal Shell 16"Φ w/.312" walls

Substructure Unit	R _n Nominal Required Bearing (kips)	R _F Factored Resistance Available (LRFD) (kips)	Estimated Pile Length (ft.)	Assumed Pile Cut-off Elevation (ft.)
WB - West Abutment (SB-01)	654	360	36	732.78
WB - Pier 1 (SB-03)	654	360	17	711.50
WB - Pier 2 (SB-05)	654	360	54	711.50
WB - East Abutment (SB-07)	654	360	26	732.41
EB - West Abutment (SB-02)	654	360	37	732.87
EB - Pier 1 (SB-04)	654	360	17	711.50
EB - Pier 2 (SB-06)	654	360	10	711.50
EB - East Abutment (SB-08)	654	360	32	732.50

Table 4.1.5 - Estimated Pile Lengths for HP 10x42 Steel H-Piles

Substructure Unit	R _n Nominal Required Bearing (kips)	R _F Factored Resistance Available (LRFD) (kips)	Estimated Pile Length (ft.)	Assumed Pile Cut-off Elevation (ft.)
WB - West Abutment (SB-01)	335	184	89	732.78
WB - Pier 1 (SB-03)	335	184	82	711.50
WB - Pier 2 (SB-05)	335	184	98	711.50
WB - East Abutment (SB-07)	335	184	88	732.41
EB - West Abutment (SB-02)	335	184	--	732.87
EB - Pier 1 (SB-04)	335	184	78	711.50
EB - Pier 2 (SB-06)	335	184	74	711.50
EB - East Abutment (SB-08)	335	184	84	732.50

Table 4.1.6 - Estimated Pile Lengths for HP 12x53 Steel H-Piles

Substructure Unit	R _n Nominal Required Bearing (kips)	R _F Factored Resistance Available (LRFD) (kips)	Estimated Pile Length (ft.)	Assumed Pile Cut-off Elevation (ft.)
WB – West Abutment (SB-01)	418	230	89	732.78
WB - Pier 1 (SB-03)	418	230	81	711.50
WB - Pier 2 (SB-05)	418	230	98	711.50
WB - East Abutment (SB-07)	418	230	88	732.41

Substructure Unit	R _n Nominal Required Bearing (kips)	R _F Factored Resistance Available (LRFD) (kips)	Estimated Pile Length (ft.)	Assumed Pile Cut-off Elevation (ft.)
EB - West Abutment (SB-02)	418	230	--	732.87
EB - Pier 1 (SB-04)	418	230	77	711.50
EB - Pier 2 (SB-06)	418	230	74	711.50
EB - East Abutment (SB-08)	418	230	84	732.50

Table 4.1.7 - Estimated Pile Lengths for HP 12x63 Steel H-Piles

Substructure Unit	R _n Nominal Required Bearing (kips)	R _F Factored Resistance Available (LRFD) (kips)	Estimated Pile Length (ft.)	Assumed Pile Cut-off Elevation (ft.)
WB - West Abutment (SB-01)	497	273	97	732.78
WB - Pier 1 (SB-03)	497	273	--	711.50
WB - Pier 2 (SB-05)	497	273	--	711.50
WB - East Abutment (SB-07)	497	273	96	732.41
EB - West Abutment (SB-02)	497	273	--	732.87

Substructure Unit	R _n Nominal Required Bearing (kips)	R _F Factored Resistance Available (LRFD) (kips)	Estimated Pile Length (ft.)	Assumed Pile Cut-off Elevation (ft.)
EB - Pier 1 (SB-04)	497	273	--	711.50
EB - Pier 2 (SB-06)	497	273	83	711.50
EB - East Abutment (SB-08)	497	273	89	732.50

Table 4.1.8 - Estimated Pile Lengths for HP 14x73 Steel H-Piles

Substructure Unit	R _n Nominal Required Bearing (kips)	R _F Factored Resistance Available (LRFD) (kips)	Estimated Pile Length (ft.)	Assumed Pile Cut-off Elevation (ft.)
WB - West Abutment (SB-01)	578	318	95	732.78
WB - Pier 1 (SB-03)	578	318	--	711.50
WB - Pier 2 (SB-05)	578	318	--	711.50
WB - East Abutment (SB-07)	578	318	92	732.41
EB - West Abutment (SB-02)	578	318	--	732.87
EB - Pier 1 (SB-04)	578	318	--	711.50
EB - Pier 2 (SB-06)	578	318	78	711.50

Substructure Unit	R _n Nominal Required Bearing (kips)	R _F Factored Resistance Available (LRFD) (kips)	Estimated Pile Length (ft.)	Assumed Pile Cut-off Elevation (ft.)
EB - East Abutment (SB-08)	578	318	87	732.50

As shown in the Tables above and in Pile Length/Pile Type, Exhibit G, scour has been included at the substructure locations. Downdrag and liquefaction have not.

KEG recommends one test pile be performed, at a minimum. A test pile is performed prior to production driving so that actual, on-site field data can be gathered to determine pile driving requirements for the project. This is also the way the contractor's proposed equipment and methodologies identified in their Pile Installation Plan can be assessed.

The piles are expected to be driven into sandy gravel and gravelly sand layers that present cobbles in their composition. Therefore, pre-coring should not be required to reach estimated embedment depths. KEG recommends using pile tips or metal shell conical tips to facilitate driving, protect piles from damage, and avoid sudden overstress.

4.2 Lateral Pile Response

Generally, the geotechnical engineer provides soil parameters to the structural engineer so that an L-Pile program or other approved software can be used for the lateral or displacement analysis of the foundations. Table 4.2.1 is included for the structural engineer's use in evaluating lateral pile response. The values were estimated based on the descriptions listed on the boring logs. No specific hydrometer analyses were performed on the site soils.

Table 4.2.1 - Soil Parameters for Lateral Pile Load Analysis

Boring	Soil Description	Elev. at the Bottom of Layer	γ (pcf)	Undrained Parameters		N Value (Average)	Assumed % fines < #200	K (pci)	ε ₅₀
				c (psf)	Φ (deg.)				
SB-01	Clayey Sand	736.4	120	-	29	8	25	25	-
	Sand	731.9	115	-	33	25	3	90	-
	Sandy Loam	723.4	120	-	32	17	35	90	-
	Sandy Clay	716.9	120	2500	0	11	45	1000	0.005
	Sand	714.4	115	-	35	26	3	90	-
	Sandy Gravel	706.9	120	-	35	25	3	-	-
	Coarse Sand	692.9	115	-	35	23	3	90	-
	Silt	685.4	110	1000	0	43	85	2000	0.004
	Fine Sand	671.4	115	-	45	58	5	225	-
	Silt	670.4	110	1000	0	67	85	2000	0.004
	Fine Sand	667.9	115	-	47	67	5	225	-
	Clayey Silt	660.9	110	1700	0	61	65	500	0.007
	Fine Sand	627.9	115	-	40	41	5	225	-

Boring	Soil Description	Elev. at the Bottom of Layer	γ (pcf)	Undrained Parameters		N Value (Average)	Assumed % fines < #200	K (pci)	ε ₅₀
				c (psf)	Φ (deg.)				
	Sand	614.9	115	-	43	51	3	225	-
SB-02	Sandy Loam	737	120	-	29	10	35	90	-
	Sand	729	115	-	34	24	3	90	-
	Clayey Sand	726.5	120	-	30	12	25	90	-
	Clayey Silt	725.5	110	1000	0	18	65	100	0.01
	Sand	724	115	-	33	18	3	90	-
	Sandy clay loam	715.5	120	-	32	16	45	90	-
	Sandy Gravel	714	120	-	31	13	3	-	-
	Gravelly Sand	691	120	-	35	24	3	90	-
	Sand	686	115	-	39	38	3	225	-
	Clayey Silt	683.5	110	1500	0	44	65	500	0.007
	Sand	673.5	115	-	41	46	3	225	-
	Silt	665	110	1000	0	44	85	2000	0.004
SB-03	Clayey Silt	710.8	110	1000	0	11	65	100	0.01
	Coarse Sand	707.3	115	-	30	9	3	25	-
	Sand	706.8	115	-	30	9	3	25	-
	Coarse Sand	694.3	115	-	33	18	3	90	-
	Sand	689.3	115	-	50	77	3	225	-
	Fine Sand	686.8	115	-	34	21	5	90	-
	Sand	682.8	115	-	36	26	3	90	-
	Silt	678.3	110	700	0	22	85	100	0.01
	Sandy Silt	672.8	115	-	32	16	25	90	-
	Sand	662.8	115	-	32	15	3	90	-
	Clayey Silt	650.8	110	900	0	32	65	100	0.01
	Fine Sand	639.8	115	-	41	44	5	225	-
SB-04	Clay	715.5	120	1000	0	34	85	100	0.01
	Gravelly Sand	709	120	-	33	19	3	90	-
	Sand	704.5	115	-	34	21	3	90	-
	Gravelly Sand	688	120	-	38	34	3	225	-
	Sand	668.5	115	-	40	41	3	225	-
	Silty Sand	663	115	-	42	47	25	225	-
	Silt	658	110	900	0	29	85	100	0.01
	Sand	640	115	-	44	55	3	225	-
SB-05	Sand	712.7	115	-	30	10	3	90	-
	Coarse Sand	694.2	115	-	35	23	3	90	-
	Gravelly Sand	689.2	120	-	36	27	3	90	-
	Fine Sand	682.7	115	-	34	21	5	90	-
	Silt	681.2	110	1000	0	26	85	100	0.01

Boring	Soil Description	Elev. at the Bottom of Layer	γ (pcf)	Undrained Parameters		N Value (Average)	Assumed % fines < #200	K (pci)	ε ₅₀
				c (psf)	Φ (deg.)				
	Clayey Silt	677.7	110	3000	0	38	65	1000	0.005
	Silt	672.7	110	500	0	46	85	30	0.02
	Sand	662.7	115	-	42	49	3	225	-
	Clayey Silt	651.2	110	1300	0	22	65	500	0.007
	Sand	634.7	115	-	41	46	3	225	-
SB-06	Gravelly Sand	710.4	120	-	32	15	3	90	-
	Sand	704.9	115	-	38	35	3	225	-
	Gravelly Sand	696.9	120	-	38	35	3	225	-
	Sandy Gravel	691.9	120	-	38	33	3	-	-
	Sand	686.9	115	-	36	27	3	90	-
	Silt	677.9	110	500	0	34	85	30	0.02
	Sand	655.4	115	-	45	57	3	225	-
	Silt	647.9	110	1000	0	43	85	100	0.01
SB-07	Sand	639.9	115	-	46	61	3	225	-
	Sandy Clay	735.6	120	2000	0	12	45	500	0.007
	Sand	725.1	115	-	35	28	3	90	-
	Clayey Sand	720.6	120	-	36	29	25	90	-
	Sand	718.6	115	-	32	17	3	90	-
	Clay	718.1	120	1000	0	9	85	100	0.01
	Sand	716.6	115	-	30	9	3	25	-
	Coarse Sand	714.1	115	-	39	38	3	225	-
	Gravelly Sand	711.6	120	-	35	23	3	90	-
	Coarse Sand	699.6	115	-	39	37	3	225	-
	Sand	692.6	115	-	35	25	3	90	-
	Coarse Sand	687.6	115	-	43	53	3	225	-
	Fine Sand	682.6	115	-	40	39	5	225	-
	Silt	679.6	110	1000	0	46	85	100	0.01
	Silty Sand	675.6	115	-	43	52	25	225	-
	Fine Sand	664.6	115	-	44	56	5	225	-
SB-08	Sand	736.9	115	-	29	10	3	90	-
	Sandy Clay	734.4	120	2000	0	16	45	500	0.007
	Gravelly Sand	722.9	120	-	34	23	3	90	-
	Clay	717.9	120	1000	0	17	85	100	0.01
	Sand	715.4	115	-	33	20	3	90	-
	Sandy Gravel	711.9	120	-	32	15	3	-	-
	Gravelly Sand	697.9	120	-	35	25	3	90	-
	Sandy Gravel	685.9	120	-	45	60	3	-	-
	Sand	681.9	115	-	41	43	3	225	-

Boring	Soil Description	Elev. at the Bottom of Layer	γ (pcf)	Undrained Parameters		N Value (Average)	Assumed % fines < #200	K (pci)	ϵ_{50}
				c (psf)	Φ (deg.)				
	Silty Sand	677.9	115	-	40	40	25	225	-
	Sand	655.4	115	-	45	57	3	225	-
	Sandy Silt	647.9	115	-	34	22	25	90	-
	Sand	645.4	115	-	39	37	3	225	-
	Sandy Clay	642.9	120	2500	0	37	45	1000	0.005
	Sand	617.9	115	-	43	52	3	225	-
	Coarse Sand	614.9	115	-	42	48	3	225	-

5.0 Construction Considerations

5.1 Construction Activities

Construction activities should be performed in accordance with the current IDOT Standard Specifications for Road and Bridge Construction and any pertinent Special Provisions or Policies.

Should any design considerations assumed by KEG change, KEG should be contacted to determine if the recommendations stated in this report still apply.

5.2 Temporary Sheet piling and Soil Retention

Temporary Sheet piling would be required at various phases of this project due to the proposed staged construction layout shown in the TS&L. The soil at the site indicates that temporary sheet piling is feasible. Temporary sheet piling shall be designed by the engineer responsible for the Contract plans. The contractor is responsible for retaining an Illinois Licensed Structural Engineer to detail the design of temporary soil retention systems.

5.3 Cofferdams and Seal Coats

Cofferdams will be required at the proposed pier locations. The estimated water surface elevation (E.W.S.E.) is listed as El. 716.75, making it greater than six ft. above the bottom elevation of the substructure. Therefore, a Type 2 cofferdam will be required. All cofferdams are required to be dewatered. Sand and gravel are present at the cofferdams' site, requiring a seal coat. A seal coat will reduce the potential for water to seep beneath the sheet piling in the dewatered cofferdam. As per the 2012 IDOT Bridge Manual, General Note 28 shall be added to the plans when a seal coat is specified.

The contractor is required to retain an Illinois-licensed structural engineer to design the cofferdams. Per the Bridge Manual, the plans and computations shall be submitted to the Bureau of Bridges and Structures for review and final approval before beginning any work on the structure.

5.4 Site and Soil Conditions

Provisions of the Standard Specifications should adequately address site and soil conditions.

6.0 Computations

Computations and analyses for special circumstances, if any, are included as exhibits. Please refer to each section of the report for reference to the exhibit containing any such calculations or analysis used.

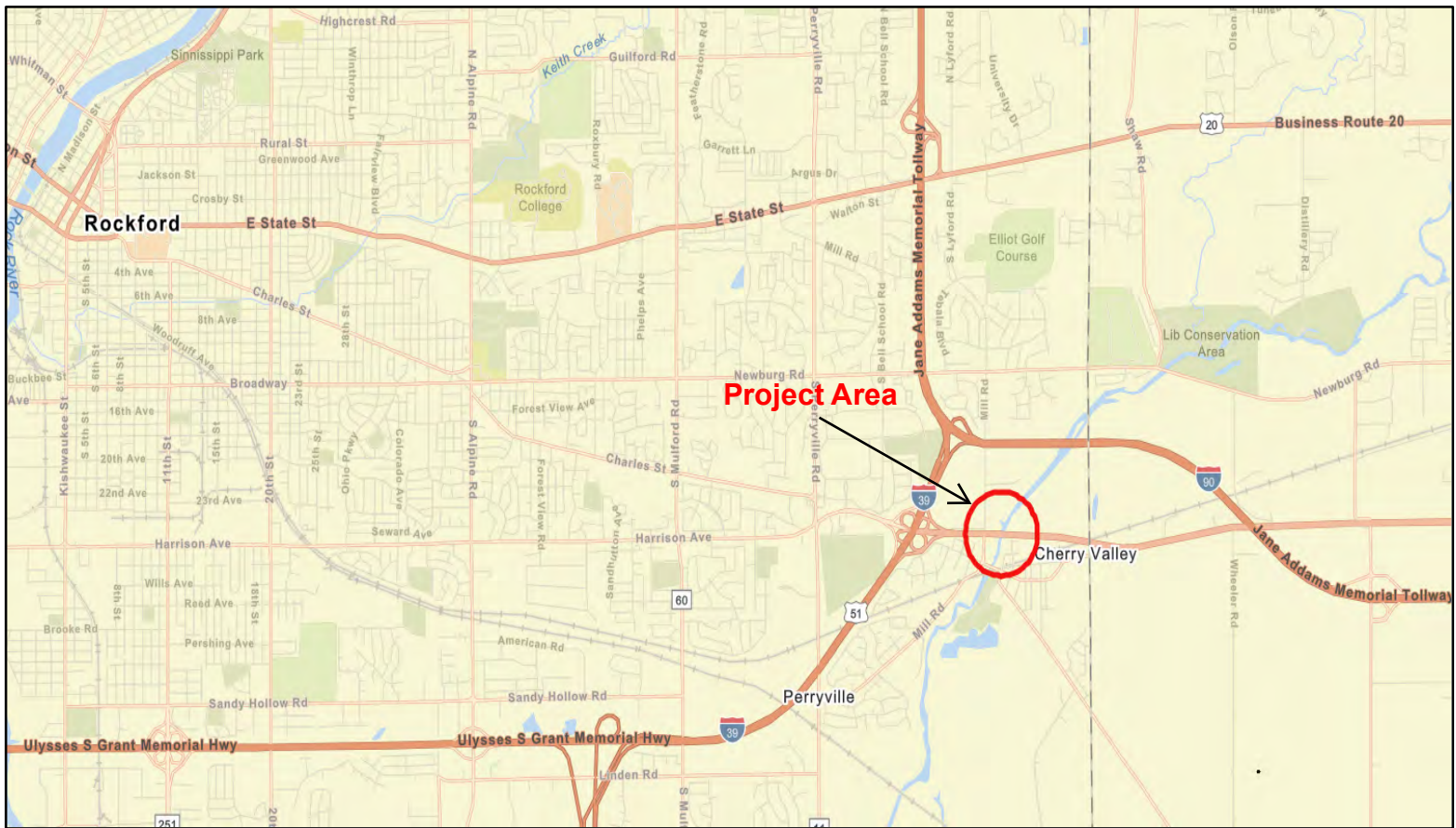
7.0 Geotechnical Data

Soil boring logs can be found in Exhibit D. The Subsurface Profile can be found in Exhibit E.

