STRUCTURE GEOTECHNICAL REPORT

068-2508

Existing SN: 068-0016

IL 16 over Tributary to the South Fork of the Sangamon River

Route: FAP 325 Section: 18(B-2,B-3) Montgomery County

D-96-522-05 Contract # 72984

Prepared By: Luke Murphy, PE IDOT Region 4 District 6 Geotechnical Unit 217-782-6709 Checked By: <u>LTM</u>

Approved By:

Luke Murphy, P.E. D-6 Geotechnical Engr.

Lic. #062-071192 Date: 2/17/2023

Date: August 14, 2019 **Revised:** February 17, 2023

Prepared For: Mary Coobme Bloxdorf Fehr-Graham Consultants Attachments: Structure Plans Subsurface Profile

> Boring Logs Special Provisions

This Report has been prepared based on a "Approved" Structure Plans dated January 20, 2023. Contact the author if there are any questions regarding this Report or if there are modifications to structure location, size, geometry, or vertical alignment.

Electronic copies of boring logs are available upon request for inclusion in the plans. Calculations are also available upon request.

This Report has been prepared according to AASHTO Standard Specifications for Highway Bridges 9th Edition 2020 and the 2023 IDOT BBS Bridge Manual.

Project Description and Proposed Structure Information

This project consists of the removal of the existing 26 ft single span bridge on closed abutments and replacing it with a triple 8'Hx12'W box culvert. Work will be performed under stage construction.

Proposed horizontal cantilever wingwalls are approximately 13.5 ft long and 9.5 ft high. There is approximately 1ft of fill above the culvert. An approximate 1.5 ft change in roadway grade is proposed.

Existing Structure and Site Investigation

The existing single span bridge was constructed in 1923.

The existing structure is located in level terrain, and the primary area land use is cultivated fields. The approach roadway is at or near grade. No existing settlement or stability problems were observed.

The channel banks are approximately 5ft and near 2V:1H slopes with no evidence of sloughing.

Rip rap has been placed under the bridge and along the banks where ditches outlet into the stream.

New borings were advanced on the existing driving lanes at the northwest and southeast corners. Borings were advanced to 25± ft below streambed by the District 6 drill crew according to AASHTO T 206 and the IDOT Geotechnical Manual.

Boring data indicates approximately 2 ft of clay loam over 13 ±ft of sand over clay loam till. Borings on roadways are filled to prevent a hazard immediately after drilling. As a result, no 24hour water elevation observations were made. The boring data indicates groundwater was encountered at 655.0 ft corresponding to the top of sand.

Geotechnical Evaluation

Settlement. There is a minor change in grade. Empirical settlement calculations estimate a settlement of less than 1 inch beneath the box. Settlement is not anticipated to be a problem.

Slope Stability. The stability of a 1:1 temporary construction slope has been analyzed including excavation to elevation 658 ft. The resulting factor-of-safety is 2.7. No stability issues are anticipated.

Seismic Considerations. Seismic events are not a significant design consideration for culverts. No analysis is required.

Scour. A 100 year scour estimate has not been calculated for the proposed culvert. The design scour elevation should correspond to the bottom of toe wall elevation. Based on available information, the upstream design scour elevation is 656.15 ft, and the downstream design scour elevation is 655.85 ft. These elevations may be adjusted during final design.

Mining Activity. ISGS records indicate no mining beneath the proposed structure.

Foundation Evaluation

Culvert Barrel. A pre-cast culvert is feasible at this site. If the pre-cast alternative is selected, cast-in-place headwalls should be included. No ground improvement is required

Wingwalls. Originally the design called for horizontal cantilevered wingwalls for both the up and downstream ends of the culvert. Due to complications acquiring Right of Way on the downstream end of the box culvert, other wingwall types have been explored on the downstream end.

<u>Soil Properties for Analysis:</u> The table below contains soil properties to be used for embedment and section modulus analysis of a sheet or soldier pile wall.

| Elev | ation | Soil Tuno | Ύ (pcf) | | Undra | ained | | Drained | | | |
|--------|--------|----------------|---------|---------|-------|-------|------|---------|----|------|------|
| Тор | Bottom | Soil Type | r (pcr) | C (psf) | ф | Ка | Кр | C (psf) | ф | Ка | Кр |
| 668.88 | 663.5 | Silty Clay | 120 | 1000 | | 1 | 1 | | 26 | 0.36 | 3.31 |
| 663.5 | 655.5 | Clay Loam | 120 | 700 | | 1 | 1 | | 26 | 0.36 | 3.31 |
| 655.5 | 650 | Fine Sand | 110 | | 29 | 0.32 | 3.97 | | 29 | 0.32 | 3.97 |
| 650 | 641 | Sandy Gravel | 125 | | 32 | 0.28 | 4.76 | | 32 | 0.28 | 4.76 |
| 641 | - | Clay Loam Till | 130 | 7200 | | 1 | 1 | 500 | 28 | 0.33 | 3.66 |

The borings showed very consistent stratigraphy with similar blow counts and unconfined compressive strengths. The cohesion (C) was taken from field Rimac results. The undrained phi angle of the Fine Sand and Sandy Gravel where taken from Wolffe 1989 and FDOT 2012. The drained phi angle of cohesive soils was based on Table 4-6 of USACE EM 1110-2-2906. Ka's and Kp's were calculated using Coulomb and assuming the wall friction angle is equal to a third of the angle of internal friction.

The effective cohesion of the Clay Loam Till was assumed as 500 psf. As taken from MnDOT Report MN/RC 2018-32 the effective cohesion could be approximately 10% of the undrained cohesion. Given the high unconfined compressive strengths of this layer, ranging from 7.2 to 10 tsf, it is believed this soil would retain cohesion in the drained condition.

Using the soil properties from the Table above, the below table of earth pressures was derived. These represent the factored values per foot of wall. The active and passive values will need multiplied by the appropriate widths for the analyses. This would be equal to the pile spacing for active and the smaller of 3 times the pile width or the pile spacing for passive.

| | | | | | σ'h (undrained) Factored per foot | | | | | | σ'h (drained) Factored per foot | | | | |
|-----------|---------|---------|--------------|---------|-----------------------------------|----------|----------|----------|----------|---------|---------------------------------|---------|---------|---------|---------|
| | | | | act | ive | pas | sive | net (-a | active) | act | ive | pas | sive | net (-a | active) |
| Elevation | σ'va | σ'vp | LL Surcharge | top | bottom | top | bottom | top | bottom | top | bottom | top | bottom | top | bottom |
| 668.88 | 0 | | 240 | 105 | | | | -105 | | 151.2 | | | | -151.2 | |
| 663.5 | 645.6 | | 240 | 347.1 | | | | -347.1 | | 499.82 | | | | -499.82 | |
| 655.63 | 1590 | 0 | 240 | 701.25 | | 1050 | | 348.75 | | 1009.8 | | 0 | | -1009.8 | |
| 655.5 | 1597.49 | 7.49 | 240 | 704.06 | 901.2 | 1055.62 | 22.3 | 351.56 | -878.9 | 1013.84 | 901.2 | 18.59 | 22.3 | -995.25 | -878.9 |
| 650 | 1859.29 | 269.29 | 240 | 1026.86 | 898.5 | 801.81 | 961.37 | -225.05 | 62.87 | 1026.86 | 898.5 | 801.81 | 961.37 | -225.05 | 62.87 |
| 641 | 2422.69 | 832.69 | 240 | 1135.13 | 1013.51 | 2972.7 | 11424.52 | 1837.57 | 10410.99 | 1135.13 | 1013.51 | 2972.7 | 5030.74 | 1837.57 | 4017.23 |
| 635 | 2828.29 | 1238.29 | 240 | 1165.61 | | 11728.72 | | 10563.09 | | 1165.61 | | 6144.11 | | 4978.5 | |

From the Allpile User's Manual, the below table of soil properties used specifically for lateral analysis was complied and should be used by the Consultant.

| Eleva | ation | Soil Type | K (pci) | e50(%) |
|--------|--------|----------------|---------|--------|
| Тор | Bottom | Son Type | K (pci) | e50(%) |
| 668.88 | 663.5 | Silty Clay | 100 | 1 |
| 663.5 | 655.5 | Clay Loam | 70 | 1.5 |
| 655.5 | 650 | Fine Sand | 20 | - |
| 650 | 641 | Sandy Gravel | 60 | - |
| 641 | - | Clay Loam Till | 2000 | 0.4 |

<u>Preliminary Feasibility Analyses:</u> Preliminary Analyses using an internal spreadsheet was conducted for the purpose of determining feasibility.