8.0 Limitations

The recommendations provided herein are for the exclusive use of the Illinois Department of Transportation (IDOT) District 2 and Alfred Benesch and Company. They are specific only to the project described. They are based on the subsurface information obtained by KEG at eight boring locations within the structure area, KEG's understanding of the project as described herein, and geotechnical engineering practice consistent with the standard of care. No other warranty is expressed or implied. KEG should be contacted if conditions encountered during construction are inconsistent with those described.

EXHIBIT A
LOCATION MAP



LOCATION MAP

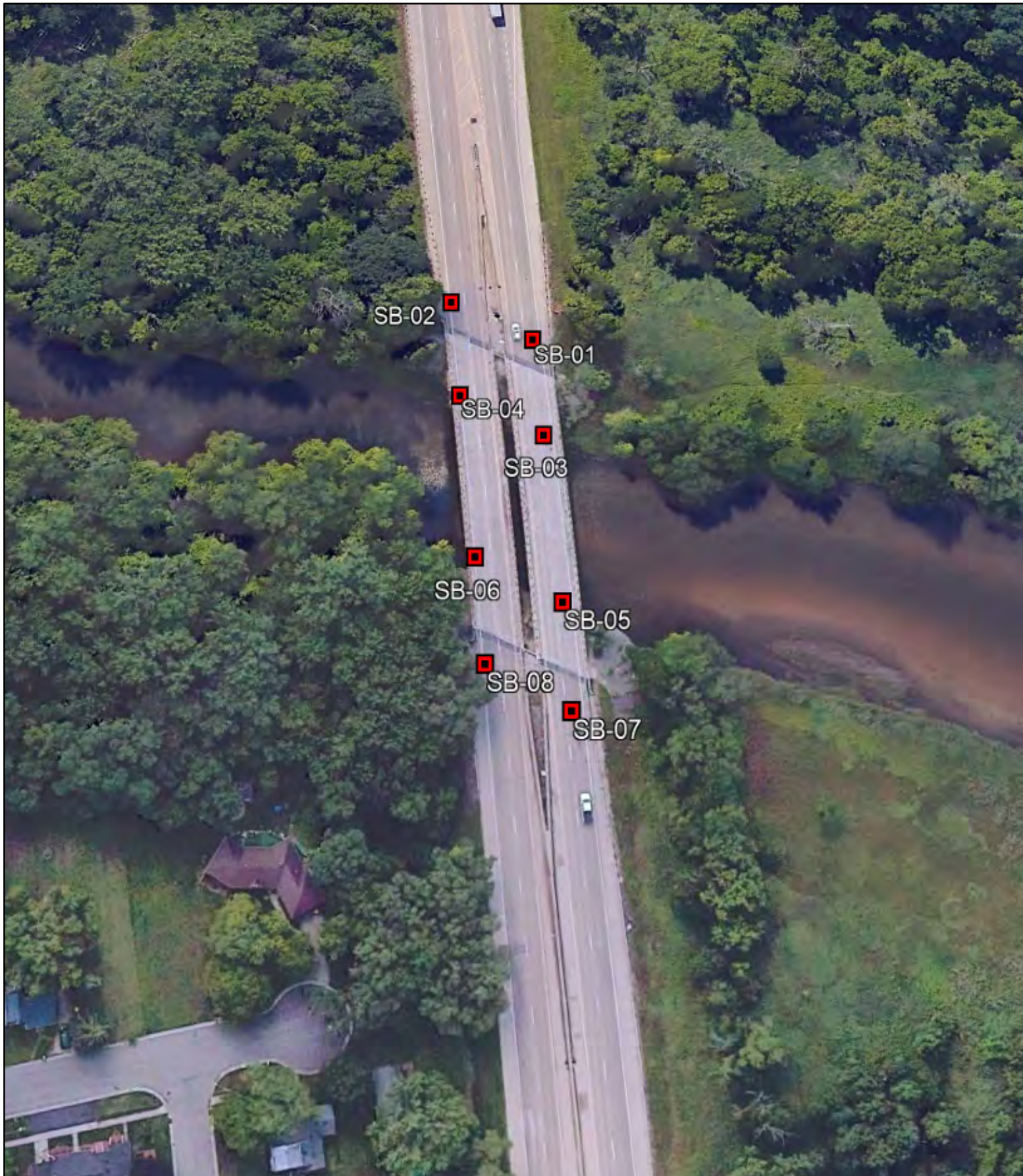
US 20 over Kishwaukee River
Winnebago County, Illinois

Exhibit No.

A

KEG JOB #19-1138.00

EXHIBIT B
BORING PLAN



BORING LOCATION MAP
US 20 over Kishwaukee River
Winnebago County, Illinois

Exhibit No.

B

KEG JOB #19-1138.00

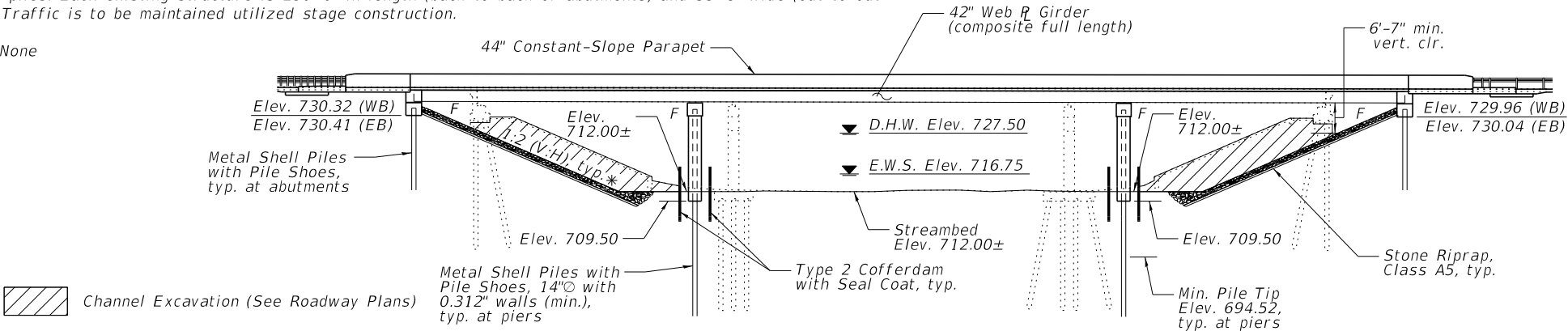
EXHIBIT C

TYPE, SIZE, AND LOCATION PLAN (TS&L)

Benchmark: McClure Benchmark Disk on northwest wingwall of westbound lane of US Rte. 20 over Kishwaukee River, approx. 600 ft east of Mill Road. Elevation 740.674.

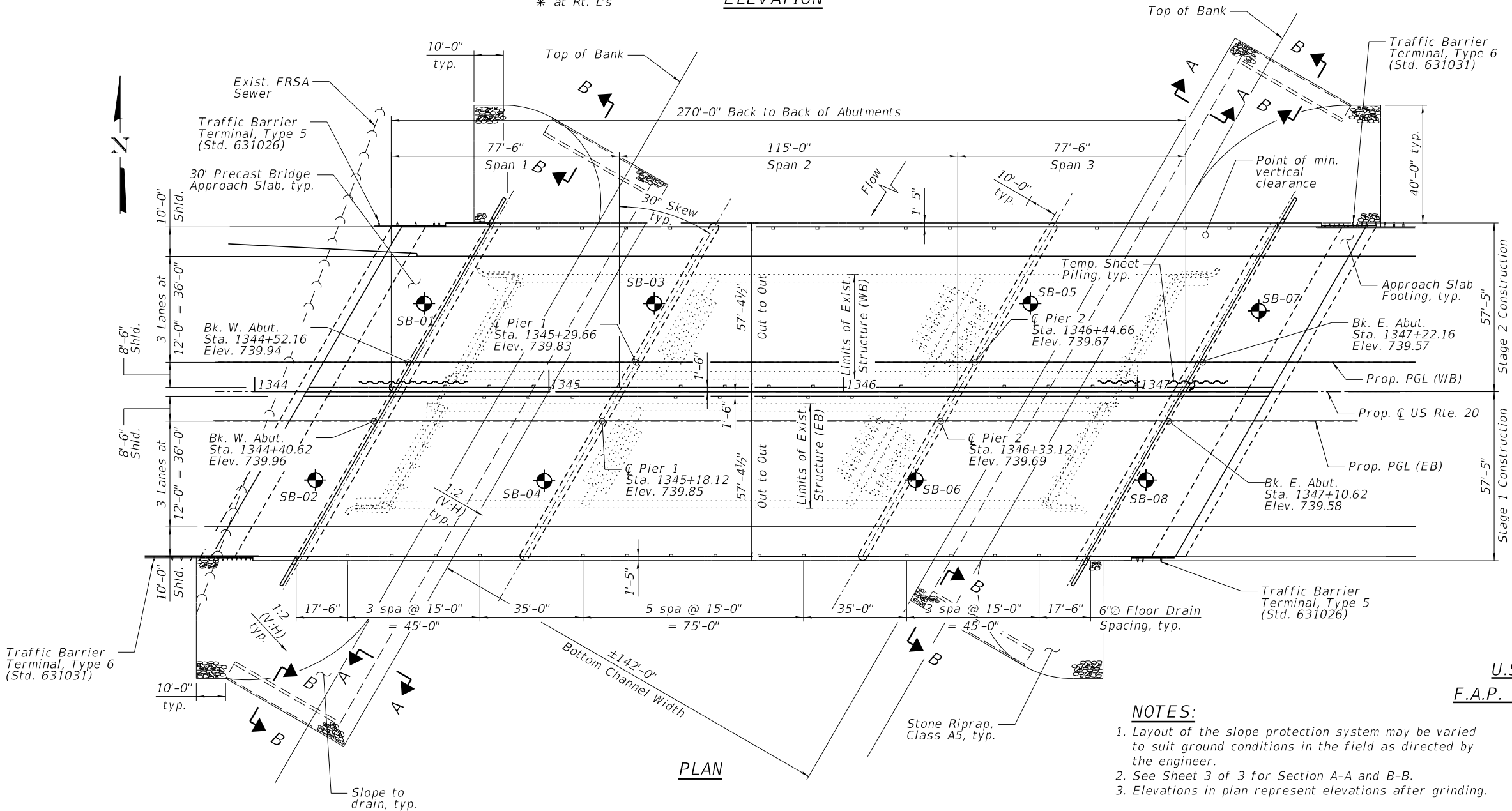
Existing Structure: SN 101-0073 (EB) and SN 101-0074 (WB) were constructed in 1962 as Project F-284(18) under Section No. 6-B for FA Route 194. Each structure is a three (3) span bridge with rolled shape steel girders and a non-composite concrete deck. The substructure is supported by stub abutments founded on concrete piles and trapezoidal piers founded on timber piles. Each existing structure is 230'-0" in length (back-to-back of abutments) and 35'-8" wide (out-to-out of deck). Traffic is to be maintained utilized stage construction.

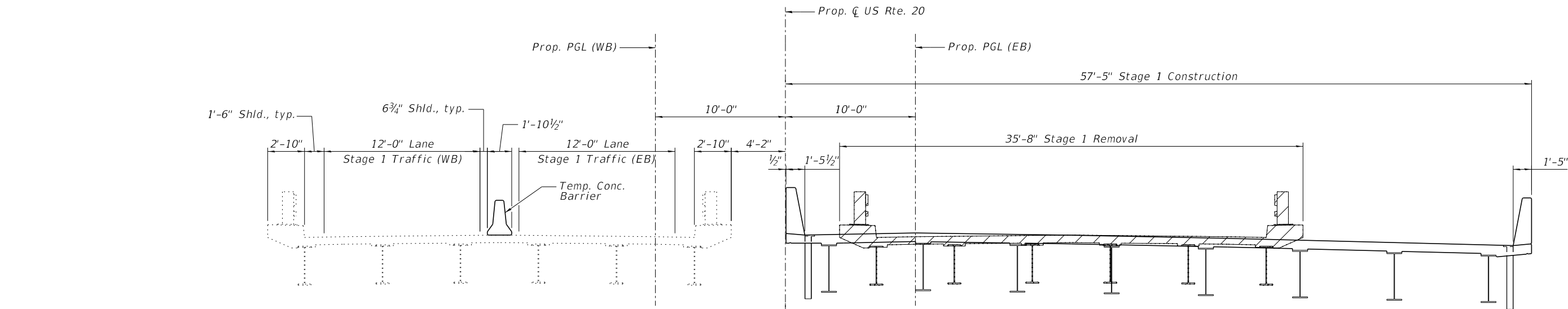
Salvage: None



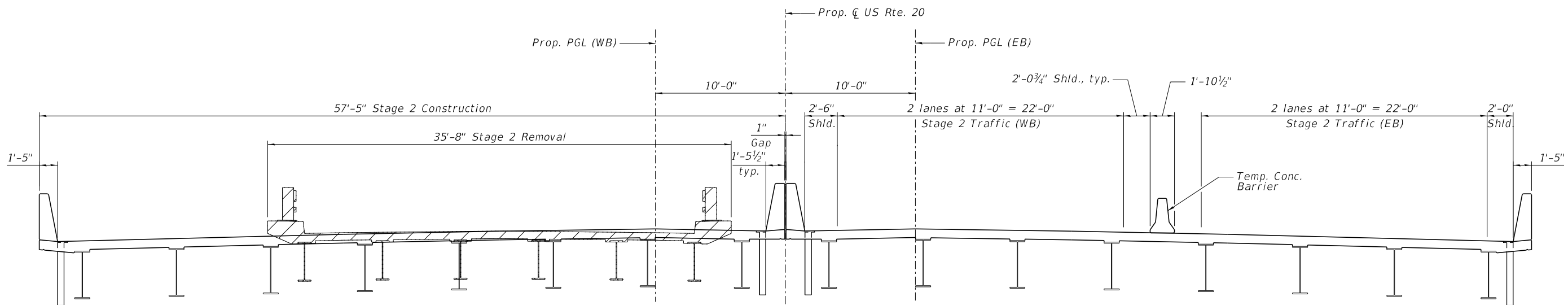
* at Rt. L's

ELEVATION





STAGE 1
(Looking east)



STAGE 2
(Looking east)

STAGE CONSTRUCTION DETAILS
U.S. ROUTE 20 OVER KISHWAUKEE RIVER
F.A.P. ROUTE 301 - SECTION (201-3)K & (4-1, 5)R
WINNEBAGO COUNTY
STATION 1345+82.83
STRUCTURE NO. 101-0225 (EB)
STRUCTURE NO. 101-0226 (WB)

NOTES:

- Existing piers shall be removed to top of existing footing in each stage.

STATE OF ILLINOIS
DEPARTMENT OF TRANSPORTATION

SHEET 2 OF 3 SHEETS

F.A.P. RTE.	SECTION	COUNTY	TOTAL SHEETS	SHEET NO.
301	(201-3)K & (4-1, 5)R	WINNEBAGO		
CONTRACT NO. 64R72				
ILLINOIS FED. AID PROJECT				

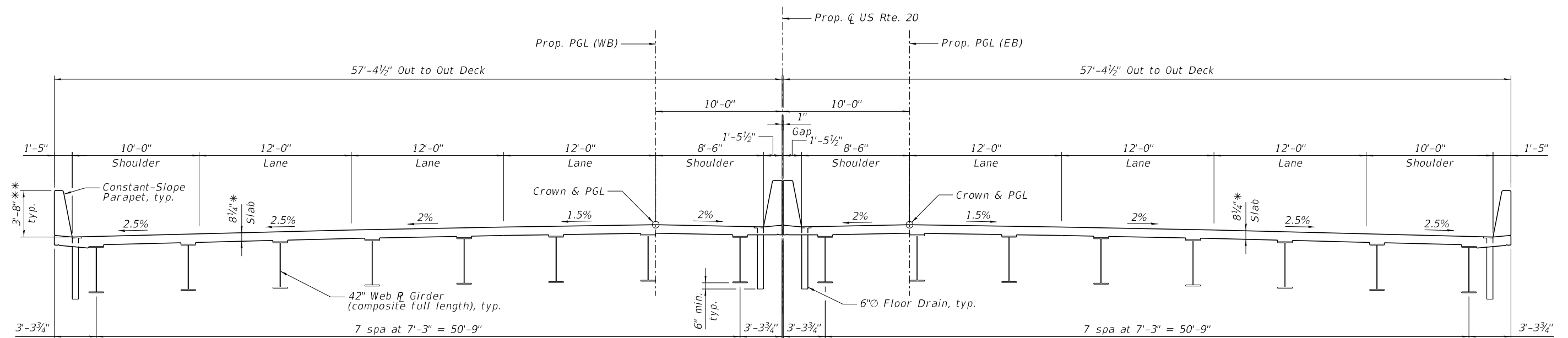
MODEL: SMODELNAMES
FILE NAME: \$FILES



Alfred Benesch & Company
35 W. Wacker Drive, Suite 3300
Chicago, Illinois 60601
312-565-0450 Job No. 10800

USER NAME =	DESIGNED - JPM	REVISED -
	CHECKED - MFH	REVISED -
PLOT SCALE =	DRAWN - JPM	REVISED -
PLOT DATE =	CHECKED - MFH	REVISED -

SDATE\$ \$TIME\$



EXHBIT D
BORING LOGS

ROUTE	FAP Route 301	DESCRIPTION	PTB 193-20 I-39 and U.S. 20 D2	LOGGED BY	KEG
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SECTION (201-3)K&(4-1,5)R **LOCATION** US-20 over Kishwaukee River

COUNTY Winnebago DRILLING METHOD MUD ROTARY HAMMER TYPE AUTO

STRUCT. NO.	101-0074		D E P T H	B L O W S	U C S	M O I S T	Surface Water Elev.		ft	D E P T H	B L O W S	U C S	M O I S T
Station	1345+79.08		(ft)	(/6")	(tsf)	(%)	Stream Bed Elev.		ft	(ft)	(/6")	(tsf)	(%)
BORING NO.	SB-01						Groundwater Elev.:						
Station	1344+57.6						First Encounter		ft				
Offset	30.0 ft LT						Upon Completion		ft				
Ground Surface Elev.	739.90	ft	(ft)	(/6")	(tsf)	(%)	After _____ Hrs.		ft	(ft)	(/6")	(tsf)	(%)
ASPHALT PAVEMENT - 3"	739.7						SANDY CLAY FILL - Black, Stiff, Moist (<i>continued</i>)						
CONCRETE PAVEMENT - 13.5"	738.5						Some Organics				4		
CLAYEY SAND FILL- Dark Brown, Medium-Grained, Medium-Dense, with Gravel and Pebbles				2		8					4		36
				4							3		
				4					716.9				
SAND FILL - Brown, Medium-Grained, Medium-Dense, with Gravel and Pebbles	736.4			8		7	SAND - Gray, Medium-to-Coarse Grained, Medium-Dense, Moist				6		16
				10							13		
				14							13		
									714.4				
				8		8	SANDY GRAVEL - Gray, Medium-Grained, Medium-Dense, Moist				10		12
				11							13		
				15							11		
	731.9						No Recovery				11		
SANDY LOAM FILL - Black, Medium-Dense, with Gravel and Cobbles, Wet Diesel Smell				4		18					11		
				3							11		
				9							15		
				5		15							
				12									
				12									
									706.9				
Becomes Moist, No More Diesel Smell				6		29	COARSE SAND - Gray, Medium-Dense, with Gravel, Moist				9		13
				6							10		
				11							12		
				4									
SANDY CLAY FILL - Black, Stiff, Moist	723.4			6	2.0	23							
				8	P								
				4			Poor Recovery				12		
				4	3.0	29					12		7
				8	P						11		