<u>Cantilevered Sheet Pile Wall:</u> The preliminary analysis for a cantilevered sheet pile wall showed a minimum section modulus of 30 cubic inches per foot, not accounting for corrosion, and a tip elevation of 628 would be required, with the limiting case being the drained condition. The tip elevation would be 13 feet into Clay Loam Till with blow counts ranging from 31 to 66 and Qu's ranging from 7.2 to 10 tsf. It is anticipated that driving sheet pile this deep into this layer would prove difficult at best and have a high probability to damage the sheet pile. A cantilevered sheet pile wall is not recommended. Technically anchors could be used to reduce the tip elevation and section modulus, however the anchors would have to extend underneath the road, which is not recommended unless other wall types are economically not feasible.

<u>Cantilevered Soldier Pile Wall:</u> A cantilevered soldier pile could be used. Using the soil properties from this memo and an internal spreadsheet the below table documents the tip elevation, minimum section modulus (not accounting for corrosion), and acceptable structural shapes, which can be refined further by Structural Engineer.

| Pile Spacing | Tip Elevation | Minimum Section Modulus | Acceptable Shapes |
|--------------|---------------|----------------------------|--------------------|
| 3.5' | 637 | 87.2 | HP 14x73 or above |
| 3.75' | 637 | 87.2 | TP 14X73 OF above |
| 4' | 637 | 110.6 | |
| 4.25' | 636 | 110.6 | HP 14x89 or above |
| 4.5' | 636 | 110.6 | HP 14x09 0I above |
| 5' | 635 | 110.6 | |
| 5.5' | 634 | 130.4 | HP 14x102 or above |
| 6' | 634 | 130.4 | HF 14X102 OF above |
| 6.5' | 633 | 152.3 | |
| 7' | 632 | 152.3 | HP 14x117 or above |
| 7.5' | 633 | 152.3 | |

A drivability analysis, using BBS 147 demonstrated that the piles could be driven to the desired tip elevations without issue, however it is believed that the analysis does not adequately model the Till's, shear strength and stiffness, as the till can have unconfined compressive strengths in excess of 9 tsf. Given this, even though the boring shows sandy soils, complicating the drilling process, the soldier piles should be set in drilled shafts extending to the calculated tip elevations.

<u>T-Type:</u> T-Type and other wall types better suited for "Fill" situations were eliminated as installing them close to the edge of pavement would require additional temporary retention, making a "Cut" type of wall, sheet or soldier pile, economically more ideal.

<u>Final Recommendation(s)</u>: Our recommendation for the final configuration of the downstream end would be a cantilevered soldier pile wall with the soldier piles being set in drilled shafts, utilizing only readily available HP Sections. If more detailed analysis precludes the use of a cantilevered soldier pile wall, utilizing readily available HP Sections, we would recommend a cantilevered soldier pile with a larger W section. The upstream end should utilize horizontal cantilevered wingwalls.

Construction Considerations

Stage Construction. This project will be constructed under stage construction.

Temporary Soil Retention. Temporary retention will be required to facilitate stage construction. The estimated maximum retained height is 11 ft. A preliminary analysis indicates a cantilevered sheet pile wall is feasible. If the final design shows a sheet pile tip elevation below 644 ft, a dense sand layer may prevent adequate embedment. In that case, use the Temporary Soil Retention System.

The designer has indicated a 1H: 1V slope on the backfill area above stage I construction. The granular culvert backfill should be wrapped with geotextile to prevent rock loss, a detail is attached. No additional retention methods are required.

Excavation. Existing abutments should be removed to 2 ft below the proposed culvert barrel and should be backfilled with <u>Rockfill-Foundation</u>. The special provision is attached.

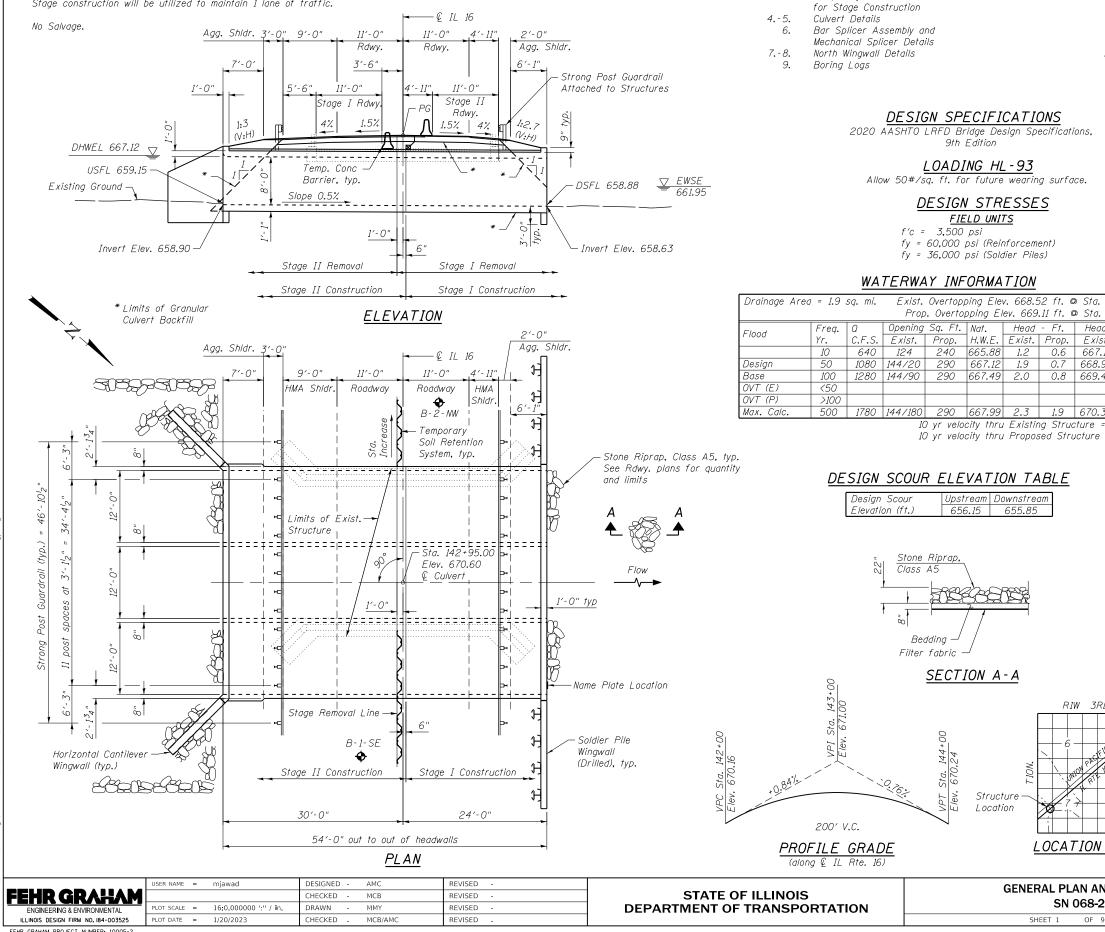
Backfill. Backfill should consist of <u>Granular Culvert Backfill</u>. The special provision is attached. A detail showing pay limits should be included. Pay limits include the temporary excavation limits in a section along the roadway and from edge of shoulder to edge of shoulder in a section along the culvert.

Ground Improvement. No ground improvement is necessary below the culvert barrel or below wingwalls.

Drilled Soldier Piles. The borings indicate Cohesionless Soils below the groundwater table will be present. The Contractor should anticipate the challenges of drilling in Cohesionless Soils below the groundwater table.



Existing Structure: SN 068-0016 at Sta. 143+00 was built in 1923 as SBI 16, Section 18. The HMA overlay was replaced in 1973 and in 2002 the bridge rail was replaced. The Structure is a single span concrete deck slab on closed abutments, 26'-0" bk. to bk. of abutments and 32'-2" out to out deck, no skew. Stage construction will be utilized to maintain 1 lane of traffic.



FEHR GRAHAM PROJECT NUMBER: 10005-2

GENERAL NOTES

Layout of slope protection system may be varied to suit ground conditions in the field as directed by the Engineer.

Excavation behind existing abutment walls shall be performed to balance front and back soil pressure before removing the existing superstructure. The Contractor shall sawcut the upper portion of the existing abutment at the stage removal line before Stage I removal to ensure the remaining portion will not be prematurely damaged.

TOTAL BILL OF MATERIAL

| ITEM | UNIT | TOTAL |
|--|---------|--------|
| Removal of Existing Structures No. 2 | Each | 1 |
| Reinforcement Bars | Pound | 39,740 |
| Bar Splicers | Each | 160 |
| Name Plates | Each | 1 |
| Concrete Box Culverts | Cu. Yd. | 243.2 |
| Granular Culvert Backfill | Cu. Yd. | 158 |
| Temporary Soil Retention System | Sq. Ft. | 381 |
| Membrane Waterproofing System for | Sq. Yd. | 235 |
| Buried Structures | | |
| Geocomposite Wall Drain | Sq. Yd. | 251 |
| Strong Post Guardrail Attached to Culvert | Foot | 94 |
| Furnishing Soldier Piles (HP Section) | Foot | 250 |
| Drilling and Setting Soldier Piles (in soil) | Cu. Ft. | 740 |
| Untreated Timber Lagging | Sq. Ft. | 402 |
| Stud Shear Connectors | Each | 104 |

| 14 | 3+00.00 | | | | | | | | |
|------------|----------|--|--|--|--|--|--|--|--|
| 137+00.00 | | | | | | | | | |
| lwater El. | | | | | | | | | |
| t. | Prop. | | | | | | | | |
| 11 | 666.48 | | | | | | | | |
| 97 | 667.80 | | | | | | | | |
| 8 | 668.29 | | | | | | | | |
| | | | | | | | | | |
| | | | | | | | | | |
| 3 | 669.88 | | | | | | | | |
| 6 | .47 fps | | | | | | | | |
| = | 4.07 fps | | | | | | | | |

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RIW 3RD P.M.

LOCATION SKETCH

Head - Ft.

INDEX OF SHEETS

Stage Construction Details

Temporary Concrete Barrier

General Plan

2.

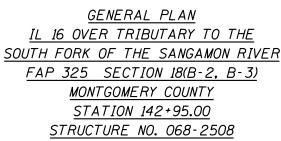
3.

STATION 142+95.00 BUILT 20___ BY STATE OF ILLINOIS F.A.P. RTE. 325 SEC. 18(B-2, B-3) LOADING HL-93 STR. NO. 068-2508

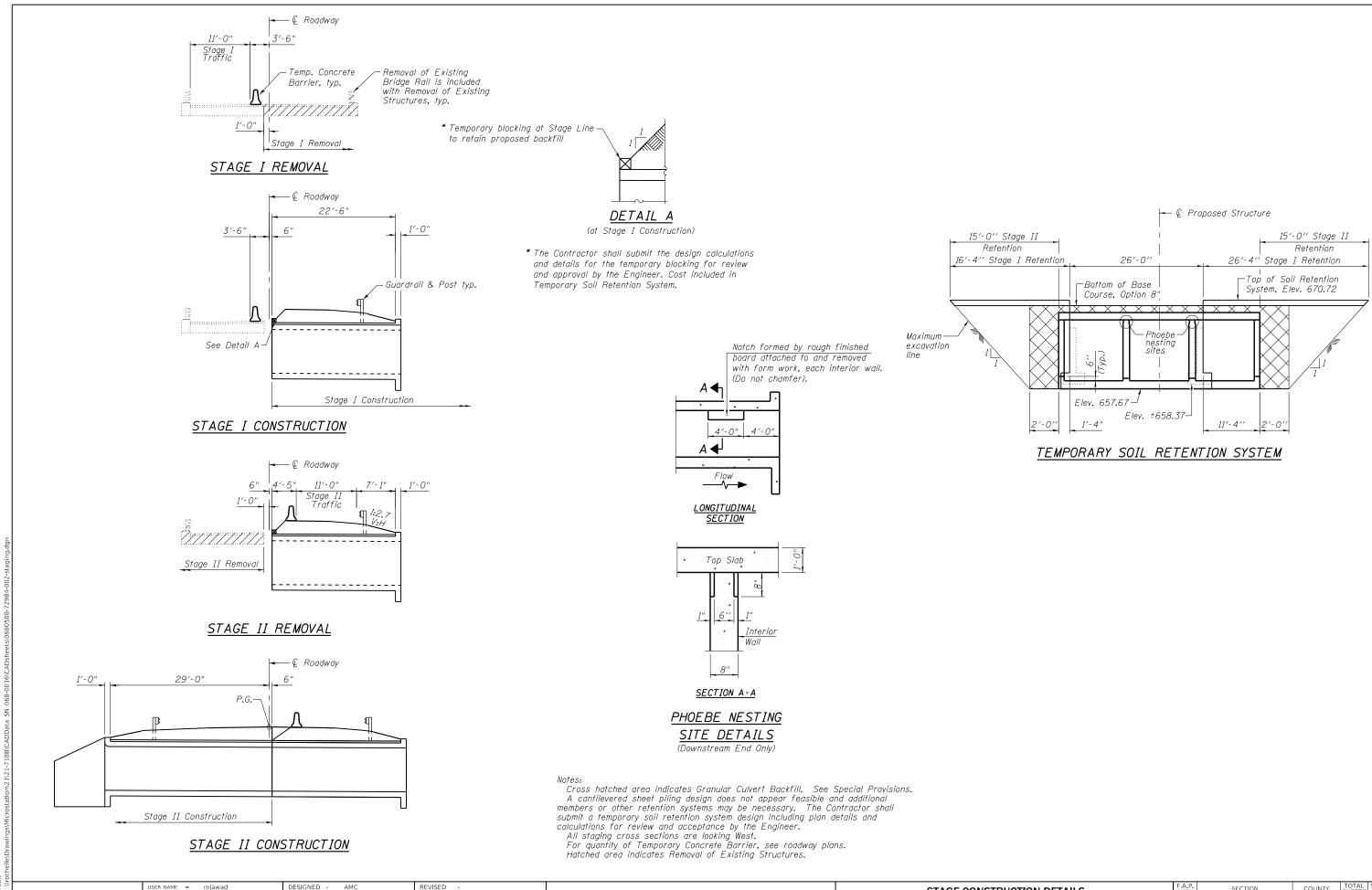
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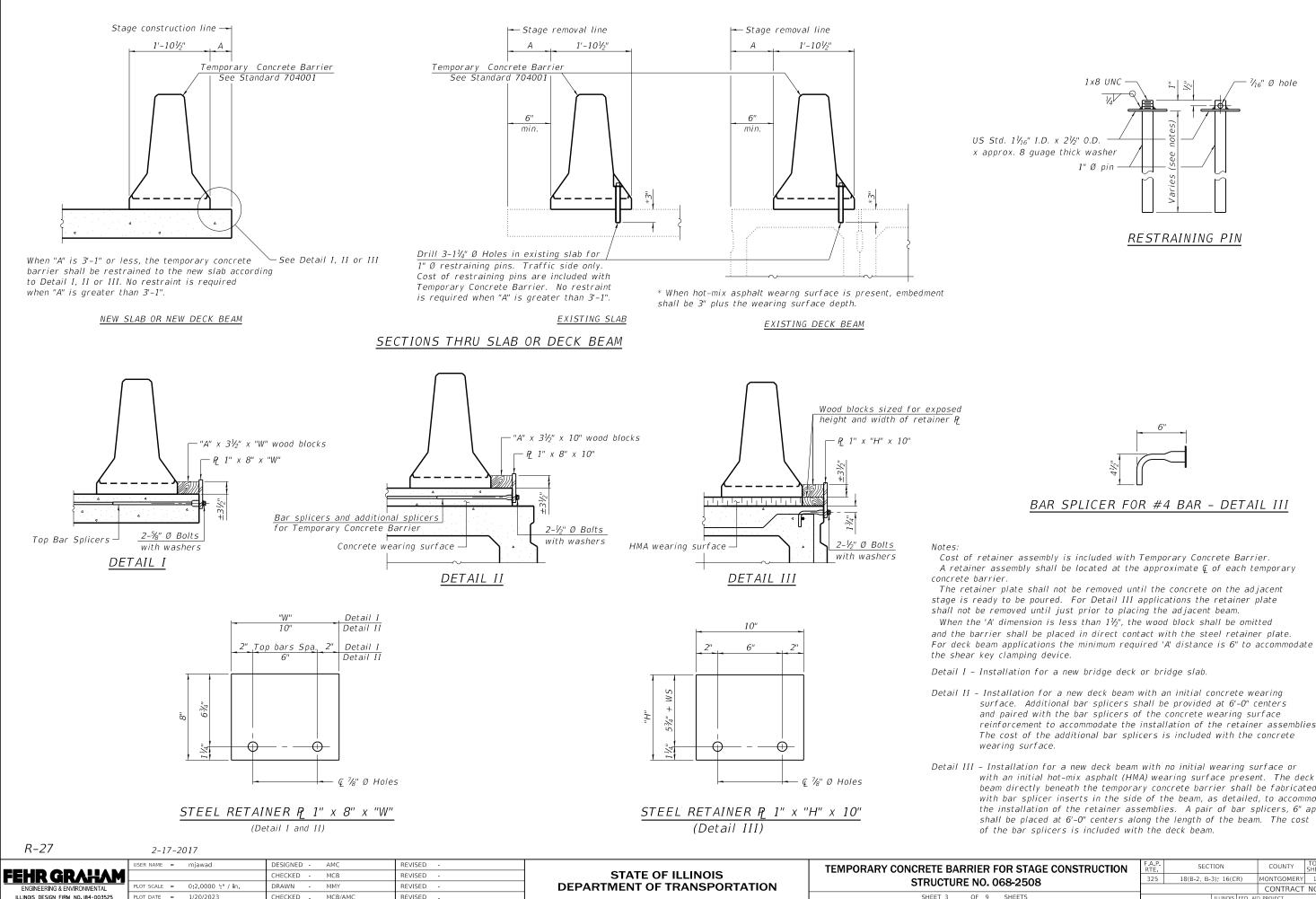
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| GENERAL PLAN AND ELEVATION | F.A.P. RTE | SECTION | COUNTY | TOTAL SHEETS | SHEET NO. | |
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| SN 068-2508 | 325 | 18(B-2, B-3); 16(CR) | MONTGOMERY | 142 | 113 | |
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| efat | | USER NAME = | mjawad | DESIGNED - A | AMC | REVISED - | | STAGE CONSTRUCTION DETAILS | F.A.P. SECTION | COUNTY TOTAL SHEET |
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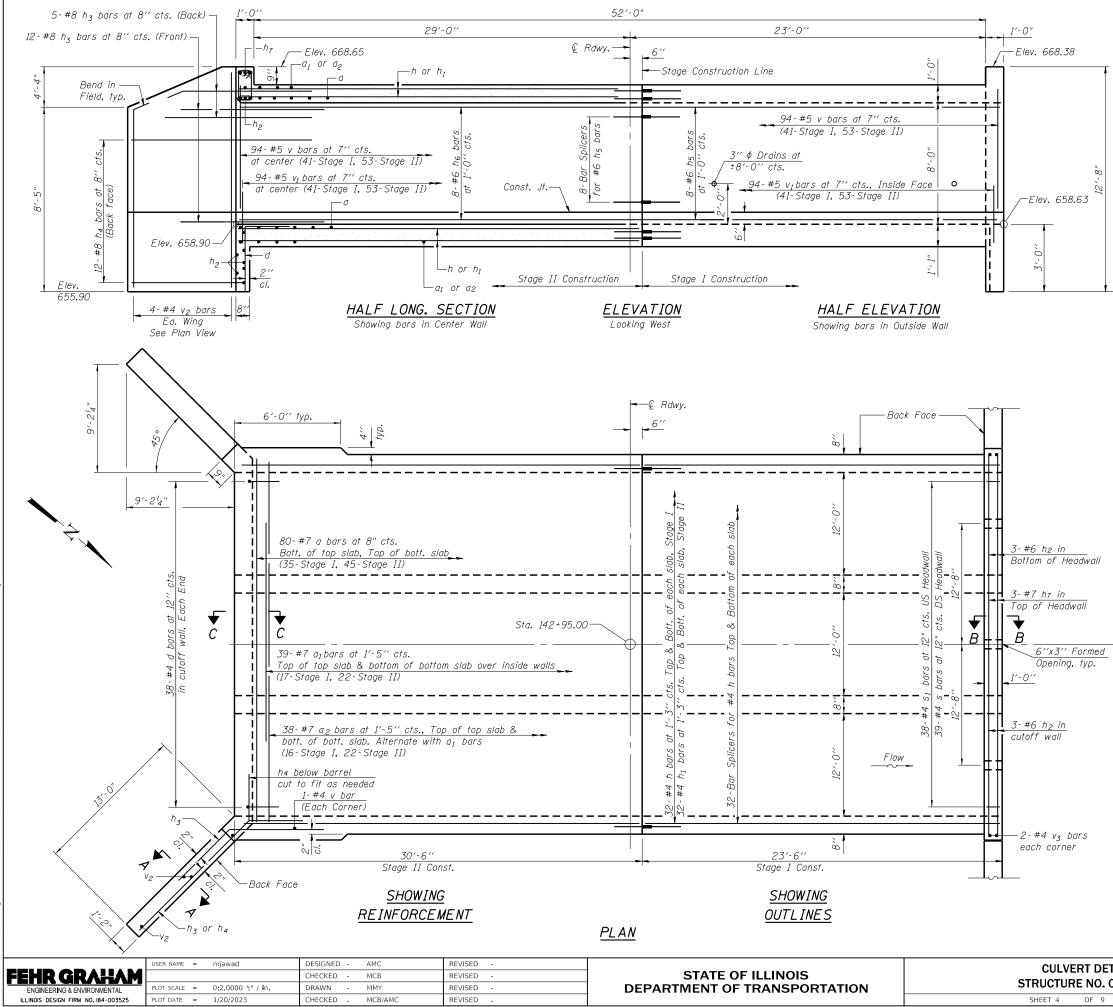
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SHEET 3 OF 9