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)

SOIL BORING LOG

Date 7/20/21

ROUTE	FAP Route 301	DESCRIPTION	PTB 193-20 I-39 and U.S. 20 D2	LOGGED BY	KEG
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SECTION (201-3)K&(4-1,5)R **LOCATION** US-20 over Kishwaukee River

COUNTY Winnebago DRILLING METHOD MUD ROTARY HAMMER TYPE AUTO

STRUCT. NO. 101-0074		DEPTH (ft)	BLOWS (/6")	UCS (tsf)	MOIST (%)	Surface Water Elev. _____ ft		DEPTH (ft)	BLOWS (/6")	UCS (tsf)	MOIST (%)
Station 1345+79.08						Stream Bed Elev. _____ ft					
BORING NO. SB-01		Ground Surface Elev. 739.90 ft				Groundwater Elev.: _____ ft					
Station 1344+57.6						First Encounter _____ ft					
Offset 30.0 ft LT						Upon Completion _____ ft					
Ground Surface Elev. 739.90						After _____ Hrs. _____ ft					
COARSE SAND - Gray, Medium-Dense, with Gravel, Moist (continued)						FINE SAND - Gray, Very-Dense, Moist (continued)					
Poor Recovery With Limestone Fragments			11			Becomes Fine			19		
			15		11				31		20
		-45	9					-65	32		
692.9											
SILT - Gray, Hard, with Sand, Moist											
			14			671.4			21		
			21		19	SILT - Gray, Hard, Moist			33		17
			22			670.4			34		
		-50				FINE SAND - Gray, Very-Dense, Moist		-70			
						667.9					
						CLAYEY SILT - Gray, Hard, Moist					
			21						24		
No More Sand			32		17				30	1.7	17
685.4			28						31	B	
FINE SAND - Gray, Very-Dense, Moist		-55						-75			
						660.9			11		
2" Gray Silt Becomes Very-Fine			18		18	FINE SAND - Gray, Dense, Moist			18		20
			25						23		
		-60	26					-80			

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)

BBS, form 137 (Rev. 8-99)



SOIL BORING LOG

ROUTE FAP Route 301 DESCRIPTION PTB 193-20 I-39 and U.S. 20 D2 LOGGED BY KEG

SECTION (201-3)K&(4-1,5)R LOCATION US-20 over Kishwaukee River

COUNTY Winnebago DRILLING METHOD MUD ROTARY HAMMER TYPE AUTO

STRUCT. NO. 101-0074
Station 1345+79.08

BORING NO. SB-01
Station 1344+57.6
Offset 30.0 ft LT
Ground Surface Elev. 739.90 ft

D E P T H (ft)	B L O W S (/6")	U C S (tsf)	M O I S T (%)
-----------------------------------	------------------------------------	--------------------------	----------------------------------

Surface Water Elev. _____ ft	Stream Bed Elev. _____ ft	Groundwater Elev.: First Encounter _____ ft	Upon Completion _____ ft	After _____ Hrs. _____ ft
------------------------------	---------------------------	--	--------------------------	---------------------------

D E P T H (ft)	B L O W S (/6")	U C S (tsf)	M O I S T (%)
-----------------------------------	------------------------------------	--------------------------	----------------------------------

FINE SAND - Gray, Dense, Moist
(continued)

18			
17			20
20			
-85			
17			
20			20
19			
-90			
14			
18			20
22			
-95			
13			
16			19
17			
-100			

FINE SAND - Gray, Dense, Moist
(continued)

14			
16			17
24			
-105			
18			
30			21
29			
-110			
23			
27			16
26			
-115			
19			
26			15
30			
-120			

Becomes Very-Dense

SAND - Gray, Medium-Grained,
Very-Dense, Moist



SOIL BORING LOG

ROUTE FAP Route 301 DESCRIPTION PTB 193-20 I-39 and U.S. 20 D2 LOGGED BY KEG

SECTION (201-3)K&(4-1,5)R LOCATION US-20 over Kishwaukee River

COUNTY Winnebago DRILLING METHOD MUD ROTARY HAMMER TYPE AUTO

STRUCT. NO. 101-0074
Station 1345+79.08

BORING NO. SB-01
Station 1344+57.6
Offset 30.0 ft LT
Ground Surface Elev. 739.90 ft

D E P T H	B L O W S	U C S Qu	M O I S T
(ft)	(/6")	(tsf)	(%)

Surface Water Elev. _____ ft
Stream Bed Elev. _____ ft
Groundwater Elev.:
First Encounter _____ ft
Upon Completion _____ ft
After _____ Hrs. _____ ft

SAND - Gray, Medium-Grained,
Very-Dense, Moist (*continued*)

Becomes Dense

614.9 -125

End of Boring

-130

-135

-140

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)



SOIL BORING LOG

ROUTE FAP Route 301 DESCRIPTION PTB 193-20 I-39 and U.S. 20 D2 LOGGED BY KEG

SECTION (201-3)K&(4-1,5)R LOCATION US-20 over Kishwaukee River

COUNTY Winnebago DRILLING METHOD MUD ROTARY HAMMER TYPE AUTO

STRUCT. NO. 101-0073
Station 1345+79.08

BORING NO. SB-02
Station 1344+20.6
Offset 30.0 ft RT
Ground Surface Elev. 739.99 ft

D E P T H (ft)	B L O W S (/6")	U C S Qu (tsf)	M O I S T (%)	Surface Water Elev. _____ ft	D E P T H (ft)	B L O W S (/6")	U C S Qu (tsf)	M O I S T (%)
				Stream Bed Elev. _____ ft				
				Groundwater Elev.: _____ ft				
				First Encounter _____ ft				
				Upon Completion _____ ft				
				After _____ Hrs. _____ ft				
ASPHALT PAVEMENT - 4.5" _____ 739.6				SANDY CLAY LOAM FILL - Black, Stiff, with Some Organics, Moist (continued)				
CONCRETE PAVEMENT - 12" _____ 738.6	4							
SANDY LOAM FILL- Dark Brown, Dense, Medium-Grained, with Cobbles and Rubble, Moist _____ 737.0	4 6		14					
SAND FILL - Brown, Dense, Fine-to-Coarse Grained, Moist _____	7					5		
	3		6			6		26
	14					7		
Becomes Brown-Gray _____	11							
	14		4			10		
	16					14		14
						10		
Becomes Black _____	14					8		
	13		6			10		12
	12					6		
CLAYEY SAND FILL - Black, Medium-Dense, Medium-Grained, with Trace Gravel, Moist _____ 729.0	4							
	5		23					
	7							
CLAYEY SILT FILL - Black, Stiff, Some Organics, Moist _____ 726.5	3					16		
	10		27			20		10
SAND FILL - Brown-Gray, Medium-Dense, Moist _____ 725.5	8			Becomes Dense		20		
SANDY CLAY LOAM FILL - Black, Stiff, with Some Organics, Moist _____ 724.0	3							
	5	1.0	29	Becomes Medium-Dense				
	12	P						
	3					11		
	6		32			10		11
	9					6		

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)

Page 2 of 2Date 7/13/21[illegible]

BBS, form 137 (Rev. 8-99)

Page 1 of 3

Date 7/22/21

BBS, form 137 (Rev. 8-99)

Page 2 of 3

Date 7/22/21

BBS, form 137 (Rev. 8-99)



SOIL BORING LOG

ROUTE FAP Route 301 DESCRIPTION PTB 193-20 I-39 and U.S. 20 D2 LOGGED BY KEG

SECTION (201-3)K&(4-1,5)R LOCATION US-20 over Kishwaukee River

COUNTY Winnebago DRILLING METHOD MUD ROTARY HAMMER TYPE AUTO

STRUCT. NO. 101-0074
Station 1345+79.08

BORING NO. SB-03
Station 1345+35.8
Offset 30.0 ft LT
Ground Surface Elev. 739.81 ft

D E P T H (ft)	B L O W S (/6")	U C S Qu (tsf)	M O I S T (%)
-------------------------------	--------------------------------	----------------------------	------------------------------

Surface Water Elev.	ft
Stream Bed Elev.	ft
Groundwater Elev.:	
First Encounter	ft
Upon Completion	ft
After _____ Hrs.	ft

D E P T H (ft)	B L O W S (/6")	U C S Qu (tsf)	M O I S T (%)
-------------------------------	--------------------------------	----------------------------	------------------------------

CLAYEY SILT - Gray, Hard, with Sand, Moist (*continued*)

No More Sand

End of Boring

650.8
FINE SAND - Gray, Dense, Moist

639.8 -100

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)



SOIL BORING LOG

ROUTE FAP Route 301 DESCRIPTION PTB 193-20 I-39 and U.S. 20 D2 LOGGED BY KEG

SECTION (201-3)K&(4-1,5)R LOCATION US-20 over Kishwaukee River

COUNTY Winnebago DRILLING METHOD MUD ROTARY HAMMER TYPE AUTO

STRUCT. NO. 101-0073
Station 1345+79.08

BORING NO. SB-04
Station 1344+98.4
Offset 30.0 ft RT
Ground Surface Elev. 739.96 ft

**D
E
P
T
H**
**B
L
O
W
S**
**U
C
S**
**M
O
I
S
T**
Qu
(ft)
(/6")
(tsf)
(%)

Surface Water Elev. _____ ft
Stream Bed Elev. _____ ft
Groundwater Elev.:
First Encounter _____ ft
Upon Completion _____ ft
After _____ Hrs. _____ ft

**D
E
P
T
H**
**B
L
O
W
S**
**U
C
S**
**M
O
I
S
T**
Qu
(ft)
(/6")
(tsf)
(%)

Note: Drilling Through Bridge Deck
CONCRETE PAVEMENT - 8.25" 739.3

Blind Drilling
Total Casing used = 40 ft

Blind Drilling
Total Casing used = 40 ft 719.0
(continued)

CLAY - Dark Brown, Medium-Stiff,
with Sand and Rubble

GRAVELLY SAND - Gray-Brown,
Coarse-Grained, with Rubble and
Pebbles, Moist

SAND - Gray, Medium-Dense,
Coarse-Grained, with Some
Gravels, Moist

GRAVELLY SAND - Gray,
Medium-Dense, Coarse-Grained,
Moist

SOIL BORING LOG

Date 7/15/21

ROUTE	FAP Route 301	DESCRIPTION	PTB 193-20 I-39 and U.S. 20 D2	LOGGED BY	KEG
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SECTION (201-3)K&(4-1,5)R **LOCATION** US-20 over Kishwaukee River

COUNTY Winnebago DRILLING METHOD MUD ROTARY HAMMER TYPE AUTO

STRUCT. NO. 101-0073
Station 1345+79.08

BORING NO.	SB-04
Station	1344+98.4
Offset	30.0 ft RT
Ground Surface Elev.	739.96

D E P T H	B L O W S	U C S Qu	M O I S T
(ft)	(/6")	(tsf)	(%)

Surface Water Elev.	_____	ft
Stream Bed Elev.	_____	ft
Groundwater Elev.:		
First Encounter	_____	ft
Upon Completion	_____	ft
After _____ Hrs.	_____	ft

D E P T H	B L O W S	U C S Qu	M O I S T
(ft)	(/6")	(tsf)	(%)

GRAVELLY SAND - Gray,
Medium-Dense, Coarse-Grained,
Moist (*continued*)
Becomes Wet

SAND - Gray, Dense, Very-Fine Grained, Moist (continued)

	9		
	7		18
	6		
	11		
	15		20
-45	9		
	13		
	28		12
	28		
	26		
	34		
-50	32		

-65	17 18 19	18
	15	
	22 22	22
-70		

SAND - Gray, Dense, Very-Fine Grained, Moist

SILTY SAND - Gray, Dense,
Very-Fine Grained, Moist

18		
24		17
26		
-55		

20		
25		14
22		
-75		

SILT - Gray, Very-Stiff, Moist

12		
17		25
18		

	12		
	13	0.9	17
80	16	B	

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)

BBS, form 137 (Rev. 8-99)



SOIL BORING LOG

ROUTE FAP Route 301 DESCRIPTION PTB 193-20 I-39 and U.S. 20 D2 LOGGED BY KEG

SECTION (201-3)K&(4-1,5)R LOCATION US-20 over Kishwaukee River

COUNTY Winnebago DRILLING METHOD MUD ROTARY HAMMER TYPE AUTO

STRUCT. NO. 101-0073
Station 1345+79.08

BORING NO. SB-04
Station 1344+98.4
Offset 30.0 ft RT
Ground Surface Elev. 739.96 ft

D E P T H	B L O W S	U C S Qu	M O I S T
(ft)	(/6")	(tsf)	(%)

Surface Water Elev. _____ ft
Stream Bed Elev. _____ ft
Groundwater Elev.:
First Encounter _____ ft
Upon Completion _____ ft
After _____ Hrs. _____ ft

SILT - Gray, Very-Stiff, Moist
(continued)

658.0

SAND - Gray, Very-Dense,
Very-Fine Grained

20

28

27

17

-85

24

39

39

22

-90

Becomes Medium-Grained

16

20

23

23

-95

14

21

24

20

640.0

-100

End of Boring

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)

The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)



SOIL BORING LOG

ROUTE FAP Route 301 DESCRIPTION PTB 193-20 I-39 and U.S. 20 D2 LOGGED BY KEG

SECTION (201-3)K&(4-1,5)R LOCATION US-20 over Kishwaukee River

COUNTY Winnebago DRILLING METHOD MUD ROTARY HAMMER TYPE AUTO

STRUCT. NO. 101-0074
Station 1345+79.08

BORING NO. SB-05
Station 1346+63.6
Offset 30.0 ft LT
Ground Surface Elev. 739.66 ft

D
E
P
T
H

B
L
O
W
S

U
C
S

M
O
I
S
T

Qu

Qu

(ft)
(/6")
(tsf)
(%)

Surface Water Elev. _____ ft
Stream Bed Elev. _____ ft

Groundwater Elev.:
First Encounter _____ ft
Upon Completion _____ ft
After _____ Hrs. _____ ft

D
E
P
T
H

B
L
O
W
S

U
C
S

M
O
I
S
T

Qu

Qu

(ft)
(/6")
(tsf)
(%)

Note: Drilling Through Bridge Deck
CONCRETE PAVEMENT - 8" 739.0

Blind Drilling
Total Casing used = 35 ft

Blind Drilling
Total Casing used = 35 ft
(continued)

SAND - Brown, Fine-to-Coarse
Grained, Loose, with Rubbles and
Gravel, Moist

Poor Recovery

Poor Recovery
No More Rubbles

COARSE SAND - Brown,
Medium-Dense, with Gravel

Becomes Brown-Gray



SOIL BORING LOG

ROUTE FAP Route 301 DESCRIPTION PTB 193-20 I-39 and U.S. 20 D2 LOGGED BY KEG

SECTION (201-3)K&(4-1,5)R LOCATION US-20 over Kishwaukee River

COUNTY Winnebago DRILLING METHOD MUD ROTARY HAMMER TYPE AUTO

STRUCT. NO. 101-0074
Station 1345+79.08

BORING NO. SB-05
Station 1346+63.6
Offset 30.0 ft LT
Ground Surface Elev. 739.66 ft

D E P T H (ft)	B L O W S (/6")	U C S Qu (tsf)	M O I S T (%)	Surface Water Elev. _____ ft	D E P T H (ft)	B L O W S (/6")	U C S Qu (tsf)	M O I S T (%)
				Stream Bed Elev. _____ ft				
				Groundwater Elev.: _____ ft				
				First Encounter _____ ft				
				Upon Completion _____ ft				
				After _____ Hrs. _____ ft				
COARSE SAND - Brown, Medium-Dense, with Gravel (continued) No Recovery	13			CLAYEY SILT - Gray, Hard, Moist (continued)				
	16							
	11							
With Limestone Fragments	12					14		
	14		7			24	0.5	19
	15					22	P	
	-45							
GRAVELLY SAND - Gray-Brown, Medium-Dense, Coarse-Grained, Moist	15							
	12		12					
	13							
Poor Recovery Becomes Gray	6					17		
	20		14			21		20
	9					24		
	-50							
FINE SAND - Gray, Medium-Dense, Moist Becomes Very-Fine Grained	10							
	10		18					
	10							
	7					20		
	13		22			24		21
	9					30		
	-55							
	10							
	12	1.0	23					
	14	P						
SILT - Gray, Stiff, Moist								
CLAYEY SILT - Gray, Hard, Moist	10					11		
	16	3.0	18			15		18
	22	P				13		
	-60							

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)



BBS, form 137 (Rev. 8-99)

Page 1 of 3

Date 7/14/21

COUNTY Winnebago DRILLING METHOD MUD ROTARY HAMMER TYPE AUTO

[illegible]

BBS, form 137 (Rev. 8-99)

Page 2 of 3Date 7/14/21

	20		
	29		21
80	36		

BBS, form 137 (Rev. 8-99)



SOIL BORING LOG

ROUTE FAP Route 301 DESCRIPTION PTB 193-20 I-39 and U.S. 20 D2 LOGGED BY KEG

SECTION (201-3)K&(4-1,5)R LOCATION US-20 over Kishwaukee River

COUNTY Winnebago DRILLING METHOD MUD ROTARY HAMMER TYPE AUTO

STRUCT. NO. 101-0073
Station 1345+79.08

BORING NO. SB-06
Station 1346+24.6
Offset 30.0 ft RT
Ground Surface Elev. 739.91 ft

D E P T H	B L O W S	U C S Qu	M O I S T
(ft)	(/6")	(tsf)	(%)

Surface Water Elev. _____ ft
Stream Bed Elev. _____ ft
Groundwater Elev.:
First Encounter _____ ft
Upon Completion _____ ft
After _____ Hrs. _____ ft

SAND - Gray- Brown, Dense,
Very-Fine Grained, Moist
(continued)
Becomes Medium-Grained

655.4

SILT - Gray, Hard, Moist

647.9

SAND - Gray, Very-Dense,
Medium-Grained, with Sandstone
Fragments, Moist

3" Seam of Silt

639.9

End of Boring

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)



SOIL BORING LOG

ROUTE FAP Route 301 DESCRIPTION PTB 193-20 I-39 and U.S. 20 D2 LOGGED BY KEG

SECTION (201-3)K&(4-1,5)R LOCATION US-20 over Kishwaukee River

COUNTY Winnebago DRILLING METHOD MUD ROTARY HAMMER TYPE AUTO

STRUCT. NO.	101-0074	D	B	U	M	Surface Water Elev.	ft	D	B	U	M
Station	1345+79.08	E	L	C	O	Stream Bed Elev.	ft	E	L	C	O
BORING NO.	SB-07	P	W	S	I	Groundwater Elev.:		P	W	S	I
Station	1347+41.2	T	S	Qu	S	First Encounter	ft	H	S	Qu	T
Offset	27.5 ft LT	H				Upon Completion	ft				
Ground Surface Elev.	739.56	(ft)	(/6")	(tsf)	(%)	After	ft	(ft)	(/6")	(tsf)	(%)
ASPHALT PAVEMENT - 2"	739.4					SAND - Dark Brown, Medium-Grained, Medium-Dense, with Trace Gravel and Organics, Wet (continued)	718.6				
CONCRETE PAVEMENT - 12"	738.4						718.1	3			
SANDY CLAY FILL - Dark Brown, Medium-Stiff, with Trace Gravel		7				CLAY - Dark Brown, Soft, Wet		4		21	
		5	2.0	17				5			
		7	P			SAND - Dark Brown, Medium-Grained, Loose, Wet	716.6				
	735.6	5				COARSE SAND - Gray, Dense, with Trace Gravel, Moist		18			
SAND FILL - Gray, Medium-Grained, Medium-Dense, with Trace Gravel		12		5				20		12	
	-5	16						18			
						GRAVELLY SAND - Brown, Dense, Moist, Coarse-Grained, Moist	714.1				
Becomes Dark Brown		11						11			
		16		6				12		10	
		18						11			
						COARSE SAND - Brown, Medium-Dense, with Gravel, Moist	711.6				
		5						10			
		11		6				12		13	
	-10	12						14			
becomes Moist											
		12									
		15		10							
		10									
Becomes Brown, Dense and Wet						No Recovery		11			
	725.1	5									
CLAYEY SAND - Dark Brown, Medium-Dense, with Gravel, Wet		19		15				10			
	-15	13						9			
		10									
		17	2.5	23							
		9	P								
With Some Organics	720.6					Poor Recovery		10			
		7				2" of Limestone Fragments		35			
		10		29				32			
	-20	7					699.6	40			

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)



SOIL BORING LOG

ROUTE FAP Route 301 DESCRIPTION PTB 193-20 I-39 and U.S. 20 D2 LOGGED BY KEG

SECTION (201-3)K&(4-1,5)R LOCATION US-20 over Kishwaukee River

COUNTY Winnebago DRILLING METHOD MUD ROTARY HAMMER TYPE AUTO

STRUCT. NO. 101-0078
Station 1345+79.08

BORING NO. SB-08
Station 1347+02.9
Offset 30.0 ft RT
Ground Surface Elev. 739.87 ft

D E P T H (ft)	B L O W S (/6")	U C S Qu (tsf)	M O I S T (%)	Surface Water Elev. _____ ft	D E P T H (ft)	B L O W S (/6")	U C S Qu (tsf)	M O I S T (%)
				Stream Bed Elev. _____ ft				
				Groundwater Elev.: _____ ft				
				First Encounter _____ ft				
				Upon Completion _____ ft				
				After _____ Hrs. _____ ft				
ASPHALT PAVEMENT - 4"				CLAY - Black, Medium-Stiff, with Trace Gravel and some Organic, Moist (<i>continued</i>)				
CONCRETE PAVEMENT - 12"						3		
	7					4	1.0	27
SAND FILL - Brown, Medium-Grained, with Trace Gravel	6		9			12	P	
	4			SAND - Brown, Loose, Fine-Grained, with Gravel, Moist				
						7		
SANDY CLAY FILL - Black, Medium-Stiff, with Cobbles and Pebbles	6	2.0	18			12		17
	10	P				12		
				SANDY GRAVEL - Brown, Loose, Moist				
						10		
GRAVELLY SAND FILL - Black-Gray, Medium-Dense, Medium-Grained	11		7			5		10
	15					1		
				GRAVELLY SAND - Brown, Loose, Coarse-Grained, Moist				
	6					10		
	13		10			12		15
	11					11		
GRAVELLY SAND - Brown-Gray, Medium-Dense, Medium-Grained, Wet								
	11							
	18		15					
	15							
Becomes Gray						11		
	6					13		14
	8		20			15		
	8							
Becomes Dense								
	13							
	12		15					
	7							
CLAY - Black, Medium-Stiff, with Trace Gravel and some Organic, Moist				Becomes Gray		15		
	4					12		8
	7					13		
	11							

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)



SOIL BORING LOG

ROUTE FAP Route 301 DESCRIPTION PTB 193-20 I-39 and U.S. 20 D2 LOGGED BY KEG

SECTION (201-3)K&(4-1,5)R LOCATION US-20 over Kishwaukee River

COUNTY Winnebago DRILLING METHOD MUD ROTARY HAMMER TYPE AUTO

STRUCT. NO. 101-0078
Station 1345+79.08

BORING NO. SB-08
Station 1347+02.9
Offset 30.0 ft RT
Ground Surface Elev. 739.87 ft

D E P T H (ft)	B L O W S (/6")	U C S (tsf)	M O I S T (%)
-----------------------------------	------------------------------------	--------------------------	----------------------------------

Surface Water Elev. _____ ft	Stream Bed Elev. _____ ft	Groundwater Elev.: First Encounter _____ ft	Upon Completion _____ ft	After _____ Hrs. _____ ft
------------------------------	---------------------------	--	--------------------------	---------------------------

D E P T H (ft)	B L O W S (/6")	U C S (tsf)	M O I S T (%)
-----------------------------------	------------------------------------	--------------------------	----------------------------------

GRAVELLY SAND - Brown, Loose,
Coarse-Grained, Moist (*continued*)

697.9

SANDY GRAVEL - Gray, Loose,
Coarse-Grained, Some Pebbles,
Moist

17

16

25

-45

18

30

50

-50

685.9

SAND - Gray, Dense, Very-Fine
Grained, with Trace Gravel, Moist

16

21

22

-55

681.9

SILTY SAND - Gray, Dense, with
Trace Gravel, Moist

15

15

25

-60

SILTY SAND - Gray, Dense, with
Trace Gravel, Moist (*continued*)

677.9

SAND - Gray, Dense, Very-Fine
Grained, Moist

18

21

28

-65

23

34

35

-70

Becomes Gray-Brown and
Very-Dense

21

30

37

-75

20

31

40

-80

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)

Page 3 of 4

Date 7/12/21

	22	
	24	14
-120	33	

BBS, form 137 (Rev. 8-99)



SOIL BORING LOG

ROUTE FAP Route 301 DESCRIPTION PTB 193-20 I-39 and U.S. 20 D2 LOGGED BY KEG

SECTION (201-3)K&(4-1,5)R LOCATION US-20 over Kishwaukee River

COUNTY Winnebago DRILLING METHOD MUD ROTARY HAMMER TYPE AUTO

STRUCT. NO. 101-0078
Station 1345+79.08

BORING NO. SB-08
Station 1347+02.9
Offset 30.0 ft RT
Ground Surface Elev. 739.87 ft

D E P T H	B L O W S	U C S Qu	M O I S T
(ft)	(/6")	(tsf)	(%)

Surface Water Elev. _____ ft
Stream Bed Elev. _____ ft
Groundwater Elev.:
First Encounter _____ ft
Upon Completion _____ ft
After _____ Hrs. _____ ft

SAND - Gray, Very-Dense,
Medium-Grained, Moist (*continued*)

617.9

COARSE SAND - Gray, Dense,
with Gravel and Sandstone
Fragments, Moist

22

26

12

614.9 -125

End of Boring

-130

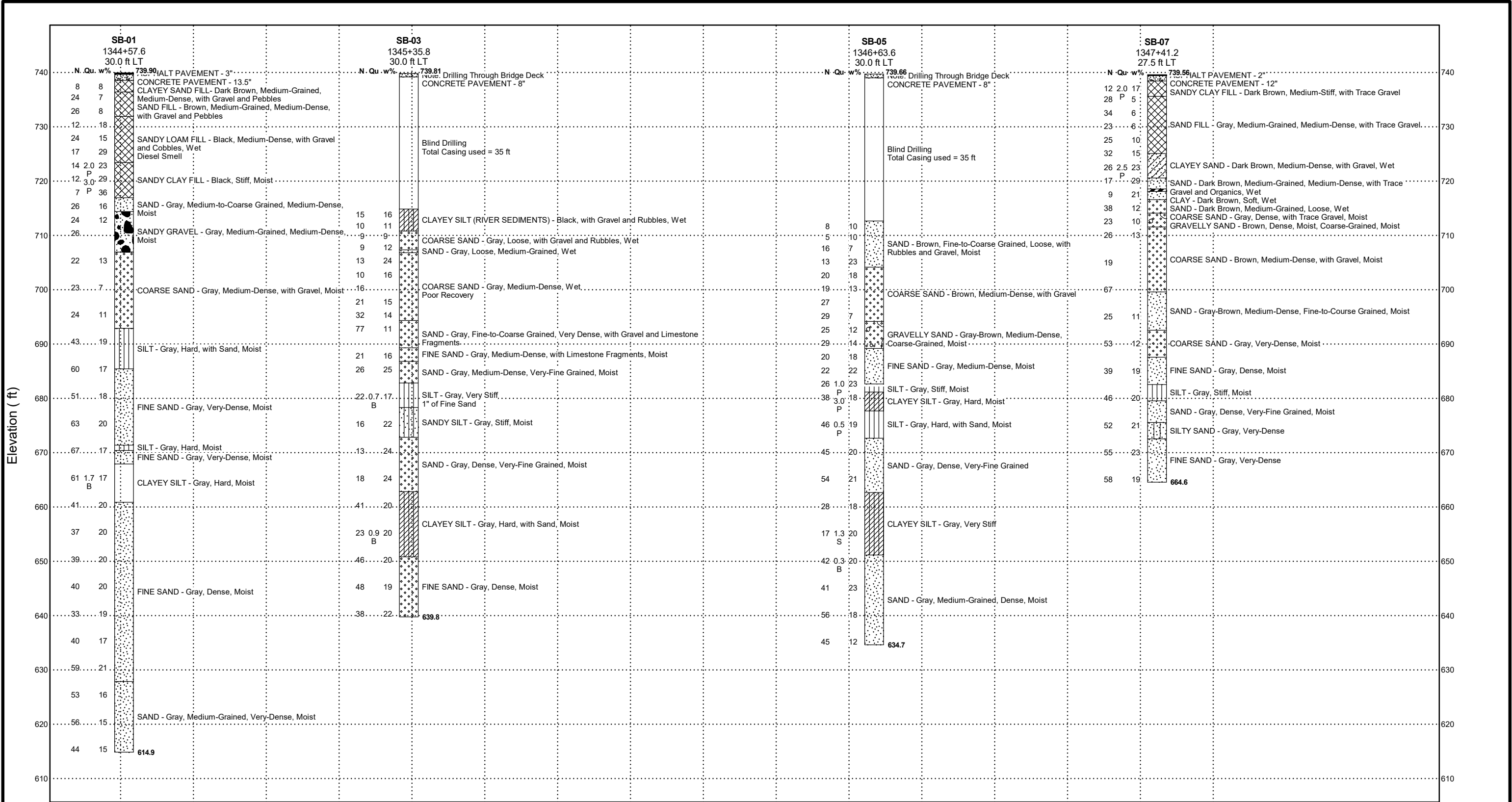
-135

-140

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)

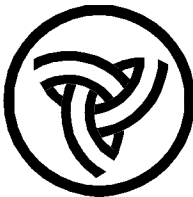
EXHIBIT E
SUBSURFACE PROFILE

PRINTERMOD2 11x17 19-1138.00 US 20 OVER KISHWAUKEE RIVER.GPJ IL_DOT.GDT 6/29/23



NOT TO HORIZONTAL SCALE

SUBSURFACE PROFILE



**Illinois Department
of Transportation**
Division of Highways

Route: FAP Route 301
Section: (201-3)K&(4-1,5)R
County: Winnebago

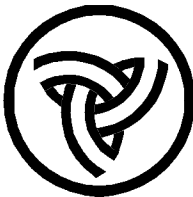
PRINTERMOD2 11X17 19-1138.00 US 20 OVER KISHWAUKEE RIVER.GPJ IL_DOT.GDT 6/29/23



NOT TO HORIZONTAL SCALE

SUBSURFACE PROFILE

Route: FAP Route 301
Section: (201-3)K&(4-1,5)R
County: Winnebago

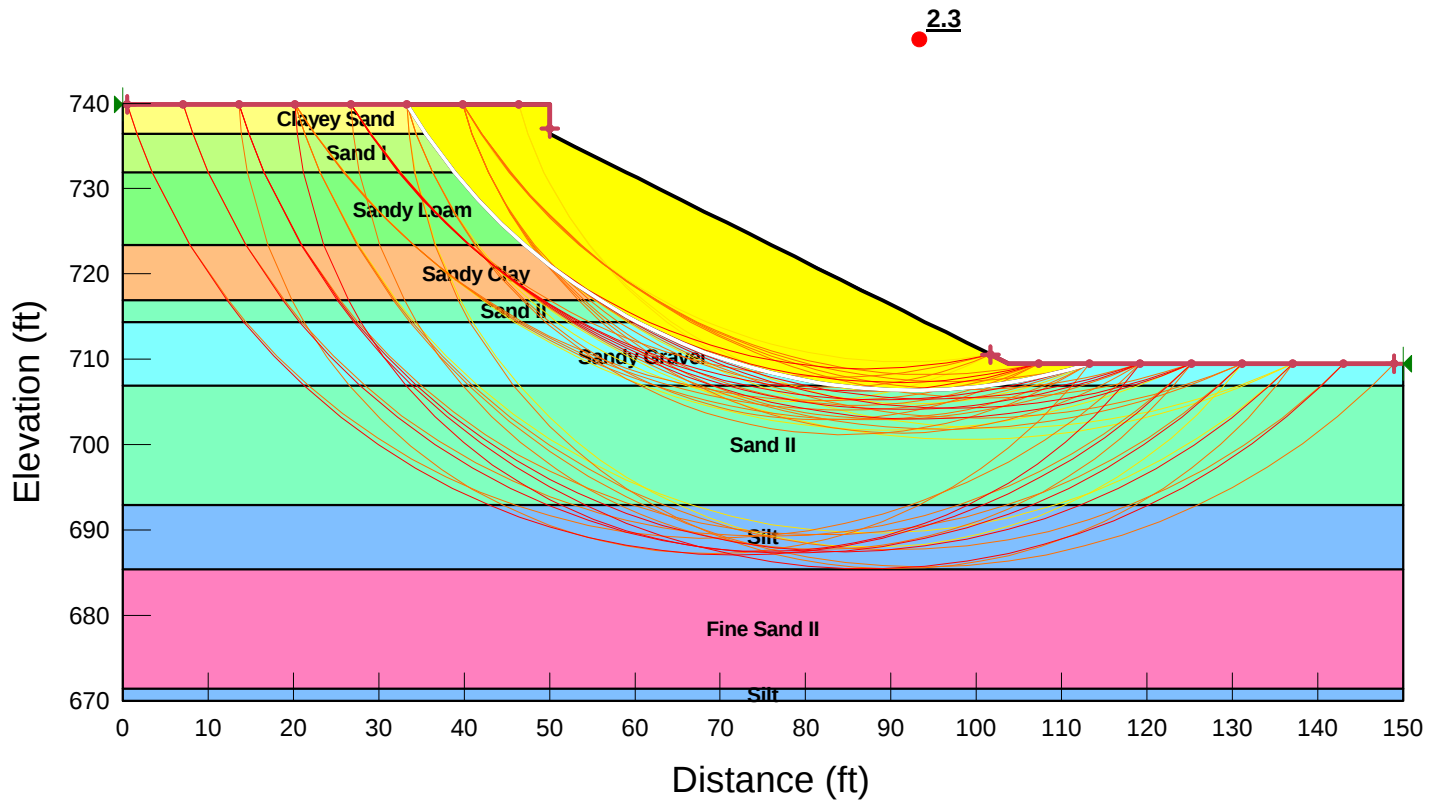


Illinois Department
of Transportation
Division of Highways

EXHIBIT F

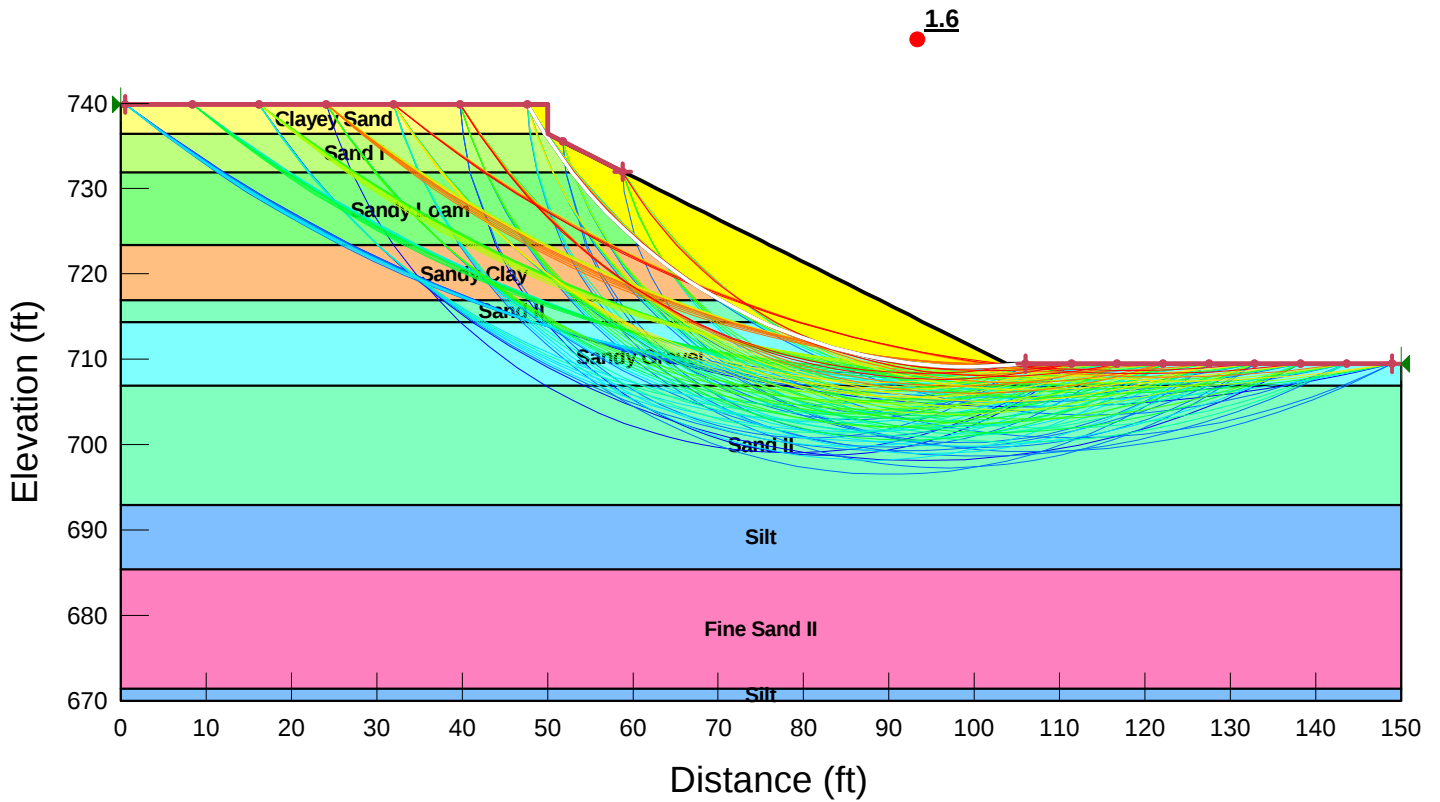
SLOPE W SLOPE STABILITY ANALYSIS

US 20 over Kishwaukee River
West Abutment (Westbound)
Boring SB-01
End of Construction (Undrained Analysis)