reinforcement to accommodate the installation of the retainer assemblies.

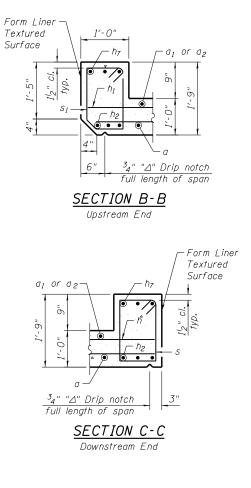
beam directly beneath the temporary concrete barrier shall be fabricated with bar splicer inserts in the side of the beam, as detailed, to accommodate the installation of the retainer assemblies. A pair of bar splicers, 6" apart,

| R FOR STAGE CONSTRUCTION | F.A.P. RTE | SECT | FION | | COUNTY | TOTAL SHEETS | SHEET NO. | |
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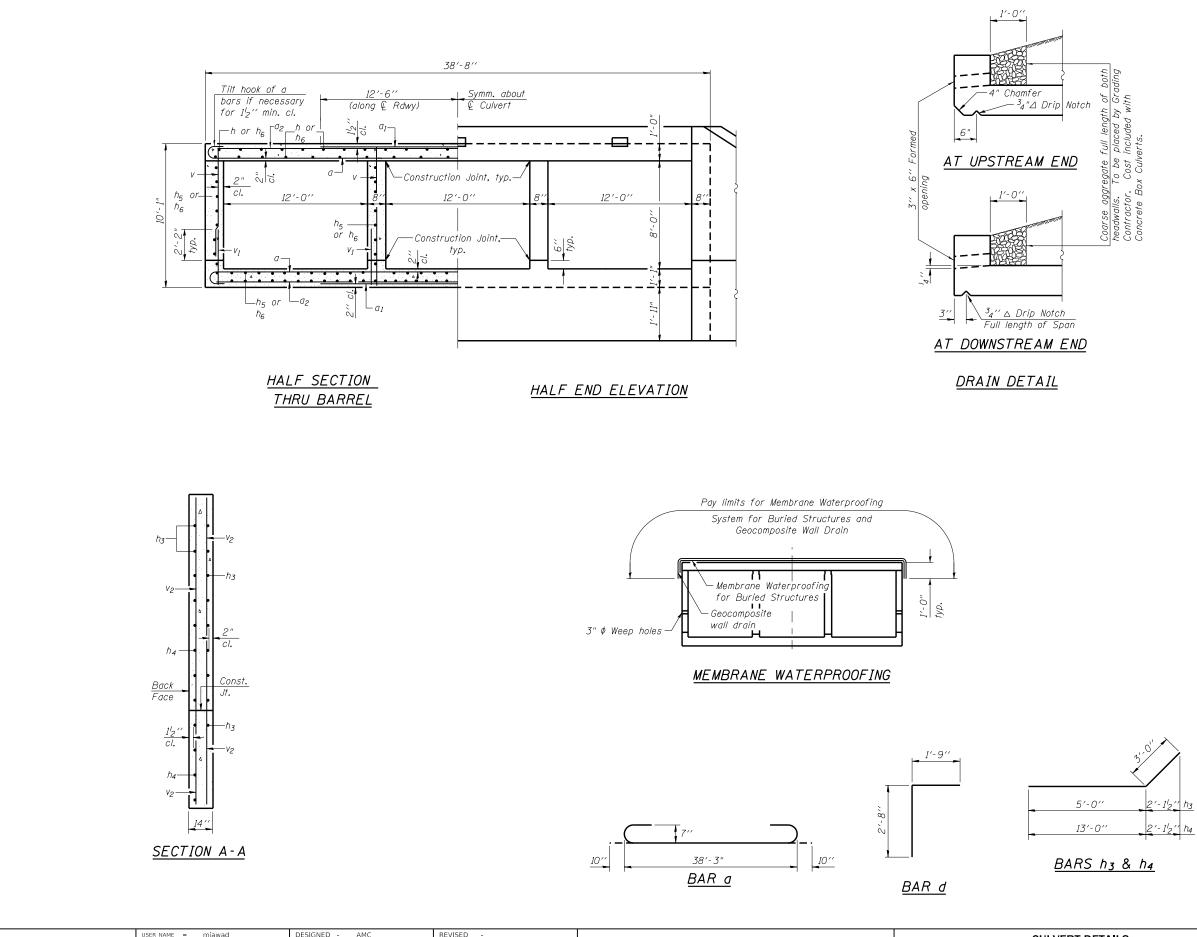
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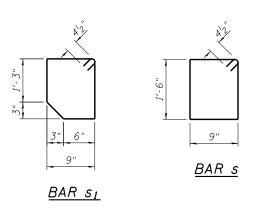
Note: See sheet 5 of 9 for Sec. A-A, bar details and Bill of Material.

| ETAILS | F.A.P. RTE | SECT | FION | | COUNTY | TOTAL SHEETS | SHEET NO. | | |
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— € Culvert



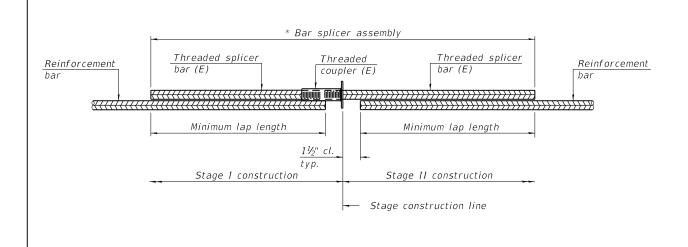
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Notes: A distance of half the length of the wingwall but not less than six feet of the barrel shall be poured monolithically with the wingwalls.

| Bar | | | | |
|----------------------|-----------|-------|----------|--------|
| Bur | No. | Size | Length | Shape |
| a | 160 | #7 | 39′-11′′ | |
| aı | 78 | #7 | 25'-0'' | |
| <i>0</i> 2 | 76 | #7 | 38'-3'' | |
| | | | | |
| d | 76 | #4 | 4'-5'' | |
| | | | | |
| h | 128 | #4 | 23'-2'' | |
| h1 | 128 | #4 | 30'-2'' | |
| h2 | 12 | #6 | 38'-3'' | |
| hз | 34 | #8 | 8'-0'' | |
| h4 | 24 | #8 | 16'-0'' | |
| h5 | 32 | #6 | 23'-2'' | |
| h ₆ | 32 | #6 | 30'-2'' | |
| h7 | 6 | #7 | 38'-3'' | |
| h8 | 52 | #5 | 17'-8'' | |
| | | | | |
| S | 39 | #4 | 5′-3″ | |
| S1 | 38 | #4 | 5′-4″ | 0 |
| | | | | |
| V | 380 | #5 | 8'-2'' | |
| V1 | 376 | #5 | 3'-4" | |
| V2 | 8 | #4 | 12'-5'' | |
| V3 | 80 | #4 | 12'-5'' | |
| | | | | |
| Concrete L | | | Cu. Yd. | 243.2 |
| Reinforcer | | | Pound | 39,740 |
| Membrane | | | | 225 |
| System fo | | 1 | Sq. Yd. | 235 |
| Structures | | | | |
| Furnishing | | | Foot | 250 |
| Piles (HP | | | | |
| Drilling an | | | Cu. Ft. | 740 |
| Soldier Pi | | 5011) | | |
| Untreated | imper | | Sq. Ft. | 402 |
| Lagging Geocompos | site Mall | | | |
| Geocompos Drain | sie wall | | Sq. Yd. | 251 |
| Stud Shea | r Conne | ctors | Each | 104 |
| Bar Splice | | | Each | 160 |
| 237 397700 | | | Luch | 100 |

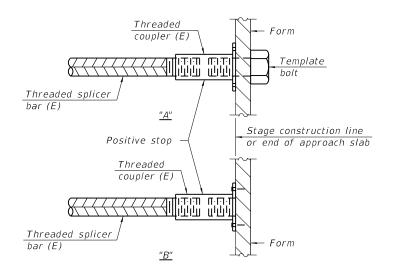
BILL OF MATERIAL



STANDARD BAR SPLICER ASSEMBLY PLAN

(All components shall be provided from one supplier)

* Epoxy not required on Bar Splicer Assembly components used in



INSTALLATION AND SETTING METHODS

- "A" : Set bar splicer assembly by means of a template bolt.
- "B" : Set bar splicer assembly by nailing to wood forms or cementing to steel forms. (E) : Indicates epoxy coating.

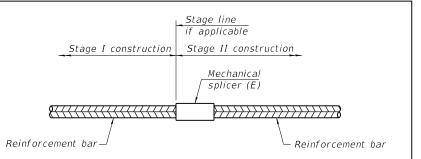
conjunction with black bars. No. assemblies Minimum Bar Location size required lap length Top Slab #4 64 1'-5" #4 1'-5" Bottom Slab 64 32 Walls #6 2'-11"

Threaded splicer bar length = min. lap length + $1\frac{1}{2}$ " + thread length

| 1-1-202 | 2 |
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| ult roche | BSD-1 | 1-1-2020 | | | | | | | |
|--------------|--------------------------------------|---------------------------------|-------------------|-----------|------------------------------|---|---------------|----------------------|--------------------|
| efat | | USER NAME = mjawad | DESIGNED - AMC | REVISED - | | BAR SPLICER ASSEMBLY AND MECHANICAL SPLICER DETAILS | F.A.P. BTE | SECTION | COUNTY TOTAL SHEET |
| AME . | FEHR GRAHAM | | CHECKED - MCB | REVISED - | STATE OF ILLINOIS | | 325 | 18(B-2, B-3); 16(CR) | MONTGOMERY 142 118 |
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FEHR GRAHAM PROJECT NUMBER: 10005-2



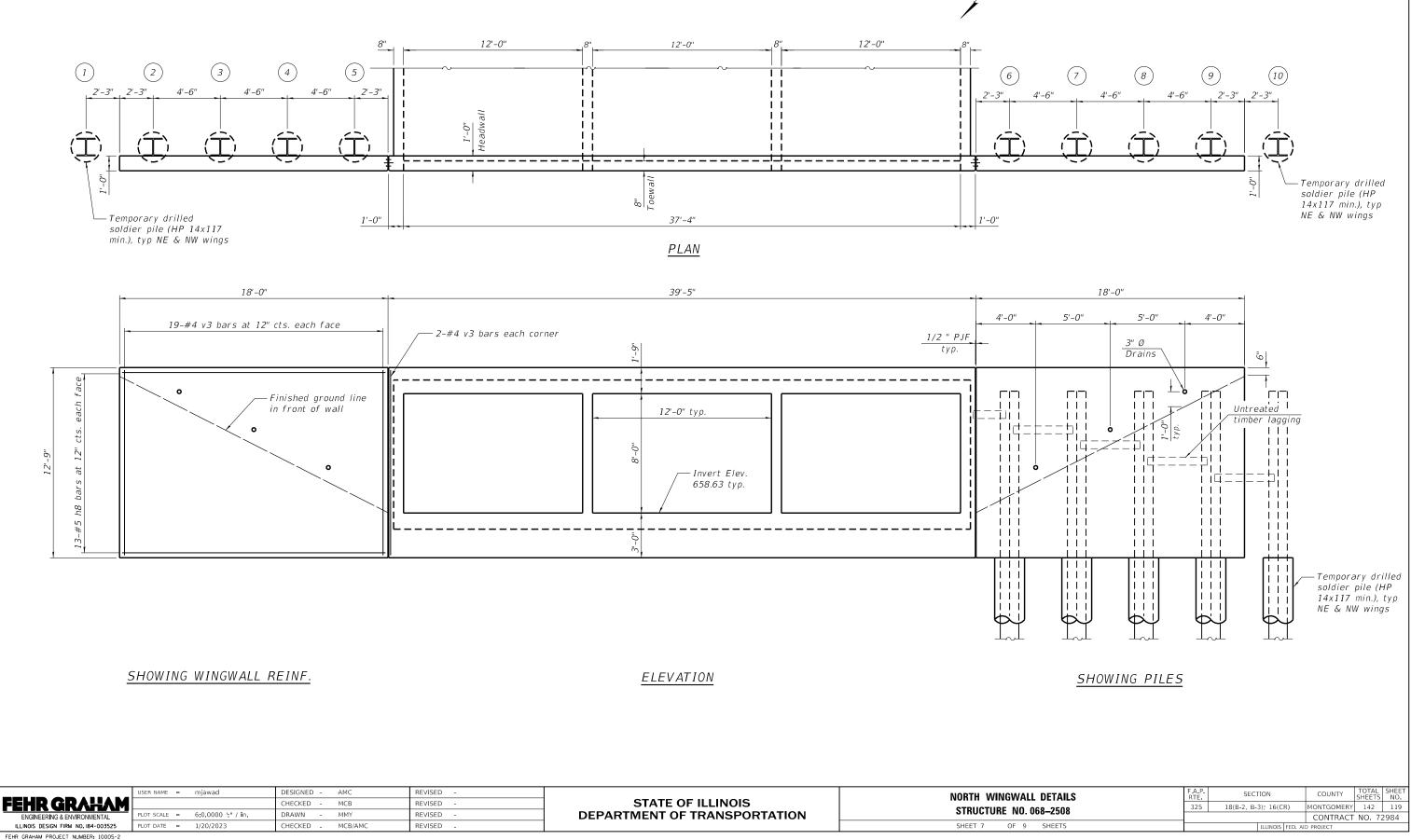
STANDARD MECHANICAL SPLICER

| l a satism | Bar | No. assemblies |
|------------|------|----------------|
| Location | size | required |
| | 0.20 | |
| | | |
| | | |
| | | |
| | | |
| | | |