Color	Name	Slope Stability Material Model	Unit Weight (pcf)	Effective Cohesion (psf)	Effective Friction Angle (°)
	Clayey Sand	Mohr-Coulomb	120	0	29
	Fine Sand II	Mohr-Coulomb	115	0	47
	Sand I	Mohr-Coulomb	115	0	33
	Sand II	Mohr-Coulomb	115	0	35
	Sandy Clay	Mohr-Coulomb	120	2,500	0
	Sandy Gravel	Mohr-Coulomb	120	0	35
	Sandy Loam	Mohr-Coulomb	120	0	32
	Silt	Mohr-Coulomb	110	1,000	0

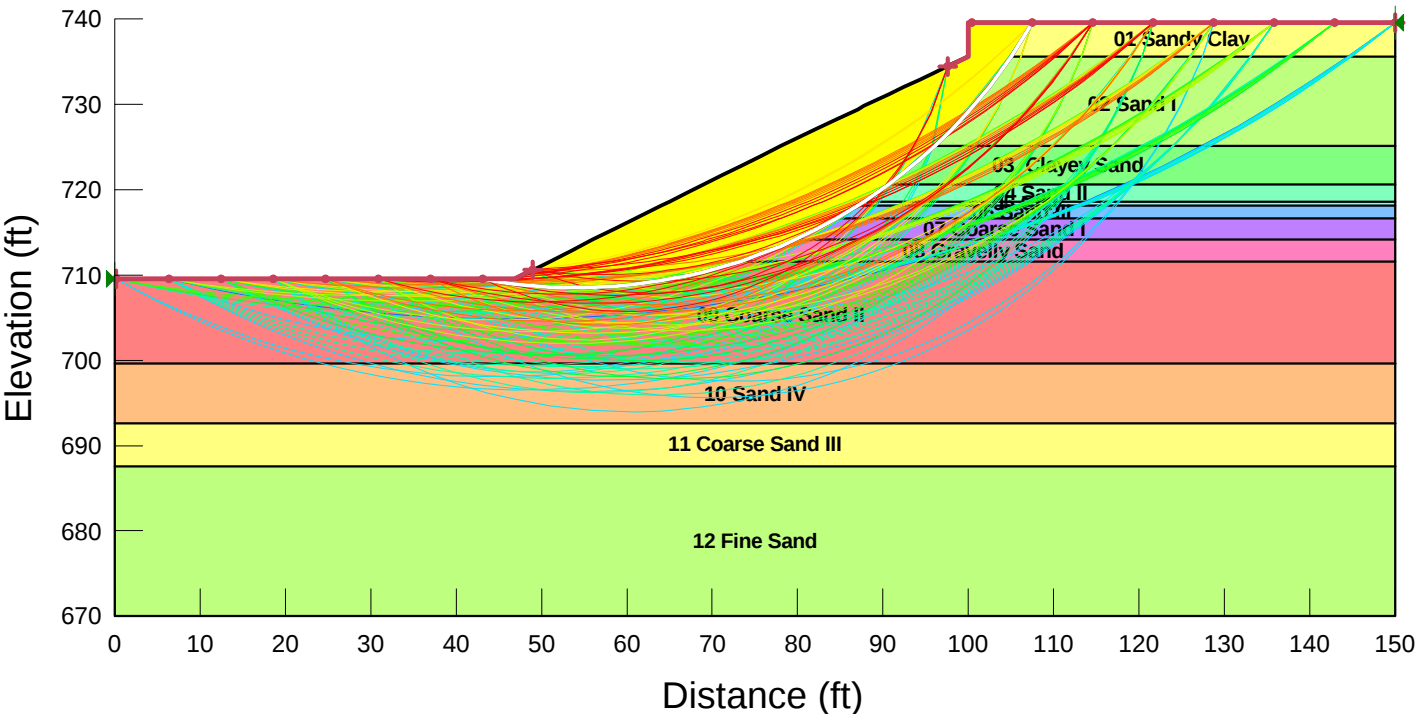
**US 20 over Kishwaukee River
West Abutment (Westbound)
Boring SB-01
Long Term (Drained Analysis)**



Color	Name	Slope Stability Material Model	Unit Weight (pcf)	Effective Cohesion (psf)	Effective Friction Angle (°)
	Clayey Sand	Mohr-Coulomb	120	0	29
	Fine Sand II	Mohr-Coulomb	115	0	47
	Sand I	Mohr-Coulomb	115	0	33
	Sand II	Mohr-Coulomb	115	0	35
	Sandy Clay	Mohr-Coulomb	120	100	30
	Sandy Gravel	Mohr-Coulomb	120	0	35
	Sandy Loam	Mohr-Coulomb	120	0	32
	Silt	Mohr-Coulomb	110	150	26

US 20 over Kishwaukee River
East Abutment (Eastbound)
Boring SB-07
End of Construction (Undrained Analysis)

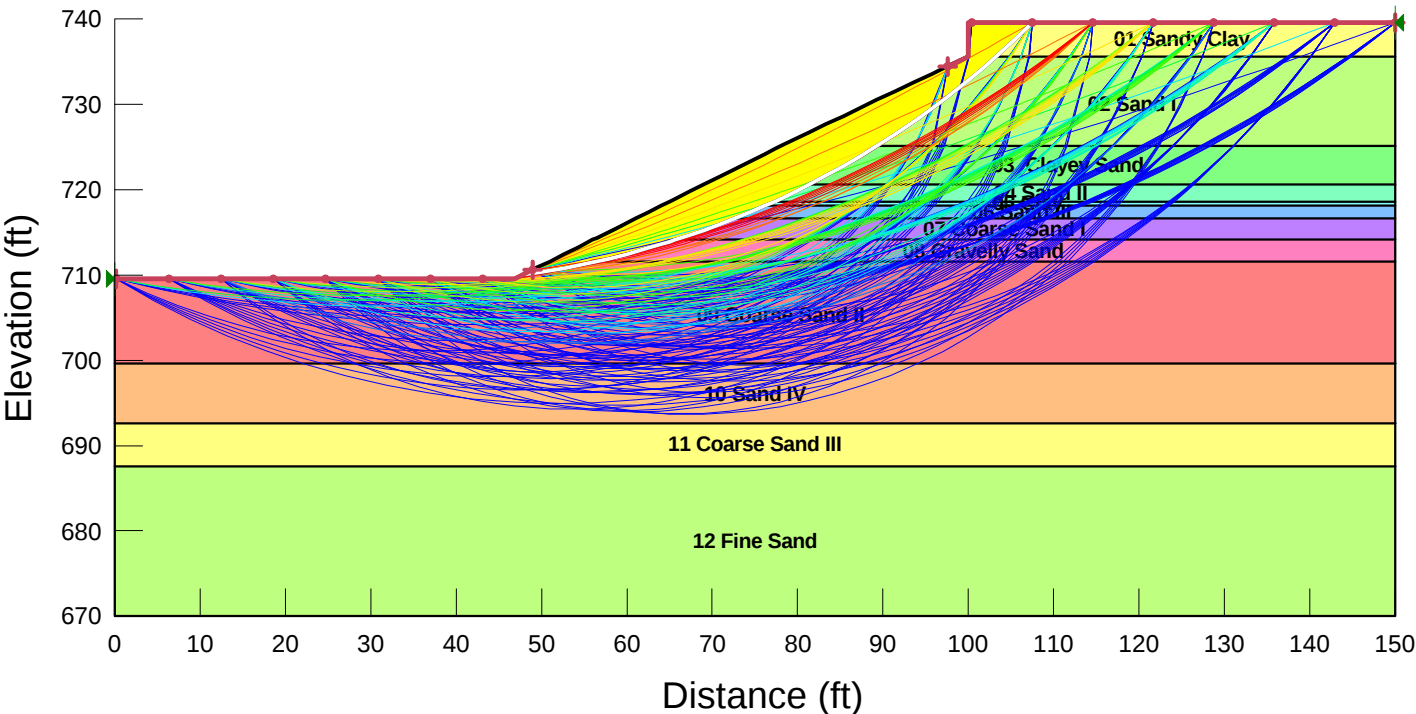
2.2



Color	Name	Slope Stability Material Model	Unit Weight (pcf)	Effective Cohesion (psf)	Effective Friction Angle (°)
	01 Sandy Clay	Mohr-Coulomb	120	2,000	0
	02 Sand I	Mohr-Coulomb	115	0	35
	03 Clayey Sand	Mohr-Coulomb	120	0	36
	04 Sand II	Mohr-Coulomb	115	0	32
	05 Clay	Mohr-Coulomb	120	1,000	0
	06 Sand III	Mohr-Coulomb	115	0	30
	07 Coarse Sand I	Mohr-Coulomb	115	0	39
	08 Gravelly Sand	Mohr-Coulomb	120	0	35
	09 Coarse Sand II	Mohr-Coulomb	115	0	39
	10 Sand IV	Mohr-Coulomb	115	0	35
	11 Coarse Sand III	Mohr-Coulomb	115	0	43
	12 Fine Sand	Mohr-Coulomb	115	0	40

US 20 over Kishwaukee River
East Abutment (Eastbound)
Boring SB-07
Long Term (Drained Analysis)

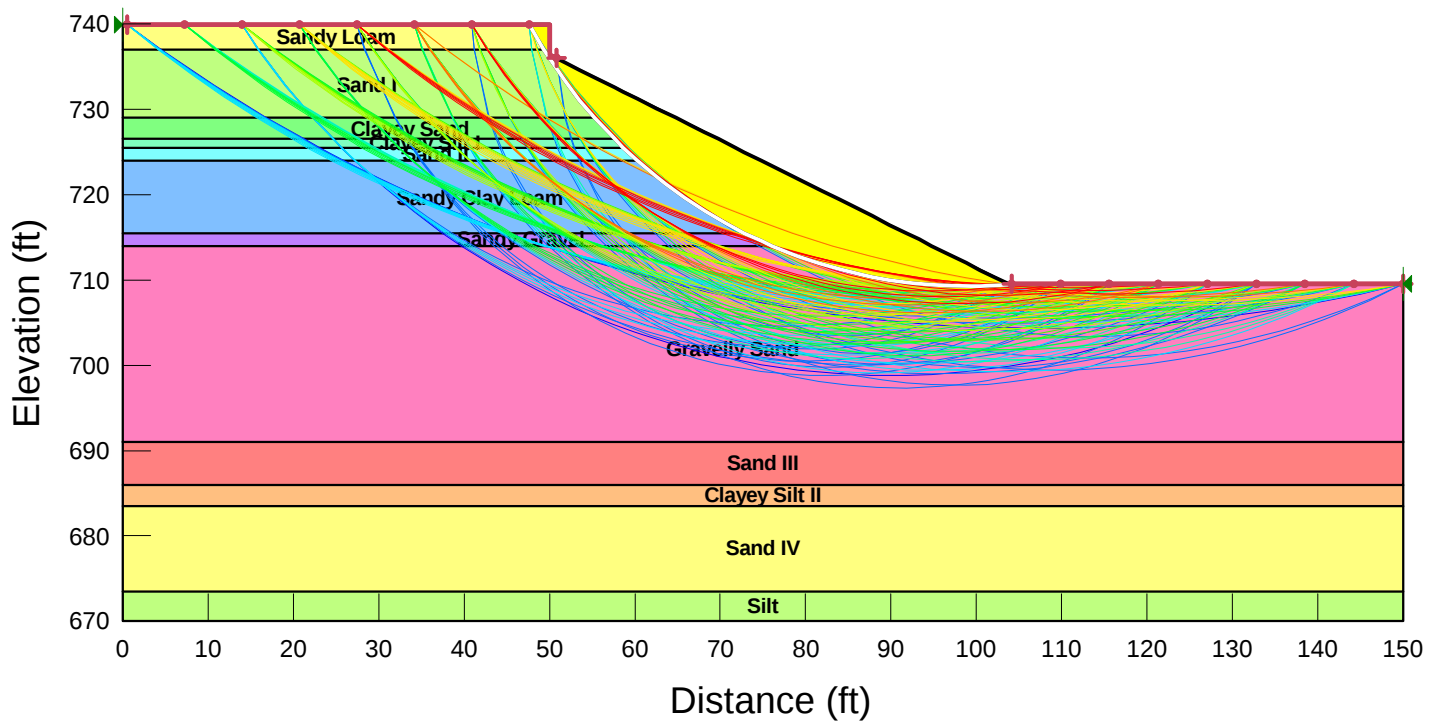
1.5



Color	Name	Slope Stability Material Model	Unit Weight (pcf)	Effective Cohesion (psf)	Effective Friction Angle (°)
	01 Sandy Clay	Mohr-Coulomb	120	100	30
	02 Sand I	Mohr-Coulomb	115	0	35
	03 Clayey Sand	Mohr-Coulomb	120	0	36
	04 Sand II	Mohr-Coulomb	115	0	32
	05 Clay	Mohr-Coulomb	120	100	26
	06 Sand III	Mohr-Coulomb	115	0	30
	07 Coarse Sand I	Mohr-Coulomb	115	0	39
	08 Gravelly Sand	Mohr-Coulomb	120	0	35
	09 Coarse Sand II	Mohr-Coulomb	115	0	39
	10 Sand IV	Mohr-Coulomb	115	0	35
	11 Coarse Sand III	Mohr-Coulomb	115	0	43
	12 Fine Sand	Mohr-Coulomb	115	0	40

US 20 over Kishwaukee River
West Abutment (Eastbound)
Boring SB-02
End of Construction (Undrained Analysis)

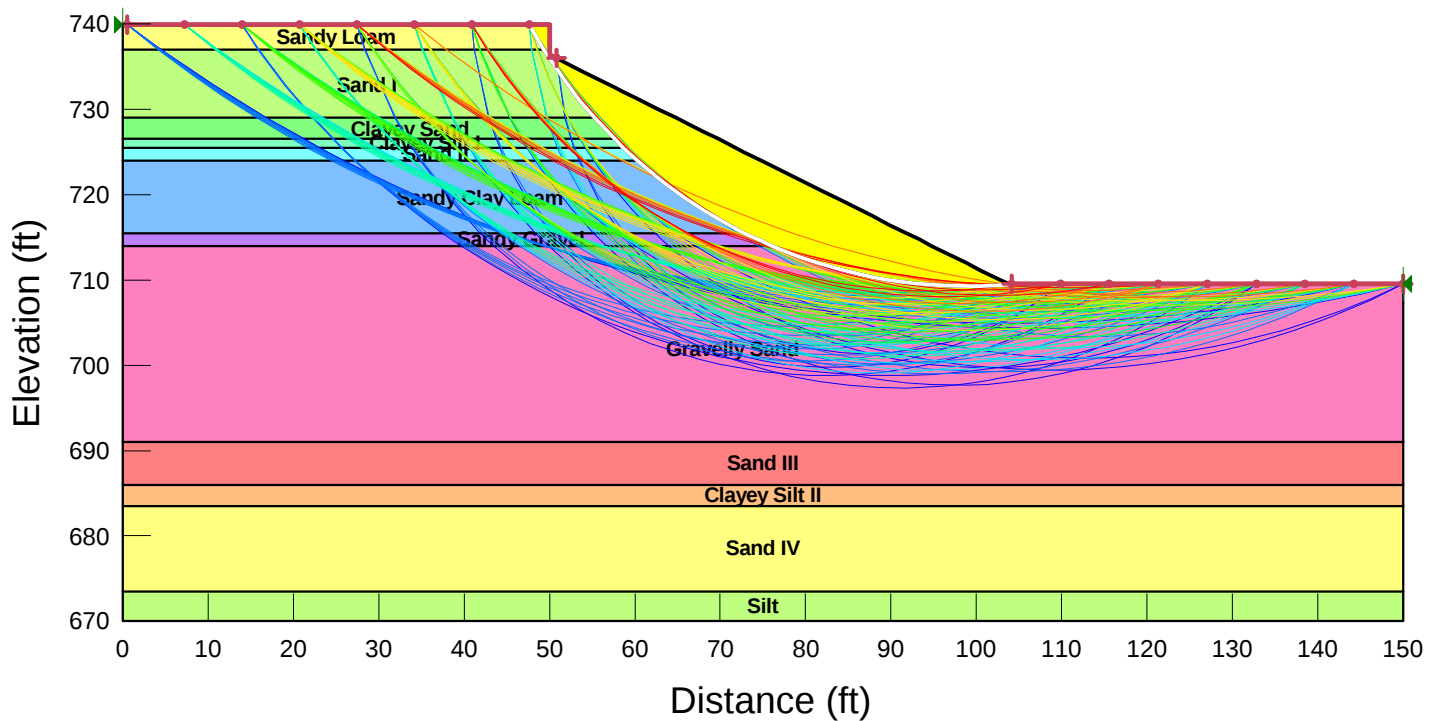
1.6



Color	Name	Slope Stability Material Model	Unit Weight (pcf)	Effective Cohesion (psf)	Effective Friction Angle (°)
	Clayey Sand	Mohr-Coulomb	120	0	30
	Clayey Silt I	Mohr-Coulomb	110	1,000	0
	Clayey Silt II	Mohr-Coulomb	110	1,500	0
	Gravelly Sand	Mohr-Coulomb	120	0	35
	Sand I	Mohr-Coulomb	115	0	34
	Sand II	Mohr-Coulomb	115	0	33
	Sand III	Mohr-Coulomb	115	0	39
	Sand IV	Mohr-Coulomb	115	0	41
	Sandy Clay Loam	Mohr-Coulomb	120	0	32
	Sandy Gravel	Mohr-Coulomb	120	0	31
	Sandy Loam	Mohr-Coulomb	120	0	29
	Silt	Mohr-Coulomb	110	1,000	0