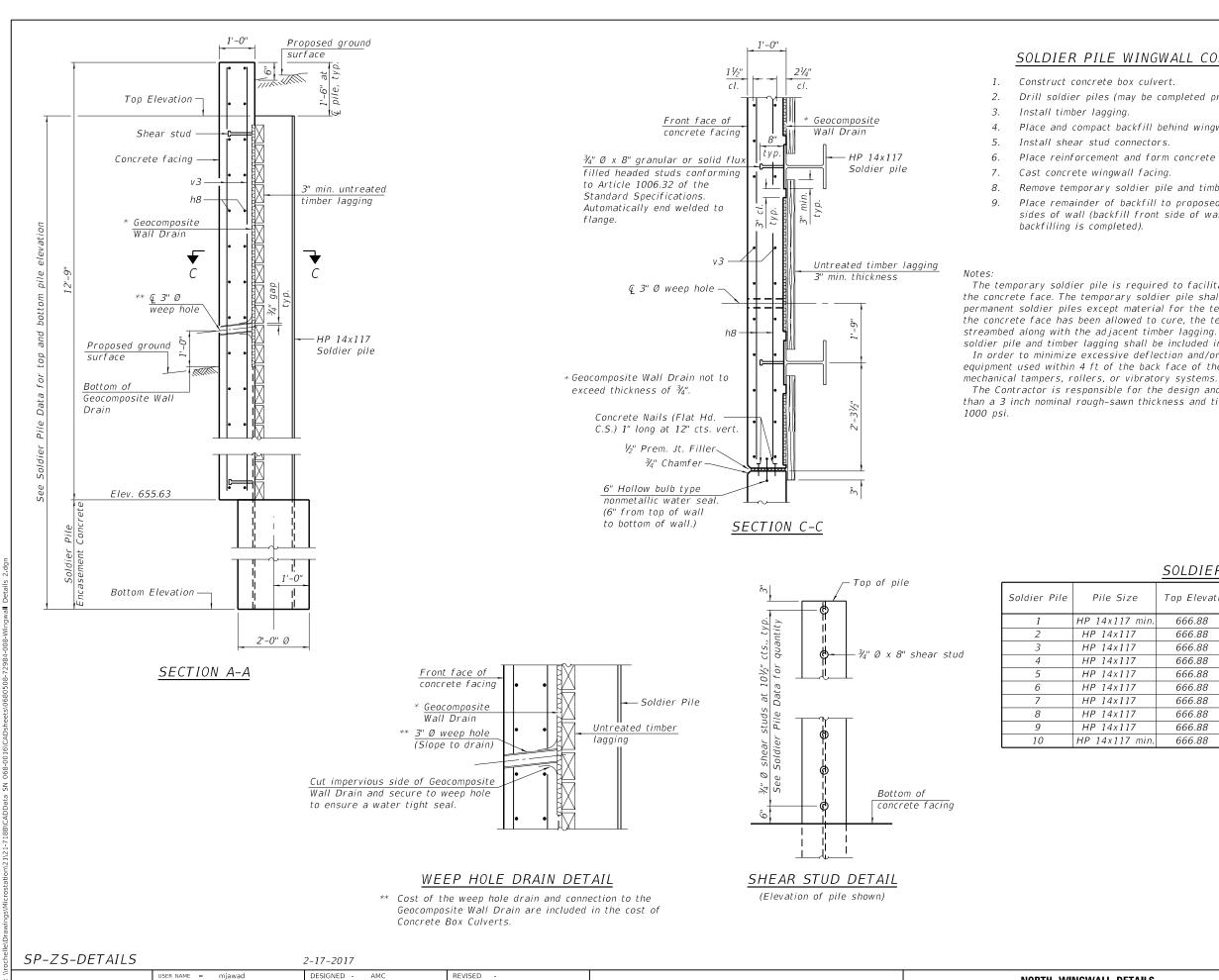
Notes:

Splicer bars shall be deformed with threaded ends and have a minimum 60 ksi yield strength.

All reinforcement shall be lapped and tied to the splicer bars. Bar splicer assemblies shall be epoxy coated according to the requirements for reinforcement bars. See Section 508 of the Standard Specifications. See approved list of bar splicer assemblies and mechanical splicers for alternatives.



| efau : ∖\r | | USER NAME = mjawad | DESIGNED - AMC | REVISED - | | NORTH WINGWALL DI |
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STATE OF ILLINOIS

DEPARTMENT OF TRANSPORTATION

ILLINOIS DESIGN FIRM NO. 184-003525 FEHR GRAHAM PROJECT NUMBER: 10005-2

EHR GRAHAM

NORTH WINGWAL STRUCTURE NO. SHEET 8 OF 9

CHECKED -

CHECKED -

DRAWN

MCB

MM

MCB/AMC

REVISED

REVISED

REVISED

PLOT DATE = 1/20/2023

OT SCALE = 0:2.0000 '." / in.

SOLDIER PILE WINGWALL CONSTRUCTION SEQUENCE

- Drill soldier piles (may be completed prior to completing construction of box culvert).
- Place and compact backfill behind wingwall to top of timber lagging.
- Place reinforcement and form concrete wall face.
- Remove temporary soldier pile and timber lagging outside limits of the wingwall. Place remainder of backfill to proposed ground surface elevations on both sides of wall (backfill front side of wall as much as possible before

The temporary soldier pile is required to facilitate backfilling of the wingwall prior to casting the concrete face. The temporary soldier pile shall conform to the construction requirements for permanent soldier piles except material for the temporary soldier pile may be new or used. After the concrete face has been allowed to cure, the temporary soldier pile shall be removed 2 ft below streambed along with the adjacent timber lagging. Cost of removing and disposing temporary soldier pile and timber lagging shall be included in the cost of Concrete Box Culverts.

In order to minimize excessive deflection and/or stresses in the soldier piles, compaction equipment used within 4 ft of the back face of the timber lagging shall be limited to lightweight

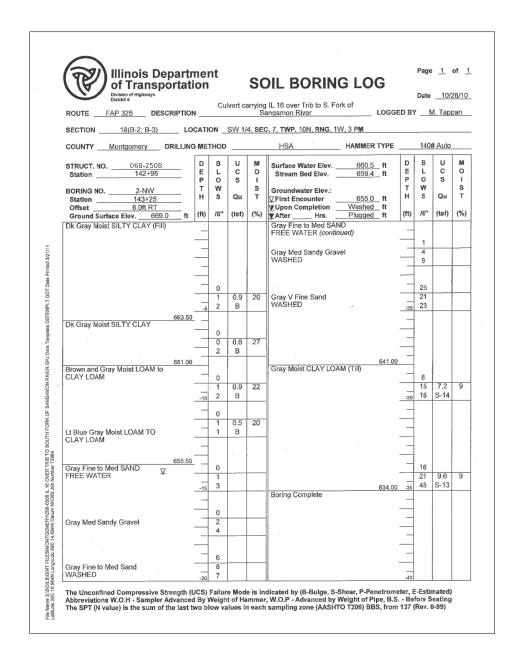
The Contractor is responsible for the design and performance of the timber lagging using no less than a 3 inch nominal rough-sawn thickness and timber with a minimum allowable bending stress of

| ile Size | Top Elevation | Bottom Elevation | Total Height (Ft.) | Number of Shear Studs |
|------------|---------------|---------------------|-----------------------|--------------------------|
| 4x117 min. | 666.88 | 635.63 | 31'-3" | |
| 14×117 | 666.88 | 635.63 | 31'-3" | 13 |
| 14×117 | 666.88 | 635.63 | 31'-3" | 13 |
| 14x117 | 666.88 | 635.63 | 31'-3" | 13 |
| 14x117 | 666.88 | 635.63 | 31'-3" | 13 |
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| 14x117 | 666.88 | 635.63 | 31'-3" | 13 |
| 14×117 | 666.88 | 635.63 | 31'-3" | 13 |
| 4x117 min. | 666.88 | 635.63 | 31'-3" | |