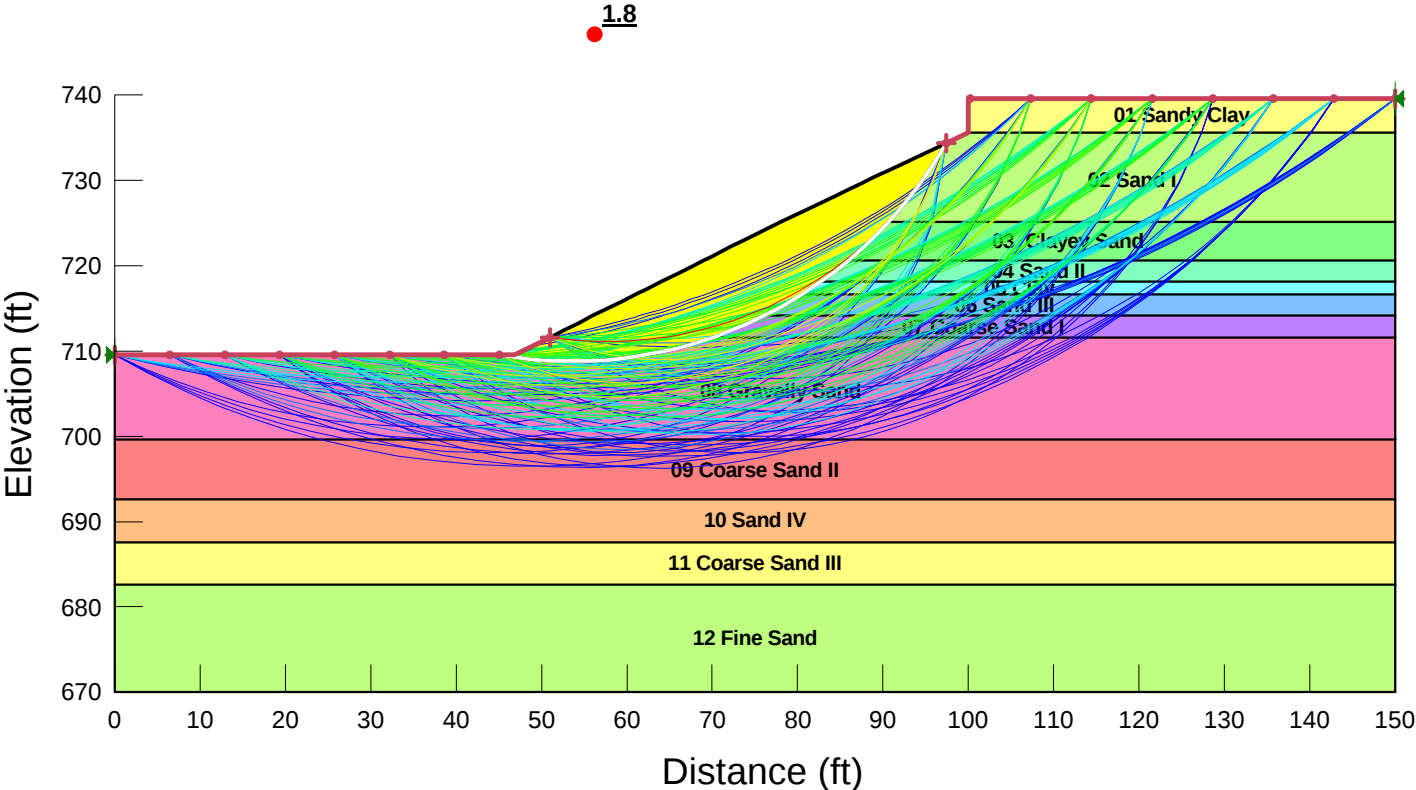
US 20 over Kishwaukee River
West Abutment (Eastbound)
Boring SB-02
Long Term (Drained Analysis)

1.5



Color	Name	Slope Stability Material Model	Unit Weight (pcf)	Effective Cohesion (psf)	Effective Friction Angle (°)
	Clayey Sand	Mohr-Coulomb	120	0	30
	Clayey Silt I	Mohr-Coulomb	110	100	26
	Clayey Silt II	Mohr-Coulomb	110	150	26
	Gravelly Sand	Mohr-Coulomb	120	0	35
	Sand I	Mohr-Coulomb	115	0	34
	Sand II	Mohr-Coulomb	115	0	33
	Sand III	Mohr-Coulomb	115	0	39
	Sand IV	Mohr-Coulomb	115	0	41
	Sandy Clay Loam	Mohr-Coulomb	120	0	32
	Sandy Gravel	Mohr-Coulomb	120	0	31
	Sandy Loam	Mohr-Coulomb	120	0	29
	Silt	Mohr-Coulomb	110	150	26

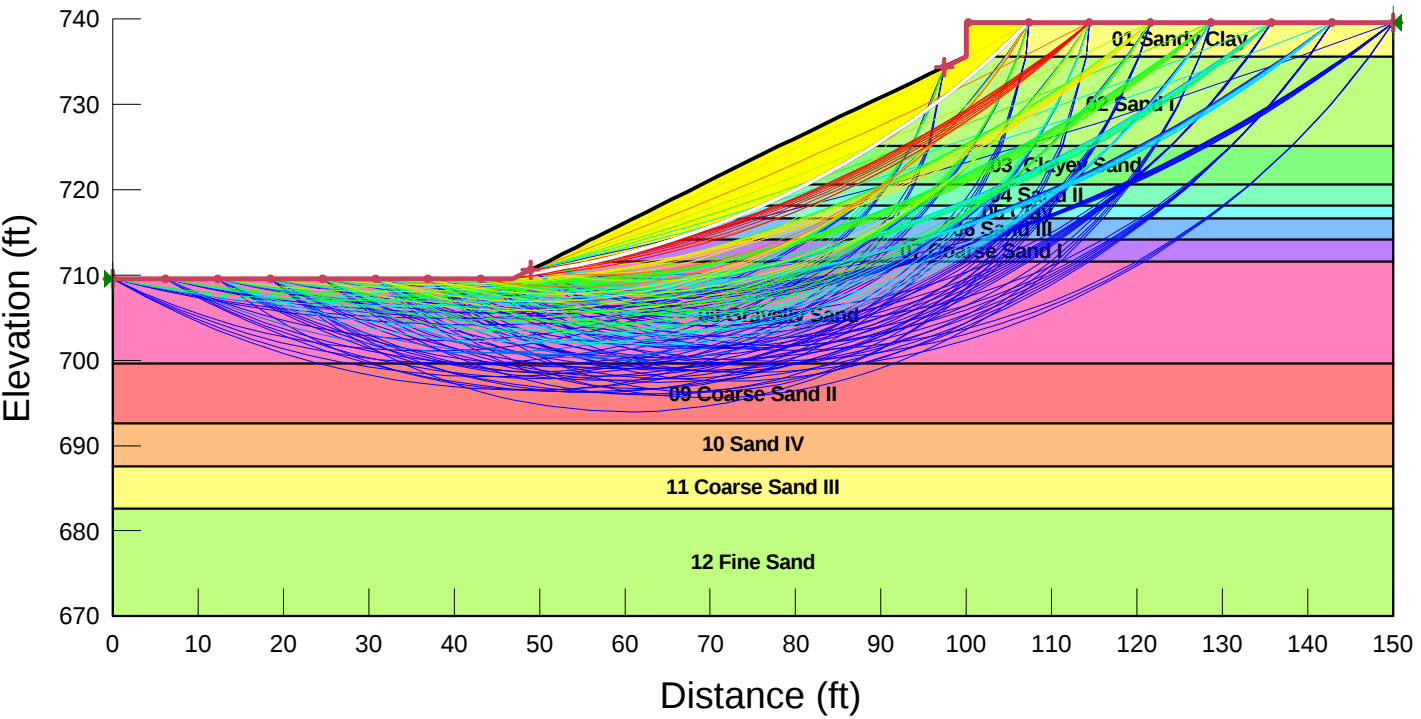
US 20 over Kishwaukee River
East Abutment (Eastbound)
Boring SB-08
End of Construction (Undrained Analysis)



Color	Name	Slope Stability Material Model	Unit Weight (pcf)	Effective Cohesion (psf)	Effective Friction Angle (°)
	01 Sandy Clay	Mohr-Coulomb	120	2,000	0
	02 Sand I	Mohr-Coulomb	115	0	35
	03 Clayey Sand	Mohr-Coulomb	120	0	36
	04 Sand II	Mohr-Coulomb	115	0	32
	05 Clay	Mohr-Coulomb	120	1,000	0
	06 Sand III	Mohr-Coulomb	115	0	30
	07 Coarse Sand I	Mohr-Coulomb	115	0	39
	08 Gravelly Sand	Mohr-Coulomb	120	0	35
	09 Coarse Sand II	Mohr-Coulomb	115	0	39
	10 Sand IV	Mohr-Coulomb	115	0	35
	11 Coarse Sand III	Mohr-Coulomb	115	0	43
	12 Fine Sand	Mohr-Coulomb	115	0	40

US 20 over Kishwaukee River
East Abutment (Eastbound)
Boring SB-08
Long Term (Drained Analysis)

1.5



Color	Name	Slope Stability Material Model	Unit Weight (pcf)	Effective Cohesion (psf)	Effective Friction Angle (°)
	01 Sandy Clay	Mohr-Coulomb	120	100	30
	02 Sand I	Mohr-Coulomb	115	0	35
	03 Clayey Sand	Mohr-Coulomb	120	0	36
	04 Sand II	Mohr-Coulomb	115	0	32
	05 Clay	Mohr-Coulomb	120	100	26
	06 Sand III	Mohr-Coulomb	115	0	30
	07 Coarse Sand I	Mohr-Coulomb	115	0	39
	08 Gravelly Sand	Mohr-Coulomb	120	0	35
	09 Coarse Sand II	Mohr-Coulomb	115	0	39
	10 Sand IV	Mohr-Coulomb	115	0	35
	11 Coarse Sand III	Mohr-Coulomb	115	0	43
	12 Fine Sand	Mohr-Coulomb	115	0	40

EXHIBIT G

PILE LENGTH/PILE TYPE

SUBSTRUCTURE=====WB - West Abut.
 REFERENCE BORING =====SB-01
 LRFD or ASD or SEISMIC =====LRFD
 PILE CUTOFF ELEV. =====732.78 ft
 GROUND SURFACE ELEV. AGAINST PILE DURING DRIVING = 730.78 ft
 GEOTECHNICAL LOSS TYPE (None, Scour, Liquef., DD) =====Scour
 BOTTOM ELEV. OF SCOUR, LIQUEF., or DD =====731.14 ft
 TOP ELEV. OF LIQUEF. (so layers above apply DD) =====ft

MAX. REQUIRED BEARING & RESISTANCE for Selected Pile, Soil Profile, & Losses

Maximum Nominal Req'd Bearing of Pile	Maximum Nominal Req'd Bearing of Boring	Maximum Factored Resistance Available in Boring	Maximum Pile Driveable Length in Boring
335 KIPS	330 KIPS	182 KIPS	88 FT.

TOTAL FACTORED SUBSTRUCTURE LOAD =====1500 kips
 TOTAL LENGTH OF SUBSTRUCTURE (along skew)=====57.50 ft
 NUMBER OF ROWS OF PILES PER SUBSTRUCTURE =====1
 Approx. Factored Loading Applied per pile at 8 ft. Cts =====208.70 KIPS
 Approx. Factored Loading Applied per pile at 3 ft. Cts =====78.26 KIPS

PILE TYPE AND SIZE =====Steel HP 10 X 42

Plugged Pile Perimeter=====3.300 FT. Unplugged Pile Perimeter=====4.858 FT.
 Plugged Pile End Bearing Area=====0.680 SQFT. Unplugged Pile End Bearing Area=====0.086 SQFT.

BOT. OF LAYER ELEV. (FT.)	LAYER THICK. (FT.)	UNCONF. COMPR. STRENGTH (TSF.)	S.P.T. N VALUE (BLOWS)	GRANULAR OR ROCK LAYER DESCRIPTION	NOMINAL PLUGGED			NOMINAL UNPLUG'D			NOMINAL REQ'D BEARING (KIPS)	FACTORED GEOTECH. LOSS FROM SCOUR or DD (KIPS)	FACTORED GEOTECH. LOSS LOAD FROM DD (KIPS)	FACTORED RESISTANCE AVAILABLE (KIPS)	ESTIMATED PILE LENGTH (FT.)
					SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)	SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)					
729.78	1.00		12	Medium Sand	0.7		17.8	1.1		3.2	3	0	0	2	3
727.28	2.50		24	Medium Sand	3.6	17.1	30.3	5.3	2.2	9.7	10	0	0	5	6
723.28	4.00		17	Medium Sand	4.1	25.9	27.5	6.0	3.3	14.8	15	0	0	8	10
722.28	1.00	2.00	14		3.8	19.1	40.9	5.7	2.4	21.7	22	0	0	12	11
719.78	2.50	3.00	12		12.6	28.6	43.9	18.6	3.6	39.0	39	0	0	21	13
716.78	3.00	2.00	7		11.5	19.1	80.5	17.0	2.4	59.2	59	0	0	33	16
714.28	2.50		26	Medium Sand	3.9	44.1	81.0	5.8	5.6	64.5	65	0	0	35	19
712.28	2.00		24	Sandy Gravel	3.8	40.7	88.2	5.5	5.1	70.5	70	0	0	39	21
709.78	2.50		26	Sandy Gravel	5.3	44.1	86.6	7.7	5.6	77.4	77	0	0	43	23
707.28	2.50		22	Clean Coarse Sand	3.6	37.3	90.2	5.3	4.7	82.7	83	0	0	45	26
704.78	2.50		22	Clean Coarse Sand	3.6	37.3	95.6	5.3	4.7	88.2	88	0	0	49	28
699.78	5.00		23	Clean Coarse Sand	7.6	39.0	108.2	11.1	4.9	100.0	100	0	0	55	33
694.78	5.00		26	Clean Coarse Sand	8.8	44.1	145.8	12.9	5.6	116.5	117	0	0	64	38
689.78	5.00		43	Clean Coarse Sand	19.8	72.9	194.4	29.2	9.2	149.4	149	0	0	82	43
684.78	5.00		60	Fine Sand	25.8	101.7	205.0	38.1	12.9	185.5	186	0	0	102	48
679.78	5.00		51	Fine Sand	19.7	86.4	245.1	29.0	10.9	217.1	217	0	0	119	53
674.78	5.00		63	Fine Sand	28.0	106.8	279.8	41.2	13.5	259.2	259	0	0	143	58
669.78	5.00		67	Fine Sand	31.2	113.6	300.8	45.9	14.4	303.8	301	0	0	165	63
664.78	5.00		61	Fine Sand	26.6	103.4	293.5	39.1	13.1	338.6	293	0	0	161	68
659.78	5.00		41	Fine Sand	13.6	69.5	300.3	20.0	8.8	357.7	300	0	0	165	73
654.78	5.00		37	Fine Sand	11.4	62.7	315.1	16.9	7.9	375.0	315	0	0	173	78
649.78	5.00		39	Fine Sand	12.5	66.1	329.3	18.4	8.4	393.5	329	0	0	181	83
644.78	5.00		40	Fine Sand	13.0	67.8	330.4	19.2	8.6	411.2	330	0	0	182	88
639.78	5.00		33	Fine Sand	9.6	55.9	351.9	14.2	7.1	426.9	352	0	0	194	93
634.78	5.00		40	Fine Sand	13.0	67.8	397.1	19.2	8.6	450.1	397	0	0	218	98
629.78	5.00		59	Fine Sand	25.1	100.0	412.1	37.0	12.7	485.8	412	0	0	227	103
624.78	5.00		53	Fine Sand	21.0	89.8	438.2	30.9	11.4	517.4	438	0	0	241	108
619.78	5.00		56	Fine Sand	23.1	94.9	440.9	33.9	12.0	548.8	441	0	0	243	113
614.78	5.00		44	Fine Sand		74.6			9.4						

SUBSTRUCTURE=====WB - Pier 1
REFERENCE BORING =====SB-03
LRFD or ASD or SEISMIC =====LRFD
PILE CUTOFF ELEV. =====711.50 ft
GROUND SURFACE ELEV. AGAINST PILE DURING DRIVING = 709.50 ft
GEOTECHNICAL LOSS TYPE (None, Scour, Liquef., DD) =====Scour
BOTTOM ELEV. OF SCOUR, LIQUEF., or DD =====701.84 ft
TOP ELEV. OF LIQUEF. (so layers above apply DD) =====ft

TOTAL FACTORED SUBSTRUCTURE LOAD =====3630 kips
TOTAL LENGTH OF SUBSTRUCTURE (along skew)=====57.50 ft
NUMBER OF ROWS OF PILES PER SUBSTRUCTURE =====1

Approx. Factored Loading Applied per pile at 8 ft. Cts ===== 505.04 KIPS
Approx. Factored Loading Applied per pile at 3 ft. Cts ===== 189.39 KIPS

MAX. REQUIRED BEARING & RESISTANCE for Selected Pile, Soil Profile, & Losses

Maximum Nominal Req'd Bearing of Pile	Maximum Nominal Req'd Bearing of Boring	Maximum Factored Resistance Available in Boring	Maximum Pile Driveable Length in Boring
335 KIPS	314 KIPS	170 KIPS	78 FT.