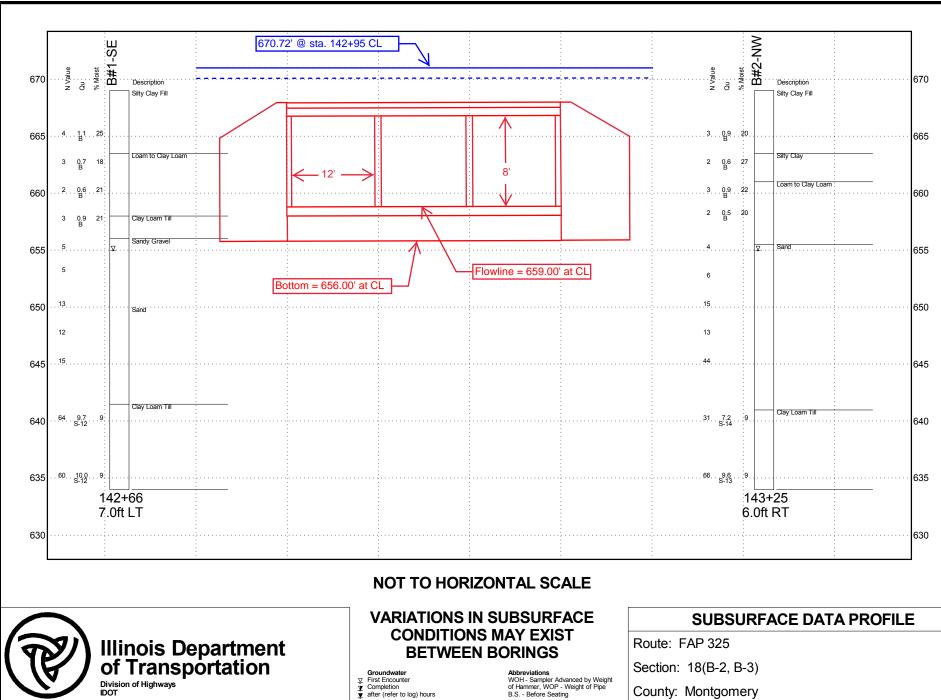
SOLDIER PILE DATA

| LL DETAILS | F.A.P. RTE | F.A.P. SECTION | | COUNTY | TOTAL SHEETS | SHEET NO. |
|------------|---------------|---------------------|---------|------------|-----------------|--------------|
| . 068–2508 | 325 | 18(B-2, B-3); 16(CR | .) | MONTGOMERY | 142 | 120 |
| . 000–2300 | | | | CONTRACT | NO. 72 | 2984 |
| SHEETS | | ILLINOIS F | ED, AIC | PROJECT | | |

| Illinois Depar of Transporta | tion | nτ | | S | DIL BORIN | g log | | | <u> </u> | |
|--|-------------|-------------|-------------|-------------|--|-----------------|-------------|-------------|--------------|-------------|
| Division of Highways District 6 | | Cu | lvert c | arrvino | a IL 16 over Trib to S. Fo | rk of | | | 10/: | |
| ROUTE FAP 325 DESCRIPT | ON | | | Ś | angamon River | LOG | GED B | Y! | M. Tap | pan |
| SECTION18(B-2, B-3) L | OCATI | ON _ | SW 1 | 4, SE | C. 7, TWP. 10N, RNG. 1V | V, 3 PM | | | | |
| COUNTY Montgomery DRILLI | NGME | THOD | | | HSA | HAMMER TYP | 'Е | 140 | # Auto | |
| STRUCT. NO. 068-2508 Station 142+95 | D E P | B L O | U C S | M 0 [| Surface Water Elev Stream Bed Elev | | D E P | B L O | U C S | M O I |
| SORING NO | T H | W S | Qu | S T | Groundwater Elev.: ⊈First Encounter | 655.0 ft | Т | WS | Qu | S T |
| Station 142+66 Offset 7.0ft LT | | /6" | | | Upon Completion | Washed ft | (ft) | /6" | (tsf) | (%) |
| Ground Surface Elev. 669.0 ft Black to Brown and Gray Moist | (ft) | 76 | (tsf) | (%) | After Hrs Washed | | (11) | 10 | (LSI) | (70) |
| SILTY CLAY (Fill) | _ | | | | Gray Wet Med SANDY FREE WATER (contin | (GRAVEL ued) | | 2 | | |
| | | | | | Gray Coarse SANDY | | _ | 6 | | |
| | _ | | | | Washed | | _ | 6 | | |
| | _ | 1 | | | | | _ | 7 | | |
| | | 2 | 1.1 | 25 | | | | 6 | | |
| 663. | -5 | 2 | В | | - | | 25 | 9 | | |
| Brown and Gray Moist LOAM to CLAY LOAM | | o | | | | | | | | |
| | | 1 | 0.7 | 18 | - | | _ | | | |
| | · _ | 2 | В | | Gray Moist CLAY LOA | 641 M (Till) | .50 | | | |
| | _ | 0 | | | Washed | | | 7 | | Ĺ |
| | | 1 | 0.6 | 21 | - | | | 21 | 9.7 | 9 |
| | 10 | 1 | B | | - | | 30 | 43 | S-12 | - |
| 658.0 Brown and Olive Gray Moist | | 0 | | | | | | | - | |
| CLAY LOAM (TIII) | | 1 | 0.9 | 21 | | | _ | | | |
| 656.0 | | 2 | В | | | | _ | | | |
| Gray Wet Med SANDY GRAVEL | _ | 0 | | | | | . — | 7 | | |
| VIEW V | _ | 2 | | | | | _ | 21 | 10.0 S-12 | 9 |
| | -15 | 3 | - | | Boring Complete | 634 | .00 -35 | - 39 | 3-12 | |
| | _ | 0 | | · · · | - | | _ | | | |
| Gray Fine SANDY GRAVEL | | 3 | | | - | | | | | |
| | _ | | | | | | | | | |
| | _ | 2 | | | | | _ | | | |
| Gray Med to Coarse SAND v/ some Pea Gravel | -20 | 7 | | | | | -40 | | | |



| efar | | USER NAME = mjawad | DESIGNED - | AMC | REVISED - | | BORING LOGS | F.A.P. BTE | SECTION | COUNTY TOTAL SH | |
|------|-------------------------------------|---------------------------------|------------|---------|-----------|------------------------------|------------------------|-------------------|---------------------------|------------------|--|
| AME | EHR GRAHAM | | CHECKED - | MCB | REVISED - | STATE OF ILLINOIS | STRUCTURE NO. 068-2508 | 325 | 18(B-2, B-3); 16(CR) | MONTGOMERY 142 1 | |
| | ENGINEERING & ENVIRONMENTAL | PLOT SCALE = 0:2.0000 ':" / in. | DRAWN - | MMY | REVISED - | DEPARTMENT OF TRANSPORTATION | 31R0CTURE NO. 008-2508 | CONTRACT NO. 7298 | | | |
| MO | ILLINOIS DESIGN FIRM NO. 184-003525 | PLOT DATE = 1/20/2023 | CHECKED - | MCB/AMC | REVISED - | | SHEET 9 OF 9 SHEETS | | ILLINOIS FED. AID PROJECT | | |
| 2 11 | R GRAHAM PROJECT NUMBER: 10005-2 | PLOT DATE = 1/20/2023 | CHECKED - | мевламе | REVISED - | | SHEELY OF Y SHEELS | | ILLINOIS FED. | AID PROJ | |



Structure Number 068-0508 Culvert carrying IL 16 over Trib to S. Fork of Sangamon River Located in the SW 1/4 of Section 7, Township 10N, Range 1W of the 3 P.M.