PILE TYPE AND SIZE =====Steel HP 10 X 42
Plugged Pile Perimeter===== 3.300 FT. Unplugged Pile Perimeter===== 4.858 FT. 82.022438
Plugged Pile End Bearing Area===== 0.680 SQFT. Unplugged Pile End Bearing Area===== 0.086 SQFT.

BOT. OF LAYER ELEV. (FT.)	LAYER THICK. (FT.)	UNCONF. COMPR. STRENGTH (TSF.)	S.P.T. N VALUE (BLOWS)	GRANULAR OR ROCK LAYER DESCRIPTION	NOMINAL PLUGGED			NOMINAL UNPLUG'D			NOMINAL REQ'D BEARING (KIPS)	FACTORED GEOTECH. LOSS FROM SCOUR or DD (KIPS)	FACTORED GEOTECH. LOSS LOAD FROM DD (KIPS)	FACTORED RESISTANCE AVAILABLE (KIPS)	ESTIMATED PILE LENGTH (FT.)
					SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)	SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)					
708.50	1.00		9	Clean Coarse Sand	0.6		7.0	0.9		1.7	2	0	0	1	3
706.00	2.50		9	Clean Coarse Sand	1.5	6.4	17.9	2.2	0.8	5.1	5	1	0	2	6
703.50	2.50		13	Clean Coarse Sand	2.1	15.9	19.8	3.1	2.0	8.2	8	2	0	2	8
701.84	1.66		10	Clean Coarse Sand	1.1	15.6	22.3	1.6	2.0	9.9	10	3	0	3	10
701.00	0.84		10	Clean Coarse Sand	0.6	17.0	33.0	0.8	2.1	12.1	12	3	0	4	11
698.50	2.50		16	Clean Coarse Sand	2.6	27.1	44.1	3.9	3.4	17.0	17	3	0	6	13
696.00	2.50		21	Clean Coarse Sand	3.5	35.6	66.2	5.1	4.5	24.4	24	3	0	11	16
693.50	2.50		32	Clean Coarse Sand	5.9	54.2	148.4	8.7	6.9	42.8	43	3	0	21	18
691.00	2.50		77	Sandy Gravel	40.1	130.5	227.5	59.0	16.5	106.8	107	3	0	56	21
688.50	2.50		100	Sandy Gravel	57.8	169.5	151.4	85.1	21.5	174.9	151	3	0	80	23
686.00	2.50		21	Medium Sand	3.2	35.6	163.0	4.6	4.5	180.7	163	3	0	87	26
683.50	2.50		26	Medium Sand	3.9	44.1	129.5	5.8	5.6	181.7	130	3	0	68	28
678.50	5.00	0.70	22		8.7	6.7	151.9	12.8	0.8	196.2	152	3	0	81	33
673.50	5.00		16	Very Fine Silty Sand	4.1	20.3	152.2	6.1	2.6	201.8	152	3	0	81	38
668.50	5.00		13	Very Fine Silty Sand	3.3	16.5	161.9	4.9	2.1	207.5	162	3	0	86	43
663.50	5.00		18	Very Fine Silty Sand	4.6	22.9	195.7	6.8	2.9	218.0	196	3	0	105	48
658.50	5.00		41	Very Fine Silty Sand	11.4	52.1	163.6	16.8	6.6	229.3	164	3	0	87	53
653.50	5.00	0.90	26		10.8	8.6	243.7	15.8	1.1	253.9	244	3	0	131	58
648.50	5.00		46	Fine Sand	16.5	78.0	263.6	24.3	9.9	278.6	264	3	0	142	63
643.50	5.00		48	Fine Sand	17.8	81.4	264.4	26.1	10.3	302.6	264	3	0	143	68
638.50	5.00		38	Fine Sand	12.0	64.4	276.4	17.6	8.2	320.2	276	3	0	149	73
633.50	5.00		38	Fine Sand	12.0	64.4	313.8	17.6	8.2	341.0	314	3	0	170	78
628.50	5.00		53	Fine Sand	21.0	89.8	339.9	30.9	11.4	372.6	340	3	0	184	83
623.50	5.00		56	Fine Sand	23.1	94.9	342.6	33.9	12.0	404.0	343	3	0	186	88
618.50	5.00		44	Fine Sand	15.3	74.6	357.9	22.5	9.4	426.5	358	3	0	194	93
613.50	5.00		44	Fine Sand	15.3	74.6	373.2	22.5	9.4	449.0	373	3	0	202	98
608.50	5.00		44	Fine Sand		74.6			9.4						

SUBSTRUCTURE=====WB - Pier 2
REFERENCE BORING =====SB-05
LRFD or ASD or SEISMIC =====LRFD
PILE CUTOFF ELEV. =====711.50 ft
GROUND SURFACE ELEV. AGAINST PILE DURING DRIVING = 709.50 ft
GEOTECHNICAL LOSS TYPE (None, Scour, Liquef., DD) =====Scour
BOTTOM ELEV. OF SCOUR, LIQUEF., or DD =====701.84 ft
TOP ELEV. OF LIQUEF. (so layers above apply DD) =====ft

TOTAL FACTORED SUBSTRUCTURE LOAD =====3630 kips
TOTAL LENGTH OF SUBSTRUCTURE (along skew)=====57.50 ft
NUMBER OF ROWS OF PILES PER SUBSTRUCTURE =====1

Approx. Factored Loading Applied per pile at 8 ft. Cts ===== 505.04 KIPS
Approx. Factored Loading Applied per pile at 3 ft. Cts ===== 189.39 KIPS

MAX. REQUIRED BEARING & RESISTANCE for Selected Pile, Soil Profile, & Losses

Maximum Nominal Req'd Bearing of Pile	Maximum Nominal Req'd Bearing of Boring	Maximum Factored Resistance Available in Boring	Maximum Pile Driveable Length in Boring
335 KIPS	330 KIPS	177 KIPS	97 FT.

PILE TYPE AND SIZE =====Steel HP 10 X 42

Plugged Pile Perimeter===== 3.300 FT. Unplugged Pile Perimeter===== 4.858 FT.
Plugged Pile End Bearing Area===== 0.680 SQFT. Unplugged Pile End Bearing Area===== 0.086 SQFT.

BOT. OF LAYER ELEV. (FT.)	LAYER THICK. (FT.)	UNCONF. COMPR. STRENGTH (TSF.)	S.P.T. N VALUE (BLOWS)	GRANULAR OR ROCK LAYER DESCRIPTION	NOMINAL PLUGGED			NOMINAL UNPLUG'D			NOMINAL REQ'D BEARING (KIPS)	FACTORED GEOTECH. LOSS FROM SCOUR or DD (KIPS)	FACTORED GEOTECH. LOSS LOAD FROM DD (KIPS)	FACTORED RESISTANCE AVAILABLE (KIPS)	ESTIMATED PILE LENGTH (FT.)
					SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)	SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)					
707.00	2.50		16	Clean Coarse Sand	2.6		15.9	3.9		5.5	6	1	0	2	5
704.50	2.50		13	Clean Coarse Sand	2.1	13.2	35.3	3.1	1.7	10.9	11	3	0	3	7
702.00	2.50		20	Clean Coarse Sand	3.3	30.5	37.7	4.8	3.9	15.6	16	4	0	4	10
701.84	0.16		19	Clean Coarse Sand	0.2	29.6	40.5	0.3	3.7	16.2	16	5	0	4	10
699.50	2.34		19	Clean Coarse Sand	2.9	32.2	40.0	4.3	4.1	20.1	20	5	0	7	12
697.00	2.50		17	Clean Coarse Sand	2.8	28.8	63.1	4.1	3.6	26.8	27	5	0	10	15
694.50	2.50		29	Clean Coarse Sand	5.1	49.2	61.5	7.5	6.2	33.5	33	5	0	14	17
692.00	2.50		25	Sandy Gravel	5.0	42.4	73.2	7.3	5.4	41.6	42	5	0	18	20
689.50	2.50		29	Sandy Gravel	6.2	49.2	64.2	9.2	6.2	48.9	49	5	0	22	22
687.00	2.50		20	Fine Sand	2.8	33.9	70.4	4.2	4.3	53.5	53	5	0	25	25
684.50	2.50		22	Fine Sand	3.1	37.3	45.8	4.6	4.7	54.5	46	5	0	21	27
682.00	2.50	1.00	26		5.9	9.5	70.7	8.6	1.2	65.6	66	5	0	32	30
679.50	2.50	3.00	38		12.6	28.6	59.5	18.6	3.6	81.1	59	5	0	28	32
674.50	5.00	0.50	46		6.4	4.8	118.4	9.5	0.6	97.3	97	5	0	49	37
669.50	5.00		45	Very Fine Silty Sand	13.0	57.2	142.8	19.2	7.2	117.9	118	5	0	60	42
664.50	5.00		54	Very Fine Silty Sand	17.3	68.6	114.3	25.5	8.7	137.5	114	5	0	58	47
659.50	5.00		18	Very Fine Silty Sand	4.6	22.9	108.5	6.8	2.9	143.0	108	5	0	55	52
654.50	5.00	1.30	17		14.3	12.4	163.8	21.1	1.6	169.3	164	5	0	86	57
649.50	5.00		42	Very Fine Silty Sand	11.8	53.4	191.7	17.3	6.8	188.7	189	5	0	99	62
644.50	5.00		41	Medium Sand	15.6	69.5	232.7	22.9	8.8	214.9	215	5	0	114	67
639.50	5.00		56	Medium Sand	27.8	94.9	241.9	41.0	12.0	253.5	242	5	0	129	72
634.50	5.00		45	Medium Sand	18.4	76.3	248.5	27.1	9.7	279.1	248	5	0	132	77
629.50	5.00		38	Fine Sand	12.0	64.4	285.9	17.6	8.2	299.9	286	5	0	153	82
624.50	5.00		53	Fine Sand	21.0	89.8	312.0	30.9	11.4	331.5	312	5	0	167	87
619.50	5.00		56	Fine Sand	23.1	94.9	314.7	33.9	12.0	362.9	315	5	0	169	92
614.50	5.00		44	Fine Sand	15.3	74.6	330.0	22.5	9.4	385.4	330	5	0	177	97
609.50	5.00		44	Fine Sand	15.3	74.6	345.3	22.5	9.4	407.9	345	5	0	185	102
604.50	5.00		44	Fine Sand		74.6			9.4						

SUBSTRUCTURE=====WB - East Abut.
REFERENCE BORING =====SB-07
LRFD or ASD or SEISMIC =====LRFD
PILE CUTOFF ELEV. =====732.41 ft
GROUND SURFACE ELEV. AGAINST PILE DURING DRIVING = 730.41 ft
GEOTECHNICAL LOSS TYPE (None, Scour, Liquef., DD) =====Scour
BOTTOM ELEV. OF SCOUR, LIQUEF., or DD =====730.77 ft
TOP ELEV. OF LIQUEF. (so layers above apply DD) =====ft

MAX. REQUIRED BEARING & RESISTANCE for Selected Pile, Soil Profile, & Losses

Maximum Nominal Req'd Bearing of Pile	Maximum Nominal Req'd Bearing of Boring	Maximum Factored Resistance Available in Boring	Maximum Pile Driveable Length in Boring
335 KIPS	325 KIPS	179 KIPS	83 FT.

TOTAL FACTORED SUBSTRUCTURE LOAD =====1500 kips
TOTAL LENGTH OF SUBSTRUCTURE (along skew)=====57.50 ft
NUMBER OF ROWS OF PILES PER SUBSTRUCTURE =====1
Approx. Factored Loading Applied per pile at 8 ft. Cts =====208.70 KIPS
Approx. Factored Loading Applied per pile at 3 ft. Cts =====78.26 KIPS

PILE TYPE AND SIZE =====Steel HP 10 X 42

Plugged Pile Perimeter=====3.300 FT. Unplugged Pile Perimeter=====4.858 FT.
Plugged Pile End Bearing Area=====0.680 SQFT. Unplugged Pile End Bearing Area=====0.086 SQFT.

BOT. OF LAYER ELEV. (FT.)	LAYER THICK. (FT.)	UNCONF. COMPR. STRENGTH (TSF.)	S.P.T. N VALUE (BLOWS)	GRANULAR OR ROCK LAYER DESCRIPTION	NOMINAL PLUGGED			NOMINAL UNPLUG'D			NOMINAL REQ'D BEARING (KIPS)	FACTORED GEOTECH. LOSS FROM SCOUR or DD (KIPS)	FACTORED GEOTECH. LOSS LOAD FROM DD (KIPS)	FACTORED RESISTANCE AVAILABLE (KIPS)	ESTIMATED PILE LENGTH (FT.)
					SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)	SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)					
729.41	1.00		23	Medium Sand	1.4		19.2	2.0		4.3	4	0	0	2	3
726.91	2.50		25	Medium Sand	3.8	17.8	44.2	5.5	2.3	12.5	13	0	0	7	6
724.41	2.50		32	Medium Sand	5.2	39.1	34.2	7.6	4.9	18.2	18	0	0	10	8
721.91	2.50	2.50	26		11.1	23.8	50.3	16.4	3.0	35.2	35	0	0	19	11
719.41	2.50		17	Medium Sand	2.6	28.8	39.2	3.8	3.6	37.3	37	0	0	20	13
716.91	2.50		9	Clean Coarse Sand	1.5	15.3	89.9	2.2	1.9	45.7	46	0	0	25	16
714.41	2.50		38	Sandy Gravel	10.4	64.4	74.9	15.3	8.2	57.7	58	0	0	32	18
711.91	2.50		23	Clean Coarse Sand	3.8	39.0	83.7	5.6	4.9	64.0	64	0	0	35	21
709.41	2.50		26	Medium Sand	3.9	44.1	75.8	5.8	5.6	68.2	68	0	0	38	23
704.41	5.00		19	Medium Sand	5.7	32.2	162.9	8.4	4.1	86.9	87	0	0	48	28
699.41	5.00		67	Medium Sand	37.9	113.6	129.6	55.8	14.4	133.7	130	0	0	71	33
694.41	5.00		25	Medium Sand	7.5	42.4	184.5	11.1	5.4	150.8	151	0	0	83	38
689.41	5.00		53	Clean Coarse Sand	29.4	89.8	190.3	43.4	11.4	191.1	190	0	0	105	43
684.41	5.00		39	Fine Sand	12.5	66.1	195.1	18.4	8.4	208.5	195	0	0	107	48
679.41	5.00		46	Very Fine Silty Sand	13.4	58.5	216.2	19.8	7.4	229.3	216	0	0	119	53
674.41	5.00		52	Very Fine Silty Sand	16.3	66.1	236.3	23.9	8.4	253.7	236	0	0	130	58
669.41	5.00		55	Very Fine Silty Sand	17.8	69.9	257.9	26.2	8.8	280.5	258	0	0	142	63
664.41	5.00		58	Very Fine Silty Sand	19.5	73.7	262.1	28.7	9.3	307.2	262	0	0	144	68
659.41	5.00		46	Very Fine Silty Sand	13.4	58.5	283.2	19.8	7.4	328.0	283	0	0	156	73
654.41	5.00		52	Very Fine Silty Sand	16.3	66.1	303.3	23.9	8.4	352.4	303	0	0	167	78
649.41	5.00		55	Very Fine Silty Sand	17.8	69.9	324.9	26.2	8.8	379.2	325	0	0	179	83
644.41	5.00		58	Very Fine Silty Sand	19.5	73.7	335.1	28.7	9.3	406.7	335	0	0	184	88
639.41	5.00		38	Fine Sand	12.0	64.4	372.5	17.6	8.2	427.5	372	0	0	205	93
634.41	5.00		53	Fine Sand	21.0	89.8	398.6	30.9	11.4	459.1	399	0	0	219	98
629.41	5.00		56	Fine Sand	23.1	94.9	401.3	33.9	12.0	490.5	401	0	0	221	103
624.41	5.00		44	Fine Sand	15.3	74.6	416.6	22.5	9.4	513.0	417	0	0	229	108
619.41	5.00		44	Fine Sand	15.3	74.6	431.9	22.5	9.4	535.5	432	0	0	238	113
614.41	5.00		44	Fine Sand		74.6			9.4						

SUBSTRUCTURE===== **EB - West Abut**
 REFERENCE BORING ===== **SB-02**
 LRFD or ASD or SEISMIC ===== **LRFD**
 PILE CUTOFF ELEV. ===== **732.87** ft
 GROUND SURFACE ELEV. AGAINST PILE DURING DRIVING = **730.87** ft
 GEOTECHNICAL LOSS TYPE (None, Scour, Liquef., DD) ===== **Scour**
 BOTTOM ELEV. OF SCOUR, LIQUEF., or DD ===== **731.14** ft
 TOP ELEV. OF LIQUEF. (so layers above apply DD) ===== ft

MAX. REQUIRED BEARING & RESISTANCE for Selected Pile, Soil Profile, & Losses

Maximum Nominal Req'd Bearing of Pile	Maximum Nominal Req'd Bearing of Boring	Maximum Factored Resistance Available in Boring	Maximum Pile Driveable Length in Boring
392 KIPS	374 KIPS	206 KIPS	32 FT.

TOTAL FACTORED SUBSTRUCTURE LOAD ===== **1500** kips
 TOTAL LENGTH OF SUBSTRUCTURE (along skew)===== **57.50** ft
 NUMBER OF ROWS OF PILES PER SUBSTRUCTURE ===== **1**
 Approx. Factored Loading Applied per pile at 8 ft. Cts ===== 208.70 KIPS
 Approx. Factored Loading Applied per pile at 3 ft. Cts ===== 78.26 KIPS

PILE TYPE AND SIZE ===== **Metal Shell 12"Φ w/.25" walls**
 Pile Perimeter===== 3.142 FT.
 Pile End Bearing Area===== 0.785 SQFT.