| Illinois Depar of Transporta | tme ation | nt | | SC | DIL BORIN | IG LOO | 3 | | Page | <u>1</u> | of <u>1</u> |
|---|-----------------|-------------|-------------|---------------|---|--------------------------------------|--------|-------------|-------------|--------------|-------------|
| Division of Highways District 6 | | | ulvert c | arrvino | g IL 16 over Trib to S. Fo | ork of | | | Date | 10/2 | 28/10 |
| ROUTE FAP 325 DESCRIPT | ION | | | | angamon River | | LOGGE | D BY | N | И. Тарр | ban |
| SECTION 18(B-2, B-3) | LOCATI | ON _ | SW 1/ | 4, SEC | C. 7, TWP. 10N, RNG. 1 | W, 3 PM | | | | | |
| COUNTY Montgomery DRILL | | THOD | | | HSA | | TYPE | | 140; | # Auto | |
| STRUCT. NO. 068-0508 Station 142+95 | D E P | B L O | U C S | M O I | Surface Water Elev. Stream Bed Elev. | <u> 660.5</u> <u> 659.4</u> | | D E P | B L O | U C S | M O I |
| BORING NO. 1-SE Station 142+66 | T H | W S | Qu | S T | Groundwater Elev.: | 655.0 | ft | T H | W S | Qu | S T |
| Offset 7.0ft LT | ft (ft) | | (tsf) | (%) | | Washed Plugged | ft | (ft) | /6" | (tsf) | (%) |
| Black to Brown and Gray Moist SILTY CLAY (Fill) | n (49 | | | (14) | Washed | | _ n | | | (, | (/ |
| SILTT CLAT (FIII) | | _ | | | Gray Wet Med SAND FREE WATER (conti | inued) | | | 2 | | |
| | | | | | Gray Coarse SANDY Washed | GRAVEL | | | 6 6 | | |
| | | | | | | | | | Ū | | |
| | _ | 1 | | | | | | _ | 7 | | |
| | | 2 | 1.1 B | 25 | | | | -25 | 6 9 | | |
| | <u></u> 3.50 | - | | | - | | | | • | | |
| Brown and Gray Moist LOAM to CLAY LOAM | | 0 | | | | | | | | | |
| | | 1 | 0.7 B | 18 | | | 641.50 | | | | |
| | | | | | Gray Moist CLAY LO | AM (Till) | 041.50 | | | | |
| | _ | 0 | | | Washed | | | _ | 7 | | |
| | | 1 | 0.6 B | 21 | | | | | 21 43 | 9.7 S-12 | 9 |
| | <u>-10</u> | - | | | | | | 30 | | 0.2 | |
| Brown and Olive Gray Moist CLAY | 3.00 | 0 | | | | | | | | | |
| LOAM (Till) | | 1 | 0.9 B | 21 | | | | | | | |
| | .00 | 1 | | | 1 | | | | | | |
| Gray Wet Med SANDY GRAVEL FREE WATER | _ | 0 | | | | | | _ | 7 | | |
| - <u></u> | | 2 | | | | | 634.00 | | 21 39 | 10.0 S-12 | 9 |
| | <u>-15</u> | | | | Boring Complete | | 034.00 | - <u>35</u> | | | |
| | | 0 | | | | | | | | | |
| Gray Fine SANDY GRAVEL | | 3 | | | - | | | | | | |
| | | | | | | | | | | | |
| | _ | 2 | | | | | | _ | | | |
| Gray Med to Coarse SAND w/ some Pea Gravel | | 7 | | | 1 | | | | | | |
| | -20 | 6 | | | | | | -40 | | | |

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer, E-Estimated) Abbreviations W.O.H - Sampler Advanced By Weight of Hammer, W.O.P - Advanced by Weight of Pipe, B.S. - Before Seating The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206) BBS, from 137 (Rev. 8-99)

| Illinois Depart of Transporta | tion | nt | | SC | | G LOC | 3 | | Page | <u>1</u> | of <u>1</u> |
|--|------------------|------------------|-------------|------------------|---|----------------|--------|------------------|------------------|-------------|------------------|
| Division of Highways District 6 | | | wate | ornina | ull 16 over Trib to C. For | rk of | | | Date | 10/2 | 28/10 |
| ROUTE FAP 325 DESCRIPTION | DN | | | San ying Sa | IL 16 over Trib to S. Foi angamon River | | LOGGE | DBY | N | И. Тар | oan |
| SECTION18(B-2, B-3) L | OCATI | ON _ | SW 1/ | 4, SEC | 2. 7, TWP. 10N, RNG. 1W | V, 3 PM | | | | | |
| COUNTY Montgomery DRILLIN | IG ME | rhod | | | HSA | | TYPE | | 1407 | # Auto | |
| STRUCT. NO. 068-0508 Station 142+95 | D E P T | B L O W | U C S | M O I S | Surface Water Elev Stream Bed Elev Groundwater Elev.: | | | D E P T | B L O W | U C S | M O I S |
| BORING NO. 2-NW Station 143+25 Offset 6.0ft RT | H | S | Qu | T | | 655.0 | ft | H | S | Qu | T |
| | t (ft) | /6" | (tsf) | (%) | ⊈ Upon Completion _ _ _ After Hrs. | Plugged | | (ft) | /6" | (tsf) | (%) |
| Dk Gray Moist SILTY CLAY (Fill) | | - | | | Gray Fine to Med SAN FREE WATER (contin | ID ued) | | | | | |
| | | - | | | | - | | | 1 | | |
| | | | | | Gray Med Sandy Grave WASHED | ei | | | 4 9 | | |
| | | - | | | | | | | | | |
| | | 0 | 0.9 | 20 | Gray V Fine Sand | | | | 25 21 | | |
| | | 2 | B | 20 | WASHED | | | -25 | 23 | | |
| 663.4 Dk Gray Moist SILTY CLAY | 50 | - | | | | | | _ | | | |
| | | 0 | 0.6 | 27 | | | | _ | | | |
| | | 2 | B | | | | | | | | |
| 661.0 Brown and Gray Moist LOAM to | 00 | - | | | Gray Moist CLAY LOA | M (Till) | 641.00 | | | | |
| CLAY LOAM | | 0 | 0.9 | 22 | - | | | | 8 15 | 7.2 | 9 |
| | -10 | | B | | - | | | -30 | 16 | S-14 | |
| | | 0 | | | | | | | | | |
| Lt Blue Gray Moist LOAM TO | _ | 1 | 0.5 B | 20 | | | | _ | | | |
| CLAY LOAM | | - | | | | | | | | | |
| 655.4 | 50 | | | | | | | | | | |
| Gray Fine to Med SAND FREE WATER ∑ | | 0 | | | - | | | | 16 21 | 9.6 | 9 |
| | - <u>15</u> | 3 | | | Boring Complete | | 634.00 | - <u>35</u> | 45 | S-13 | |
| | | | | | | | | | | | |
| Gray Med Sandy Gravel | | 0 | | | - | | | _ | | | |
| | | 4 | | | - | | | | | | |
| | | | | | | | | | | | |
| Gray Fine to Med Sand | | 6 8 | | | - | | | | | | |
| WASHED | -20 | 7 | | | | | | -40 | | | |

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer, E-Estimated) Abbreviations W.O.H - Sampler Advanced By Weight of Hammer, W.O.P - Advanced by Weight of Pipe, B.S. - Before Seating The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206) BBS, from 137 (Rev. 8-99)

GRANULAR CULVERT BACKFILL 6M6 10/15/13

This work consists of backfilling box culverts or three-sided structures with granular materials. This work shall be performed at locations shown on the plans or as directed by the Engineer.

Backfilling shall be performed according to Article 502.10. The backfill material shall meet the requirements of Article 1004.05, except the gradation shall be CA-06 or CA-10. This work satisfies select granular backfill (porous granular material) requirements of ASTM C 1577.

Granular Culvert Backfill will be measured for payment in cubic yards compacted in place. Additional material required to backfill excavation outside the limits shown on the plans will not be measured for payment. This work shall be paid for at the contract unit price per cubic yard for GRANULAR CULVERT BACKFILL.

ROCKFILL - FOUNDATION 6M10 6/15/17

This work consists of constructing a layer of rockfill below culverts or spread footings having unstable or unsuitable soil conditions. When shown on the plans, the rockfill limits and thickness shall be confirmed by the Engineer prior to excavating below the theoretical top of rockfill line.

Rockfill materials shall meet the requirements of Article 1005.01 of the Standard Specifications. The gradation of rockfill shall be primary crusher run. The maximum dimension shall be 8 inches. Rockfill may contain broken pavement or rock excavation as defined in Article 205.04 and with the approval of the Engineer.

Materials shall meet the requirements of the following Articles of the Standard Specifications:

Bedding or Capping Material 1003.04 or 1004.05

The method of rockfill placement shall be approved by the Engineer. Rockfill shall be capped according to application as shown below:

| Spread Footing | 4 to 6 inches CA-6 |
|----------------------------|---|
| Cast-In-Place Box Culverts | 4 to 6 inches CA-7 or CA-11 |
| Pre-Cast Box Culverts | Porous Granular Bedding Material (Article 540.02) |
| Pre-Cast Pipe Culverts | Coarse or Fine Aggregate Bedding (Article 542.04) |

Excavation shall be performed according to Section 202 of the Standard Specifications.

In spread footing applications, the CA-6 cap shall be compacted to the satisfaction of the Engineer. No compaction of rockfill is required for culvert applications.

This work will be measured and paid for at the contract unit price per ton for ROCKFILL -FOUNDATION. The contract price for ROCKFILL-FOUNDATION shall include excavation, aggregate materials, aggregate material placement, and placement of excavated materials within right-of-way or disposal off right-of-way. *Excavation will not be measured or paid for separately or as part of EARTH EXCAVATION.* For precast concrete box culverts, porous granular bedding material and the excavation volume required for bedding will be paid for according to Article 540.08. For pipe culverts, the aggregate bedding material and excavation volume required for the aggregate bedding material will be paid for according to Article 542.11.