BOT. OF LAYER ELEV. (FT.)	LAYER THICK. (FT.)	UNCONF. COMPR. STRENGTH (TSF.)	S.P.T. N VALUE (BLOWS)	GRANULAR OR ROCK LAYER DESCRIPTION	NOMINAL						NOMINAL REQ'D BEARING (KIPS)	FACTORED GEOTECH. LOSS FROM SCOUR or DD (KIPS)	FACTORED GEOTECH. LOSS LOAD FROM DD (KIPS)	FACTORED RESISTANCE AVAILABLE (KIPS)	ESTIMATED PILE LENGTH (FT.)
					SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)								
727.37	3.50		12	Medium Sand	12.1		65.5				66	0	0	36	6
724.87	2.50		18	Medium Sand	13.0	53.4	33.8				34	0	0	19	8
722.37	2.50	1.00	17		8.7	8.6	108.1				108	0	0	59	11
719.87	2.50		15	Sandy Gravel	13.9	74.2	112.1				112	0	0	62	13
715.87	4.00		13	Sandy Gravel	19.3	64.3	185.7				186	0	0	102	17
713.37	2.50		24	Sandy Gravel	22.6	118.7	168.8				169	0	0	93	20
710.87	2.50		16	Sandy Gravel	14.8	79.1	302.3				302	0	0	166	22
705.87	5.00		40	Sandy Gravel	111.2	197.8	294.9				295	0	0	162	27
700.87	5.00		16	Sandy Gravel	29.7	79.1	374.0				374	0	0	206	32
695.87	5.00		26	Sandy Gravel	50.5	128.5	436.9				437	0	0	240	37
690.87	5.00		38	Very Fine Silty Sand	49.5	140.9	508.6				509	0	0	280	42
685.87	5.00		44	Very Fine Silty Sand	60.6	163.2	558.1				558	0	0	307	47
680.87	5.00		41	Very Fine Silty Sand	54.8	152.0	650.0				650	0	0	357	52
675.87	5.00		51	Very Fine Silty Sand	75.9	189.1	714.7				715	0	0	393	57
670.87	5.00		48	Very Fine Silty Sand	69.0	178.0	754.0				754	0	0	415	62
665.87	5.00		40	Very Fine Silty Sand		148.3									

SUBSTRUCTURE===== **EB - Pier 1**
REFERENCE BORING ===== **SB-04**
LRFD or ASD or SEISMIC ===== **LRFD**
PILE CUTOFF ELEV. ===== **711.50** ft
GROUND SURFACE ELEV. AGAINST PILE DURING DRIVING = **709.50** ft
GEOTECHNICAL LOSS TYPE (None, Scour, Liquef., DD) ===== **Scour**
BOTTOM ELEV. OF SCOUR, LIQUEF., or DD ===== **701.84** ft
TOP ELEV. OF LIQUEF. (so layers above apply DD) ===== ft

MAX. REQUIRED BEARING & RESISTANCE for Selected Pile, Soil Profile, & Losses

Maximum Nominal Req'd Bearing of Pile	Maximum Nominal Req'd Bearing of Boring	Maximum Factored Resistance Available in Boring	Maximum Pile Driveable Length in Boring
335 KIPS	329 KIPS	175 KIPS	77 FT.

TOTAL FACTORED SUBSTRUCTURE LOAD ===== **3630** kips
TOTAL LENGTH OF SUBSTRUCTURE (along skew)===== **57.50** ft
NUMBER OF ROWS OF PILES PER SUBSTRUCTURE ===== **1**
Approx. Factored Loading Applied per pile at 8 ft. Cts ===== 505.04 KIPS
Approx. Factored Loading Applied per pile at 3 ft. Cts ===== 189.39 KIPS

PILE TYPE AND SIZE ===== **Steel HP 10 X 42**

Plugged Pile Perimeter===== 3.300 FT. Unplugged Pile Perimeter===== 4.858 FT.
Plugged Pile End Bearing Area===== 0.680 SQFT. Unplugged Pile End Bearing Area===== 0.086 SQFT.

BOT. OF LAYER ELEV. (FT.)	LAYER THICK. (FT.)	UNCONF. COMPR. STRENGTH (TSF.)	S.P.T. N VALUE (BLOWS)	GRANULAR OR ROCK LAYER DESCRIPTION	NOMINAL PLUGGED			NOMINAL UNPLUG'D			NOMINAL REQ'D BEARING (KIPS)	FACTORED GEOTECH. LOSS FROM SCOUR or DD (KIPS)	FACTORED GEOTECH. LOSS LOAD FROM DD (KIPS)	FACTORED RESISTANCE AVAILABLE (KIPS)	ESTIMATED PILE LENGTH (FT.)
					SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)	SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)					
707.00	2.50		13	Medium Sand	2.0		32.5	2.9		6.7	7	1	0	3	5
704.50	2.50		30	Medium Sand	4.7	30.5	30.8	7.0	3.9	12.9	13	4	0	3	7
704.34	0.16		23	Sandy Gravel	0.3	24.1	42.0	0.4	3.1	14.7	15	4	0	4	7
702.00	2.34		23	Sandy Gravel	4.2	35.1	53.5	6.1	4.4	21.8	22	6	0	6	10
699.50	2.50		25	Sandy Gravel	5.0	42.4	38.1	7.3	5.4	26.5	26	6	0	8	12
697.00	2.50		13	Sandy Gravel	2.5	22.0	59.3	3.7	2.8	32.5	33	6	0	12	15
694.50	2.50		24	Sandy Gravel	4.7	40.7	118.2	6.9	5.1	46.3	46	6	0	19	17
692.00	2.50		56	Sandy Gravel	23.9	94.9	159.1	35.2	12.0	83.7	84	6	0	40	20
689.50	2.50		66	Sandy Gravel	31.6	111.9	142.4	46.5	14.2	124.1	124	6	0	62	22
684.50	5.00		50	Very Fine Silty Sand	15.3	63.6	138.6	22.5	8.0	144.2	139	6	0	70	27
679.50	5.00		35	Very Fine Silty Sand	9.3	44.5	150.4	13.6	5.6	158.1	150	6	0	77	32
674.50	5.00		37	Very Fine Silty Sand	9.9	47.0	169.2	14.6	6.0	173.9	169	6	0	87	37
669.50	5.00		44	Very Fine Silty Sand	12.6	55.9	185.6	18.5	7.1	192.9	186	6	0	96	42
664.50	5.00		47	Very Fine Silty Sand	13.9	59.8	148.3	20.4	7.6	206.9	148	6	0	75	47
659.50	5.00	0.90	29		10.8	8.6	220.4	15.8	1.1	230.5	220	6	0	115	52
654.50	5.00		55	Very Fine Silty Sand	17.8	69.9	267.5	26.2	8.8	260.4	260	6	0	137	57
649.50	5.00		78	Very Fine Silty Sand	33.3	99.2	256.3	49.0	12.5	303.8	256	6	0	135	62
644.50	5.00		43	Very Fine Silty Sand	12.2	54.7	271.1	17.9	6.9	322.1	271	6	0	143	67
639.50	5.00		45	Very Fine Silty Sand	13.0	57.2	291.3	19.2	7.2	342.1	291	6	0	154	72
634.50	5.00		38	Fine Sand	12.0	64.4	328.7	17.6	8.2	363.0	329	6	0	175	77
629.50	5.00		53	Fine Sand	21.0	89.8	354.8	30.9	11.4	394.5	355	6	0	199	82
624.50	5.00		56	Fine Sand	23.1	94.9	357.5	33.9	12.0	425.9	357	6	0	190	87
619.50	5.00		44	Fine Sand	15.3	74.6	372.8	22.5	9.4	448.4	373	6	0	199	92
614.50	5.00		44	Fine Sand	15.3	74.6	388.1	22.5	9.4	470.9	388	6	0	207	97
609.50	5.00		44	Fine Sand		74.6			9.4						

SUBSTRUCTURE===== **EB - Pier 2**
REFERENCE BORING ===== **SB-06**
LRFD or ASD or SEISMIC ===== **LRFD**
PILE CUTOFF ELEV. ===== **711.50** ft
GROUND SURFACE ELEV. AGAINST PILE DURING DRIVING = **709.50** ft
GEOTECHNICAL LOSS TYPE (None, Scour, Liquef., DD) ===== **Scour**
BOTTOM ELEV. OF SCOUR, LIQUEF., or DD ===== **701.84** ft
TOP ELEV. OF LIQUEF. (so layers above apply DD) ===== ft

MAX. REQUIRED BEARING & RESISTANCE for Selected Pile, Soil Profile, & Losses

Maximum Nominal Req'd Bearing of Pile	Maximum Nominal Req'd Bearing of Boring	Maximum Factored Resistance Available in Boring	Maximum Pile Driveable Length in Boring
335 KIPS	327 KIPS	176 KIPS	73 FT.

TOTAL FACTORED SUBSTRUCTURE LOAD ===== **1500** kips
TOTAL LENGTH OF SUBSTRUCTURE (along skew)===== **57.50** ft
NUMBER OF ROWS OF PILES PER SUBSTRUCTURE ===== **1**
Approx. Factored Loading Applied per pile at 8 ft. Cts ===== 208.70 KIPS
Approx. Factored Loading Applied per pile at 3 ft. Cts ===== 78.26 KIPS

PILE TYPE AND SIZE ===== **Steel HP 10 X 42**

Plugged Pile Perimeter===== 3.300 FT. Unplugged Pile Perimeter===== 4.858 FT.
Plugged Pile End Bearing Area===== 0.680 SQFT. Unplugged Pile End Bearing Area===== 0.086 SQFT.

BOT. OF LAYER ELEV. (FT.)	LAYER THICK. (FT.)	UNCONF. COMPR. STRENGTH (TSF.)	S.P.T. N VALUE (BLOWS)	GRANULAR OR ROCK LAYER DESCRIPTION	NOMINAL PLUGGED			NOMINAL UNPLUG'D			NOMINAL REQ'D BEARING (KIPS)	FACTORED GEOTECH. LOSS FROM SCOUR or DD (KIPS)	FACTORED GEOTECH. LOSS LOAD FROM DD (KIPS)	FACTORED RESISTANCE AVAILABLE (KIPS)	ESTIMATED PILE LENGTH (FT.)
					SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)	SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)					
706.50	3.00		7	Sandy Gravel	1.6		16.2	2.4		4.2	4	1	0	1	5
704.00	2.50		13	Sandy Gravel	2.5	14.5	32.2	3.7	1.8	9.6	10	2	0	3	8
701.84	2.16		18	Sandy Gravel	3.0	28.0	36.4	4.4	3.5	14.2	14	4	0	4	10
701.50	0.34		18	Sandy Gravel	0.5	29.3	177.1	0.7	3.7	32.6	33	4	0	14	10
699.00	2.50		100	Sandy Gravel	57.8	169.5	131.5	85.1	21.5	104.7	105	4	0	54	13
696.50	2.50		39	Sandy Gravel	11.0	66.1	134.0	16.2	8.4	119.7	120	4	0	62	15
694.00	2.50		34	Sandy Gravel	8.3	57.6	138.9	12.3	7.3	131.6	132	4	0	68	18
691.50	2.50		32	Sandy Gravel	7.4	54.2	129.0	10.9	6.9	140.3	129	4	0	67	20
689.00	2.50		29	Very Fine Silty Sand	3.7	36.9	128.9	5.5	4.7	145.3	129	4	0	67	23
686.50	2.50		26	Very Fine Silty Sand	3.3	33.1	104.0	4.9	4.2	146.6	104	4	0	53	25
684.00	2.50	0.50	31		3.2	4.8	141.8	4.7	0.6	155.8	142	4	0	74	28
681.50	2.50		31	Very Fine Silty Sand	4.0	39.4	157.3	5.9	5.0	163.1	157	4	0	83	30
679.00	2.50		40	Very Fine Silty Sand	5.5	50.9	169.1	8.1	6.4	172.0	169	4	0	89	33
674.00	5.00		45	Very Fine Silty Sand	13.0	57.2	197.4	19.2	7.2	193.1	193	4	0	102	38
669.00	5.00		57	Very Fine Silty Sand	18.9	72.5	230.3	27.9	9.2	222.8	223	4	0	119	43
664.00	5.00		68	Very Fine Silty Sand	25.9	86.4	252.4	38.1	10.9	260.3	252	4	0	135	48
659.00	5.00		65	Very Fine Silty Sand	23.8	82.6	257.1	35.1	10.5	293.0	257	4	0	137	53
654.00	5.00		50	Very Fine Silty Sand	15.3	63.6	254.6	22.5	8.0	313.2	255	4	0	136	58
649.00	5.00		36	Very Fine Silty Sand	9.6	45.8	310.0	14.1	5.8	333.2	310	4	0	167	63
644.00	5.00		72	Very Fine Silty Sand	28.7	91.5	312.0	42.3	11.6	372.1	312	4	0	168	68
639.00	5.00		51	Very Fine Silty Sand	15.8	64.8	327.3	23.2	8.2	395.2	327	4	0	176	73
634.00	5.00		38	Fine Sand	12.0	64.4	364.7	17.6	8.2	416.1	365	4	0	197	78
629.00	5.00		53	Fine Sand	21.0	89.8	390.8	30.9	11.4	447.6	391	4	0	211	83
624.00	5.00		56	Fine Sand	23.1	94.9	393.5	33.9	12.0	479.0	394	4	0	213	88
619.00	5.00		44	Fine Sand	15.3	74.6	408.8	22.5	9.4	501.5	409	4	0	221	93
614.00	5.00		44	Fine Sand	15.3	74.6	424.1	22.5	9.4	524.1	424	4	0	229	98
609.00	5.00		44	Fine Sand		74.6			9.4						

SUBSTRUCTURE===== **EB - East Abut.**
REFERENCE BORING ===== **SB-08**
LRFD or ASD or SEISMIC ===== **LRFD**
PILE CUTOFF ELEV. ===== **732.41** ft
GROUND SURFACE ELEV. AGAINST PILE DURING DRIVING = **730.41** ft
GEOTECHNICAL LOSS TYPE (None, Scour, Liquef., DD) ===== **Scour**
BOTTOM ELEV. OF SCOUR, LIQUEF., or DD ===== **730.77** ft
TOP ELEV. OF LIQUEF. (so layers above apply DD) ===== ft

MAX. REQUIRED BEARING & RESISTANCE for Selected Pile, Soil Profile, & Losses

Maximum Nominal Req'd Bearing of Pile	Maximum Nominal Req'd Bearing of Boring	Maximum Factored Resistance Available in Boring	Maximum Pile Driveable Length in Boring
335 KIPS	292 KIPS	160 KIPS	58 FT.

TOTAL FACTORED SUBSTRUCTURE LOAD ===== **1500** kips
TOTAL LENGTH OF SUBSTRUCTURE (along skew)===== **57.50** ft
NUMBER OF ROWS OF PILES PER SUBSTRUCTURE ===== **1**
Approx. Factored Loading Applied per pile at 8 ft. Cts ===== 208.70 KIPS
Approx. Factored Loading Applied per pile at 3 ft. Cts ===== 78.26 KIPS

PILE TYPE AND SIZE ===== **Steel HP 10 X 42**

Plugged Pile Perimeter===== 3.300 FT. Unplugged Pile Perimeter===== 4.858 FT.
Plugged Pile End Bearing Area===== 0.680 SQFT. Unplugged Pile End Bearing Area===== 0.086 SQFT.

BOT. OF LAYER ELEV. (FT.)	LAYER THICK. (FT.)	UNCONF. COMPR. STRENGTH (TSF.)	S.P.T. N VALUE (BLOWS)	GRANULAR OR ROCK LAYER DESCRIPTION	NOMINAL PLUGGED			NOMINAL UNPLUG'D			NOMINAL REQ'D BEARING (KIPS)	FACTORED GEOTECH. LOSS FROM SCOUR or DD (KIPS)	FACTORED GEOTECH. LOSS LOAD FROM DD (KIPS)	FACTORED RESISTANCE AVAILABLE (KIPS)	ESTIMATED PILE LENGTH (FT.)
					SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)	SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)					
727.41	3.00		33	Sandy Gravel	9.4		27.3	13.9		16.2	16	0	0	9	5
724.91	2.50		16	Sandy Gravel	3.1	17.9	41.5	4.5	2.3	22.1	22	0	0	12	8
722.91	2.00		19	Sandy Gravel	2.9	29.0	46.0	4.3	3.7	26.6	27	0	0	15	10
719.91	3.00		18	Sandy Gravel	4.2	30.5	29.2	6.1	3.9	30.1	29	0	0	16	13
717.91	2.00	1.00	16		4.7	9.5	65.0	6.9	1.2	40.9	41	0	0	23	15
715.41	2.50		24	Sandy Gravel	4.7	40.7	39.2	6.9	5.1	44.0	39	0	0	22	17
712.41	3.00		6	Sandy Gravel	1.4	10.2	69.4	2.0	1.3	49.7	50	0	0	27	20
709.91	2.50		23	Sandy Gravel	4.5	39.0	82.3	6.6	4.9	57.3	57	0	0	32	23
704.91	5.00		28	Sandy Gravel	11.8	47.5	89.0	17.3	6.0	74.0	74	0	0	41	28
699.91	5.00		25	Sandy Gravel	9.9	42.4	126.1	14.6	5.4	92.1	92	0	0	51	33
694.91	5.00		41	Sandy Gravel	24.7	69.5	216.8	36.3	8.8	136.8	137	0	0	75	38
689.91	5.00		80	Sandy Gravel	84.8	135.6	220.7	124.8	17.2	251.3	221	0	0	121	43
684.91	5.00		43	Very Fine Silty Sand	12.2	54.7	229.1	17.9	6.9	268.8	229	0	0	126	48
679.91	5.00		40	Very Fine Silty Sand	11.0	50.9	251.5	16.2	6.4	286.5	252	0	0	138	53
674.91	5.00		49	Very Fine Silty Sand	14.8	62.3	291.7	21.8	7.9	311.5	292	0	0	160	58
669.91	5.00		69	Very Fine Silty Sand	26.6	87.7	315.8	39.1	11.1	350.2	316	0	0	174	63
664.91	5.00		67	Very Fine Silty Sand	25.2	85.2	346.0	37.0	10.8	387.9	346	0	0	190	68
659.91	5.00		71	Very Fine Silty Sand	28.0	90.3	323.2	41.2	11.4	422.7	323	0	0	178	73
654.91	5.00		31	Very Fine Silty Sand	8.0	39.4	295.6	11.8	5.0	430.0	296	0	0	163	78
649.91	5.00	0.40	15		5.2	3.8	320.8	7.7	0.5	440.3	321	0	0	176	83
644.91	5.00	2.50	37		22.2	23.8	387.0	32.7	3.0	478.6	387	0	0	213	88
639.91	5.00		40	Sandy Gravel	23.1	67.8	435.6	34.0	8.6	515.8	436	0	0	240	93
634.91	5.00		55	Sandy Gravel	46.2	93.2	502.2	68.1	11.8	586.5	502	0	0	276	98
629.91	5.00		67	Medium Sand	37.9	113.6	501.1	55.8	14.4	637.3	501	0	0	276	103
624.91	5.00		44	Medium Sand	17.7	74.6	540.8	26.0	9.4	666.2	541	0	0	297	108
619.91	5.00		57	Medium Sand	28.8	96.6	554.3	42.3	12.2	706.6	554	0	0	305	113
614.91	5.00		48	Clean Coarse Sand		81.4			10.3						